

Axial Depletion Behavior of Gd-155 and Gd-157 in an i-SMR Core Considering Coolant Temperature Gradients

Ji Hoon Lee¹, Jin Sun Kim², Gonghoon Bae², Seung Min Woo^{1*}

¹Department of Nuclear Engineering, Kyung Hee University, 1732, Gyeonggi-do, 17104, Republic of Korea

²KEPCO Nuclear Fuel Co. Ltd., Republic of Korea

*Corresponding author : woosm@khu.ac.kr

INTRODUCTION

- i-SMR use relatively high gadolinium loading to control excess reactivity without relying on soluble boron.
- Because Gd-155 and Gd-157 absorption cross-sections are highly spectrum-dependent, temperature-driven coolant density changes can produce non-uniform depletion of these isotopes.
- Therefore, this study investigates the axial depletion behavior of Gd-155 and Gd-157, focusing on segment-wise burnout to clarify how the axial moderation profile affects local burnable absorber depletion.

METHODOLOGY

◆ i-SMR(innovative Small Modular Reactor)

- ✓ Core, Steam Generator, Pressurizer, and Primary Coolant System are integrated into a single Pressure Vessel.
- ✓ Compact core geometry and strong thermal hydraulic coupling in i-SMR results in axial and radial variations in neutron moderation and spectrum.
- ✓ Compared to large pressurized water reactors, i-SMR typically operates with shorter fuel assemblies and lower coolant flow rates, leading to relatively steep axial coolant temperature gradients.
- ✓ Gadolinium-bearing fuel is used in i-SMRs to control excess reactivity and improve power distribution, but the depletion of Gd-155 and Gd-157 is highly sensitive to local neutron spectrum and moderation conditions.

◆ Core Modeling

- ✓ 69 fuel assemblies categorized into four distinct types (A01, A02, A04, and A05).
- ✓ Non-control rod condition.
- ✓ Active core height of 240 cm discretized into 24 axial nodes at 10 cm intervals.
- ✓ Lower 210 cm consists of Gd₂O₃-UO₂ fuel, while the upper 30 cm consists of lower-enriched UO₂ fuel.

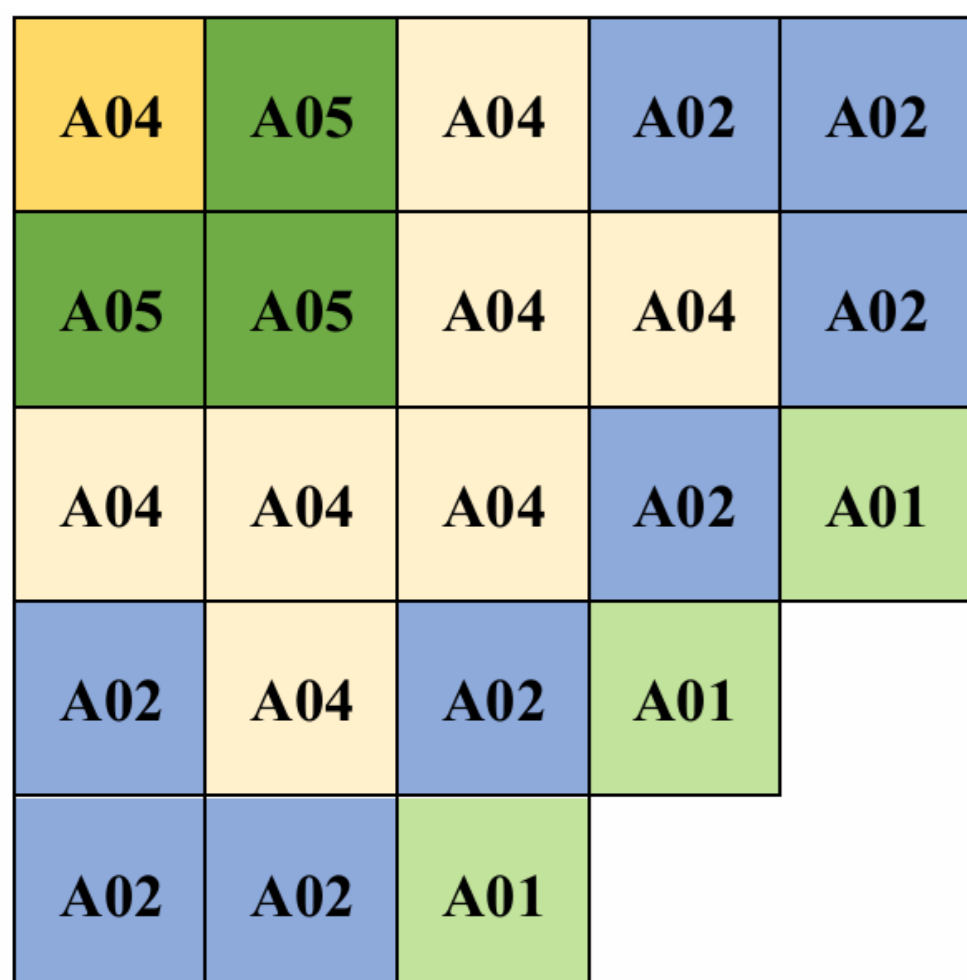


Fig. 1. i-SMR Radial Quarter-Core Loading Pattern

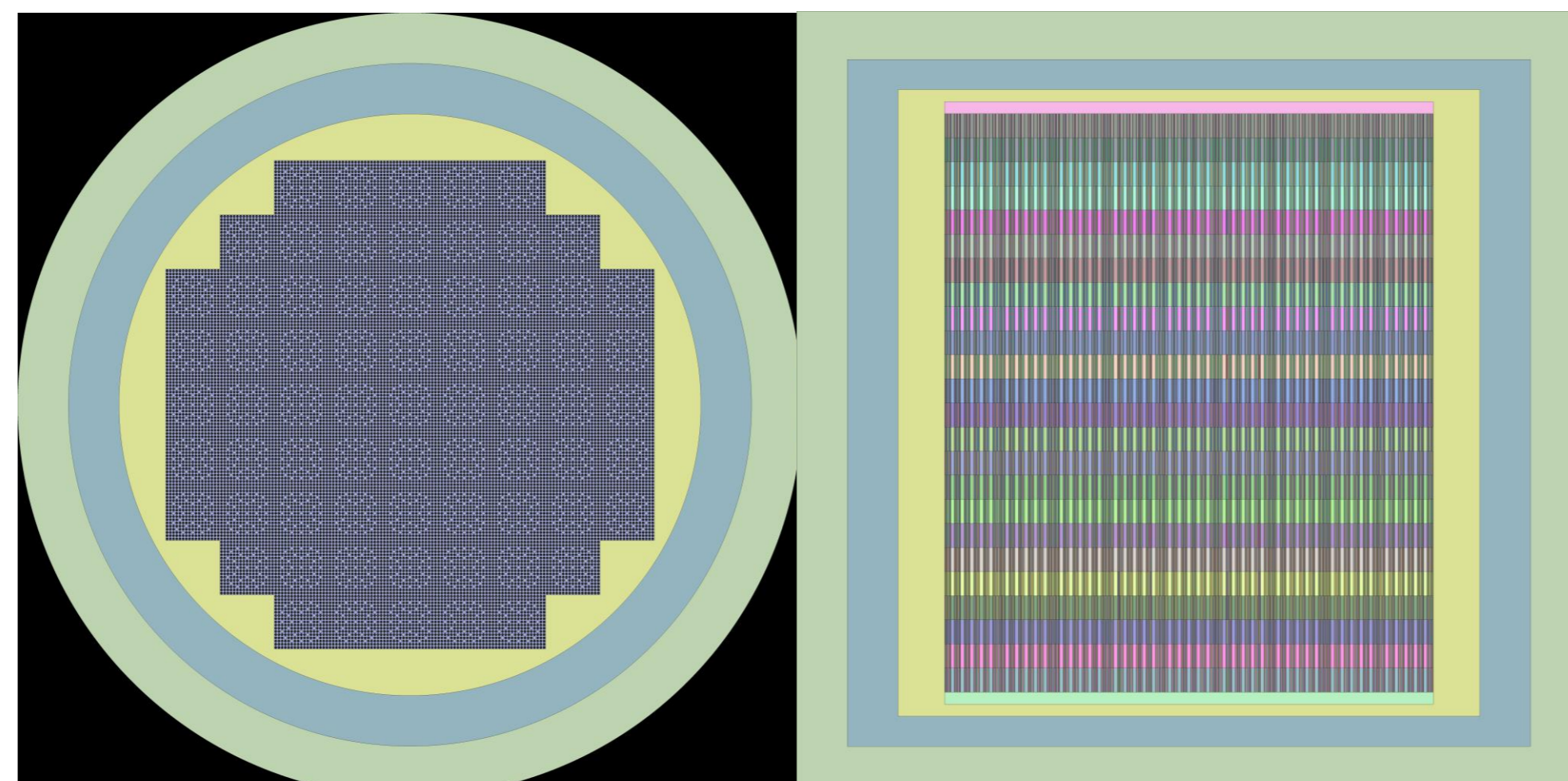


Fig. 2. i-SMR Core Radial and Axial View

◆ Coolant Temperature Distribution

- ✓ Linear axial temperature gradient.
- ✓ Temperature rise (ΔT) of 35 K was applied between the core inlet (lower core) and outlet (upper core).
- ✓ 35 K change induces a continuous decrease in coolant density toward the upper regions.
- ✓ Density 0.753g/cm³ to 0.675g/cm³.

Core Height (cm)	Coolant Temperature (K)
0-10 (1 st floor)	559.88
10-20 (2 nd floor)	561.34
20-30 (3 rd floor)	562.80
30-40 (4 th floor)	564.25
40-50 (5 th floor)	565.71
50-60 (6 th floor)	567.17
60-70 (7 th floor)	568.63
70-80 (8 th floor)	570.09
80-90 (9 th floor)	571.55
90-100 (10 th floor)	573.00
100-110 (11 th floor)	574.46
110-120 (12 th floor)	575.92
120-130 (13 th floor)	577.38
130-140 (14 th floor)	578.84
140-150 (15 th floor)	580.30
150-160 (16 th floor)	581.75
160-170 (17 th floor)	583.21
170-180 (18 th floor)	584.67
180-190 (19 th floor)	586.13
190-200 (20 th floor)	587.59
200-210 (21 st floor)	589.05
210-220 (22 nd floor)	590.50
220-230 (23 rd floor)	591.96
230-240 (24 th floor)	593.42

Table I. Assigned Coolant Temperature for each segment

ACKNOWLEDGMENT

- This work was supported by the Nuclear Safety Research Program through the Regulatory Research Management Agency for SMRs (RMAS) and the Nuclear Safety and Security Commission (NSSC) of the Republic of Korea (No. RS-2024-00509189).
- This work was supported by the Innovative Small Modular Reactor Development Agency grant funded by the Korea Government (MCEE) (No. RS-2024 00407975).

RESULT

◆ k_{eff}

- ✓ Code: Serpent 2
- ✓ Library: ENDF/B-VII.1
- ✓ Burnup: 2 years / 20 MWD/kgU
- ✓ Cycle: 5,000,000 nps / 100 active cycles / 40 inactive cycles
- ⇒ $k_{eff} < 10$ pcm

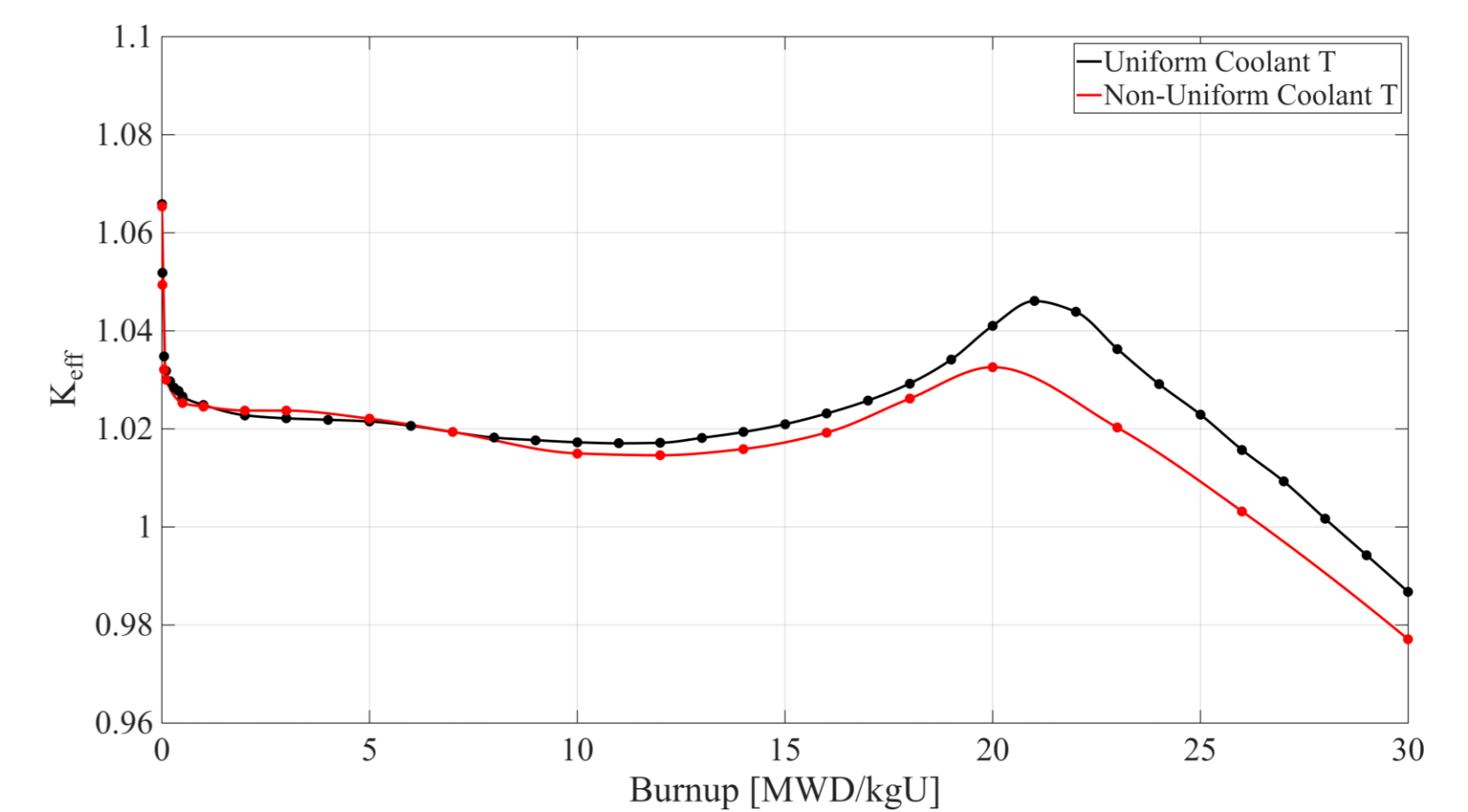


Fig. 3. k_{eff} change through depletion cycle

◆ Gadolinium Depletion

- ✓ The analysis was performed at the 1st, 5th, 9th, 13th, 17th, and 21st axial nodes corresponding to the Gd-containing fuel layers.

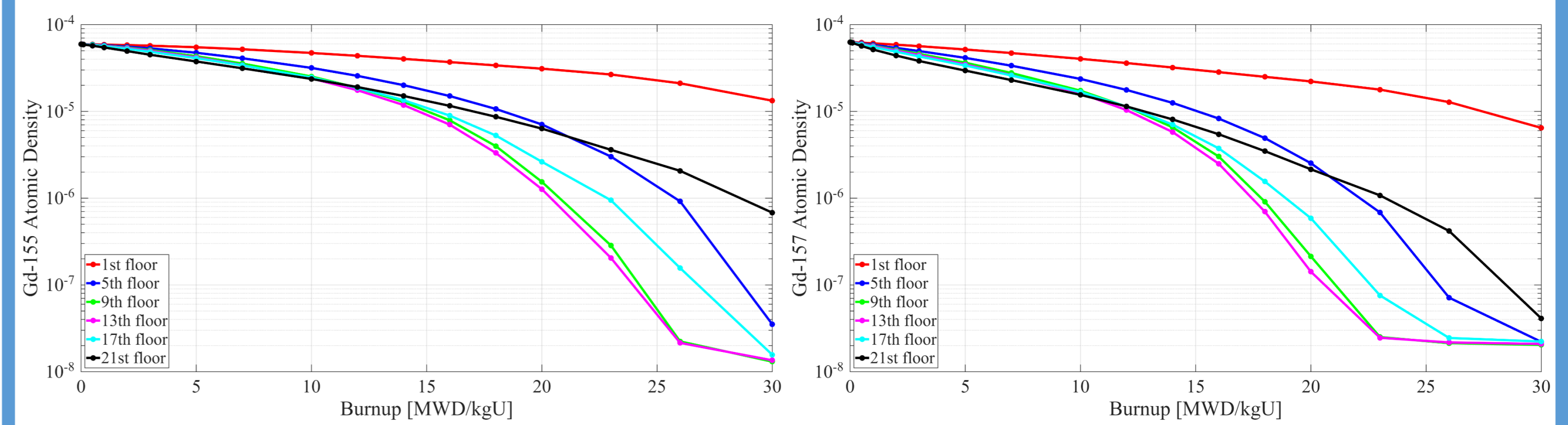


Fig. 4. Gd-155 Atomic Density changes through depletion cycle

Fig. 5. Gd-157 Atomic Density changes through depletion cycle

- ✓ To further examine this behavior, the changes in the overall gadolinium atomic density was conducted.

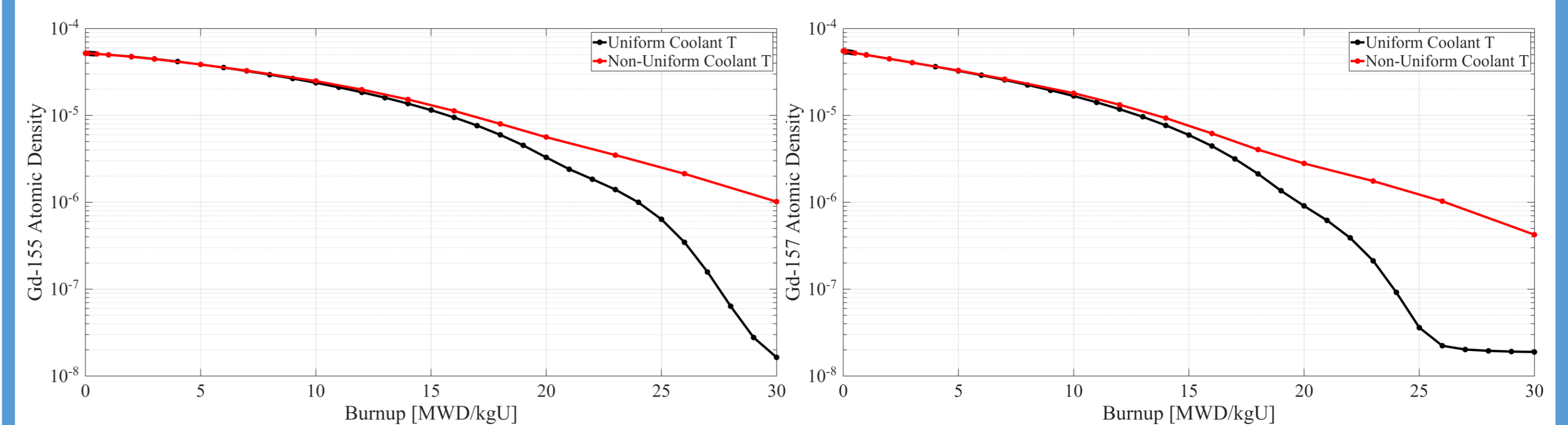


Fig. 6. Total Gd-155 Atomic Density changes through depletion cycle

Fig. 7. Total Gd-157 Atomic Density changes through depletion cycle

◆ Axial Power Distribution

- ✓ Non-uniform depletion ⇒ Axial power distribution change.
- ✓ BOC: Lack of gadolinium fuel ⇒ Tilted toward upper core.
- ✓ MOC: Restores the local reactivity ⇒ Cosine shape.
- ✓ EOC: Clearer cosine shape.

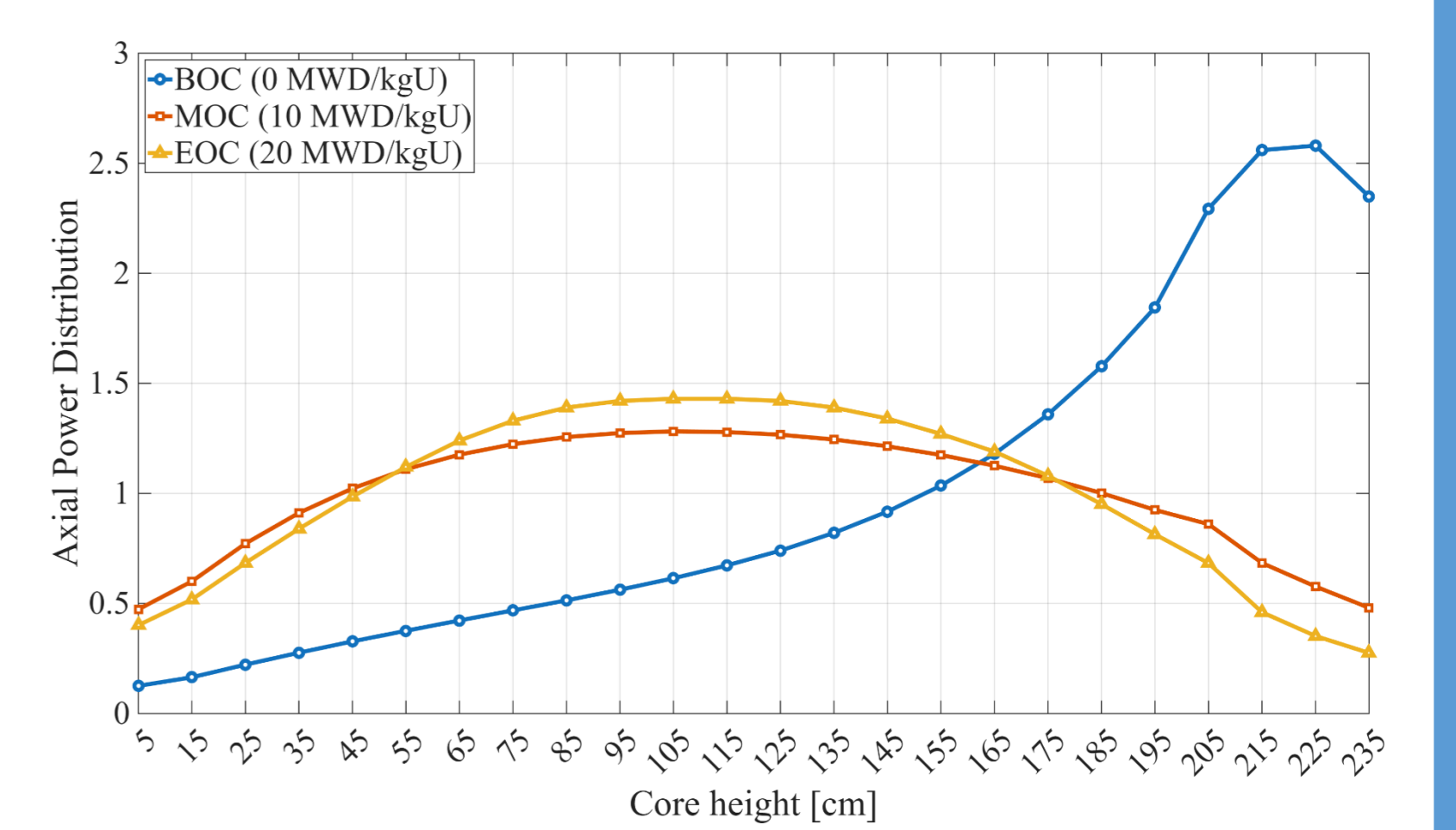


Fig. 8. BOC, MOC, EOC Axial Power Distribution

CONCLUSION

- Axial coolant temperature gradient significantly affects the depletion of Gd-155 and Gd-157.
- Compared with the uniform coolant temperature case, the non-uniform case showed lower overall gadolinium depletion, mainly because gadolinium in the lower axial region burned less.
- These findings highlight the need to consider axial thermal-hydraulic conditions, and future work will examine whether reversing the fuel rod orientation or modifying the axial gadolinium loading pattern can improve depletion balance.

REFERENCE

- [1] Kim, J., Jung, T., & Yoon, J. "Reactor core design with practical gadolinia burnable absorbers for soluble boron-free operation in the innovative SMR." Nuclear Engineering and Technology, 56(8), 3144–3154 (2024).
- [2] Duderstadt, J. J., & Hamilton, L. J. Nuclear Reactor Analysis. Wiley (1976).
- [3] Leppänen, J., et al. "The Serpent Monte Carlo code: Status, development and applications in 2013." Annals of Nuclear Energy, 82, 142–150 (2015).
- [4] Wei, X., Zhu, Y., Yang, S., Xu, D., Jin, X. Modeling of the Gadolinium Fuel Tests with the Jasmine Fuel Performance Code. In: Liu, J., Jiao, Y. (eds) Proceedings of the 2023 Water Reactor Fuel Performance Meeting. WRFPM 2023. Springer Proceedings in Physics, vol 299. Springer, Singapore. https://doi.org/10.1007/978-981-99-7157-2_35. (2024).