

Source Term Sensitivity Evaluation under SBO Induced Severe Core Damage Using MAAP-ISAAC in Wolsong Unit 2 Plants

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INTRODUCTION

The main objective of this paper is to evaluate a station blackout (SBO) accident resulting in hypothetical severe core damage using MAAP-ISAAC (Integrated Severe Accident Analysis code for CANDU plants), mainly about the fission product behavior, as ex-containment (= environmental release) source term evaluation for the R/B failure case.

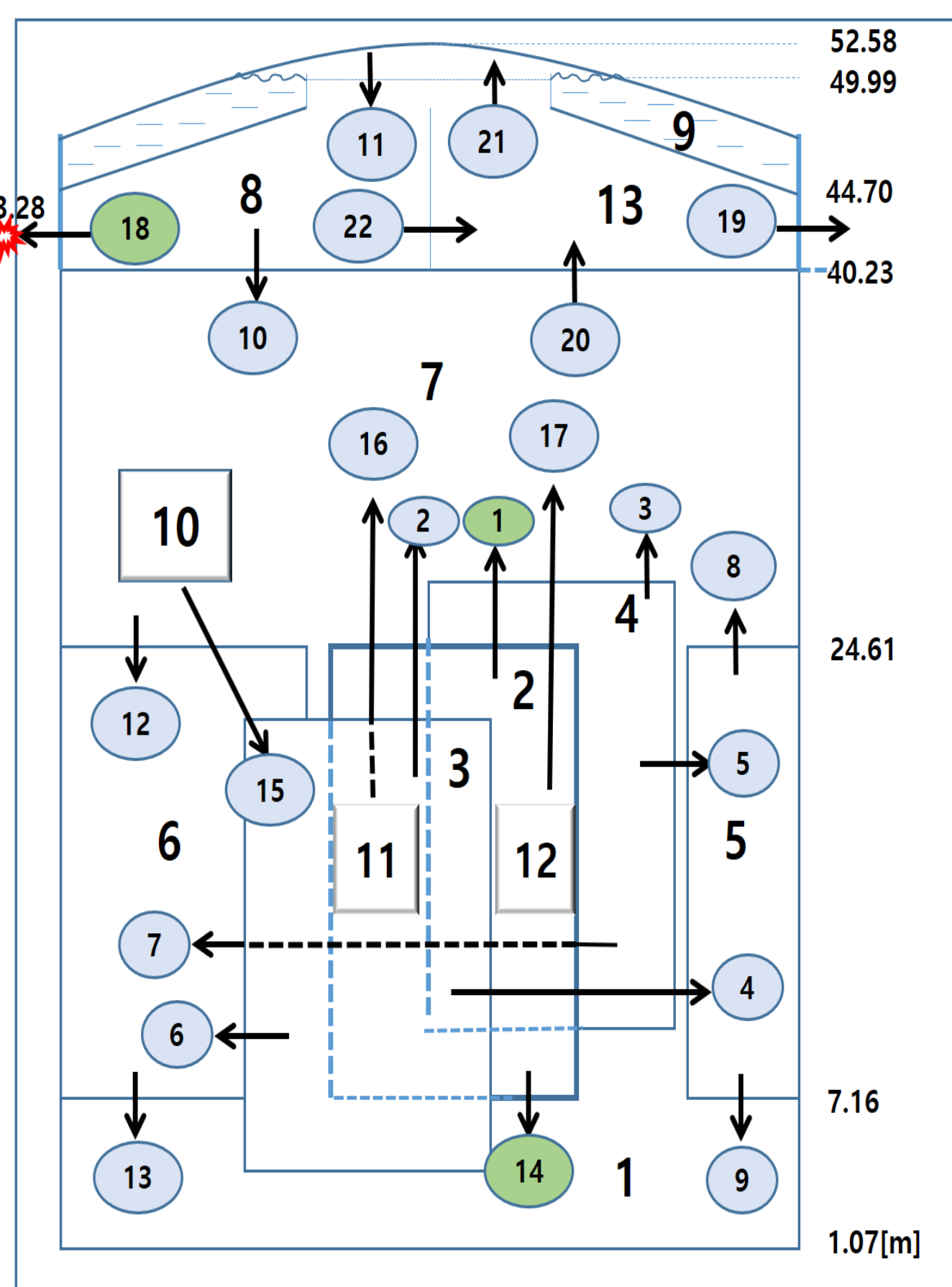
This work is done for providing code comparison basis with CAISER (CANDU Advanced Integrated SEVerRe) code [1] which is an up-to-date PHWR severe accident code developed and being improved at KAERI (Korea Atomic Energy Research Institute) following a demand for an accurate and detailed code in a CANDU society.

[1] KAERI (Jun Young Kang, Yong Mann Song, Dong Gun Son, Keun Sang Choi, Jong Yeob Jung, Jun Ho Bae, Byeonghee Lee), **Comparative Analysis of CANDU Severe Accident Using CAISER**, *Annals of Nuclear Energy*, Vol.227, February (2026), 11931

CANDU6 R/B Nodalization Scheme in ISAAC (with R/B rupture failure)

ISAAC Configuration for Reactor Building (R/B)

Node	Compartment
1	Basement
2	Reactor vault
3, 4	Fueling machine room
5	Moderator room
6	Access area
7	Boiler room
8, 13	Upper dome
9	Dousing tank
10	Degasser condenser tank
11, 12	End Shield



Status of Major Safety System in SBO

Cases	Rx Trip	PHTS loop Isolation	MFW or AFW	ECCS	MCS	ESC	R/B Failure	Comments
SBO-N	O	X	X	X	X	X	X	no AC power
SBO-Y	O	X	X	X	X	X	O	

SBO Main Event Progress in ISAAC4.03

Event Timing (4x4 checker: local balloon)	MAAPP-ISAAC [sec]	
	SBO-Y	SBO-N
SBO start	0	
Dousing spray operation	10,494~11,531 (Δt: ~1,000)	
(first) Channel (PT/CT) failure	14,029/21,758(Loop 1/2)	
100% fuel channel relocation	36,569	
Moderator dryout / Corium debris melt	40,054 / 48,313	
RV water saturation /	58,720 /	
RV water dryout	162,057	166,690
R/B rupture failure	81,025	N/A
CV creep failure	148,559	157,163
RV floor MCCI start	171,307	175,730
RV floor peak ablation rate	224,542	224,736
Zr 100% oxidation	232,822	240,591
RV BMT failure	39,6386	425,736
Calculation end	500,000	

CONCLUSIONS

- In intact R/B scenario (SBO-N), the tiny radiation leakage is calculated from the R/B (= containment) design leakage which is a background/basis leakage (= 0.01% (3.6g) of Cs initial inventory until 500,000 seconds). This is approximately 2% compared to the case of R/B rupture failure (SBO-Y).
- In failed R/B scenario (SBO-Y), when R/B failure occurs at approximately 81,000 seconds (~1 day), in-core FPs released to the R/B atmosphere (almost of aerosol form) are mostly deposited. Nevertheless both the suspended aerosols (left in the atmosphere (=0.144%)) and the resuspended aerosols (which are agitated from the deposited by pressure difference) have chances to become ex-containment ST. At approximately 200,000 seconds (~2.3 days when CV already failed and MCCI has started), the cumulative ex-containment ST becomes saturated at 0.537% (= 165g) for Cs elements. This is about 5 times (using 93.5% conversion factor of Cs into Cs-137) higher than the domestic AMP standard (= 100 TBq of Cs-137).
- The release fraction order among 12 FP groups (including Cs and I) in ISAAC code is as follows.

✓ Noble>CsOH/CsI>Sb>TeO₂>Te₂>MoO₂>SrO>BaO>CeO₂>La₂O₃>UO₂

ISAAC Fission Product Models

The ISAAC model employs temperature dependent vapor pressure correlations and the ideal gas law to calculate the driving force for a condensation or an evaporation

Aerosol formation from the supersaturated vapor allows us to calculate the vapor diffusion rate to the walls; if the mass of the vapor is supersaturated in a time step, the excess mass is assumed to form aerosols

Vapor deposition removal rate is

$$\lambda = D_f \frac{Sh}{h_c}$$

Diffusion coefficient near the heat sinks is

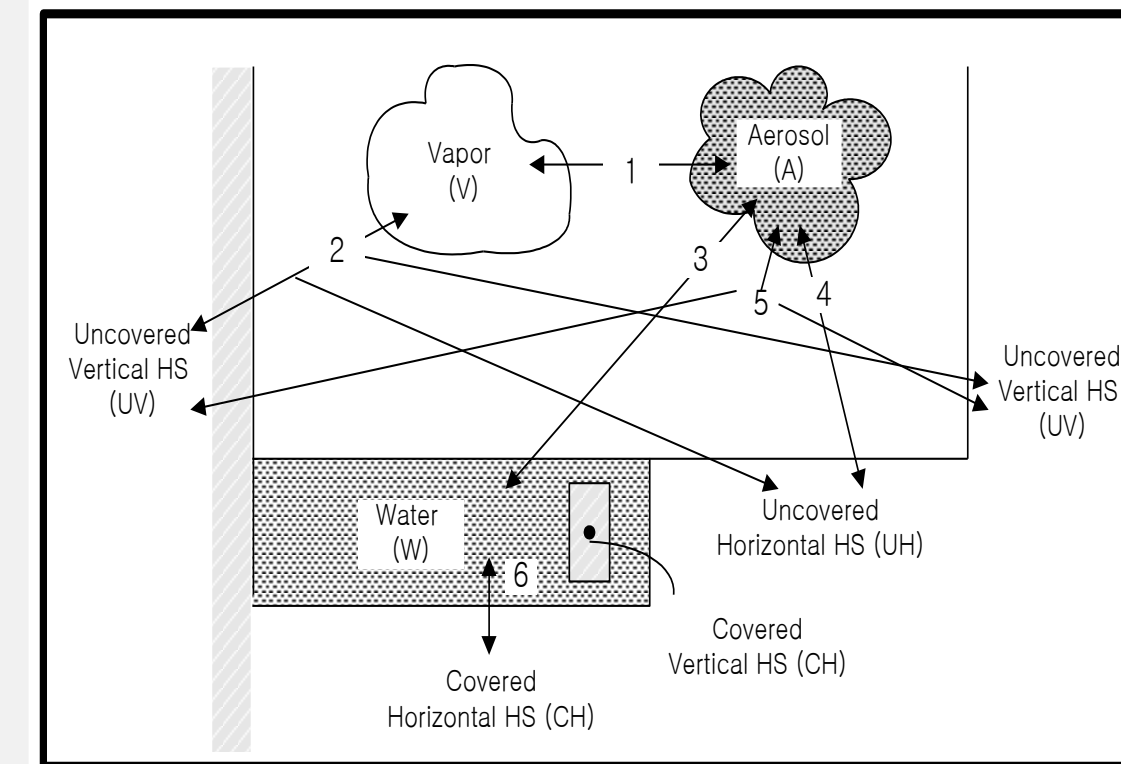
$$D_f = 4.7 \cdot 10^{-3} \tau_m^{1.5} / \left[10 \cdot P_{gas} \left(1 + 829 / T_m \right) \right]$$

Where,

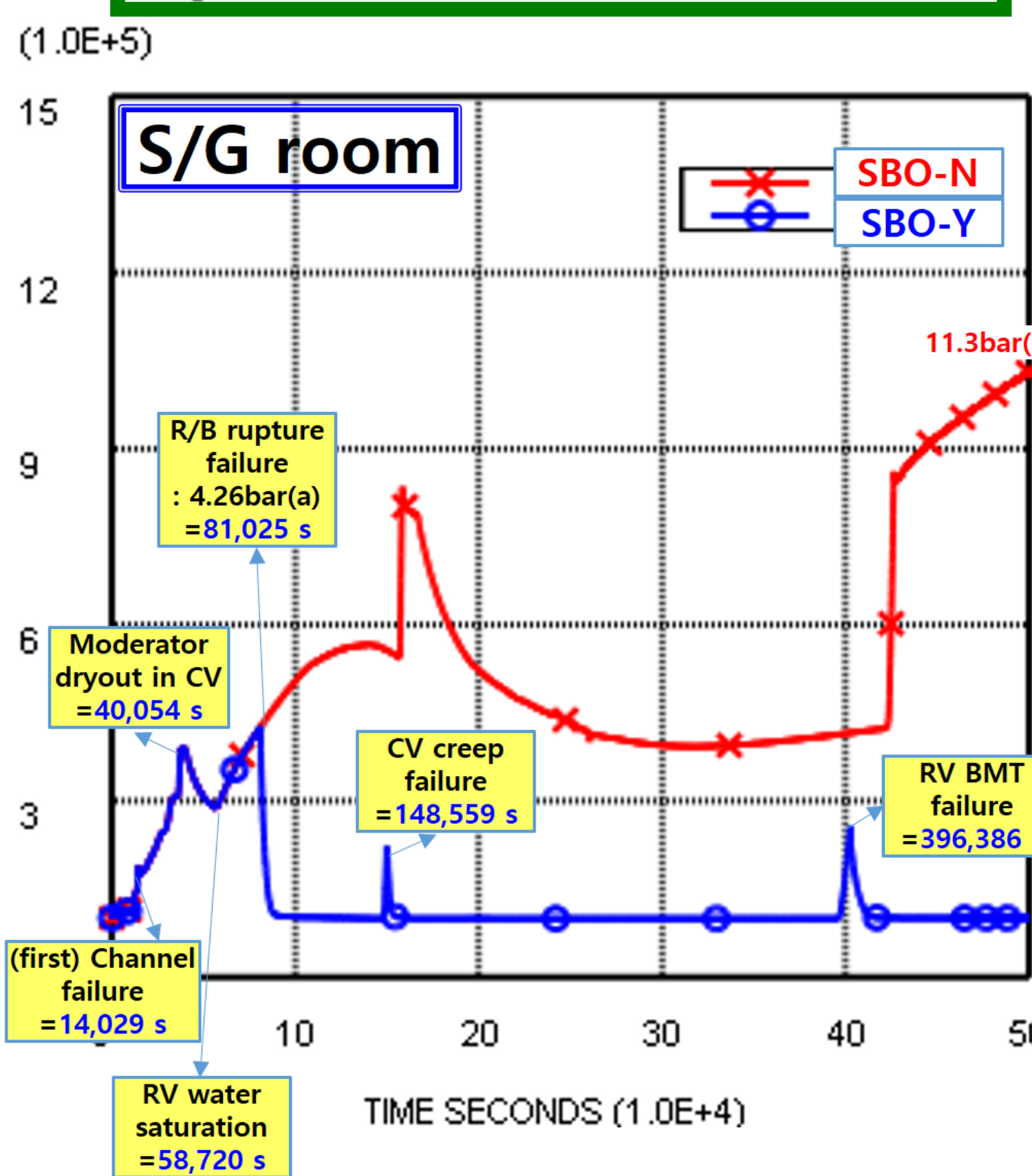
Sh = Sherwood number

h_c = Characteristic length of condensation

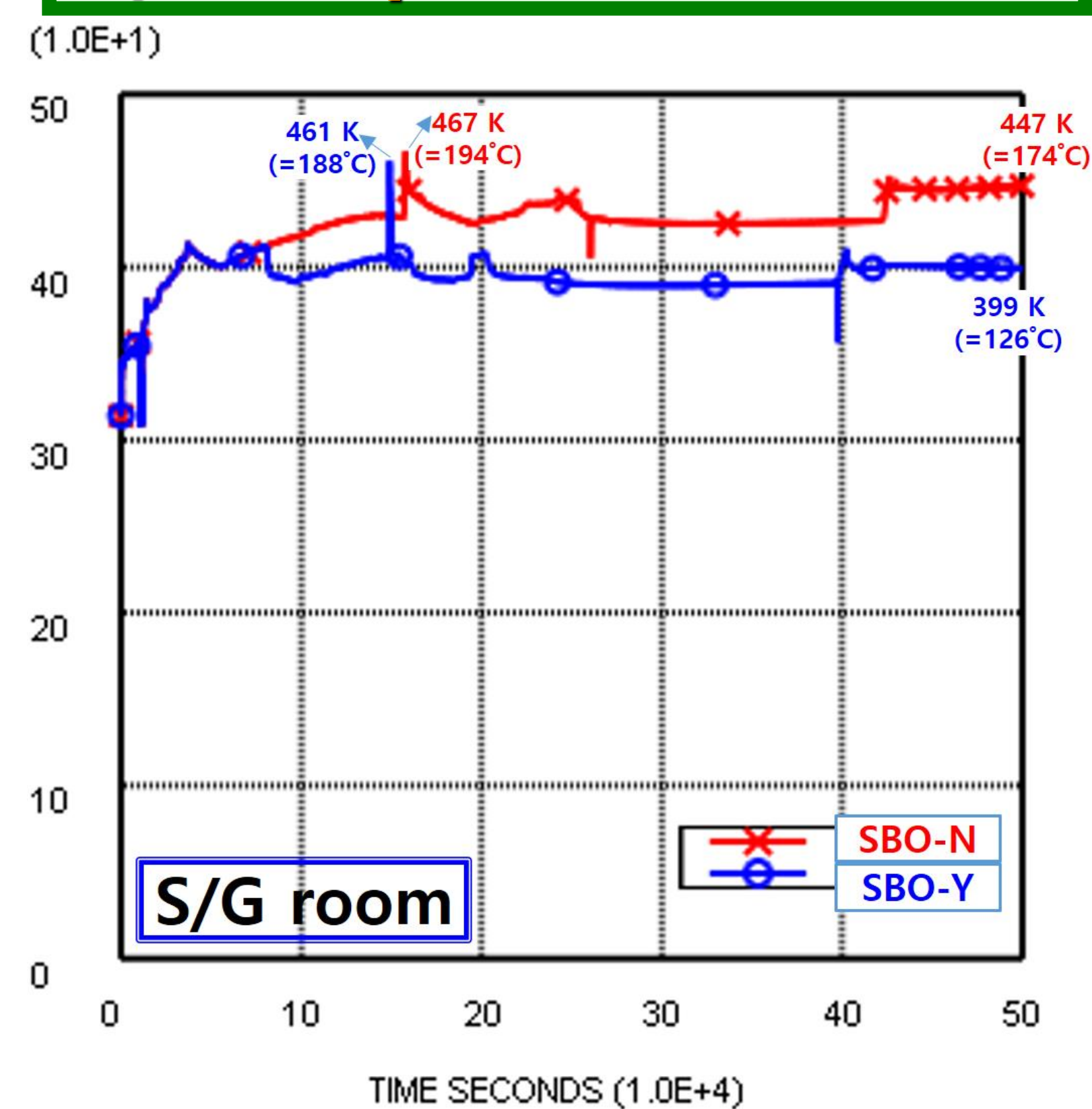
P_{gas} = Gas pressure, T_m = 0.5 (T_g + T_{WALL})



R/B Pressure Prediction

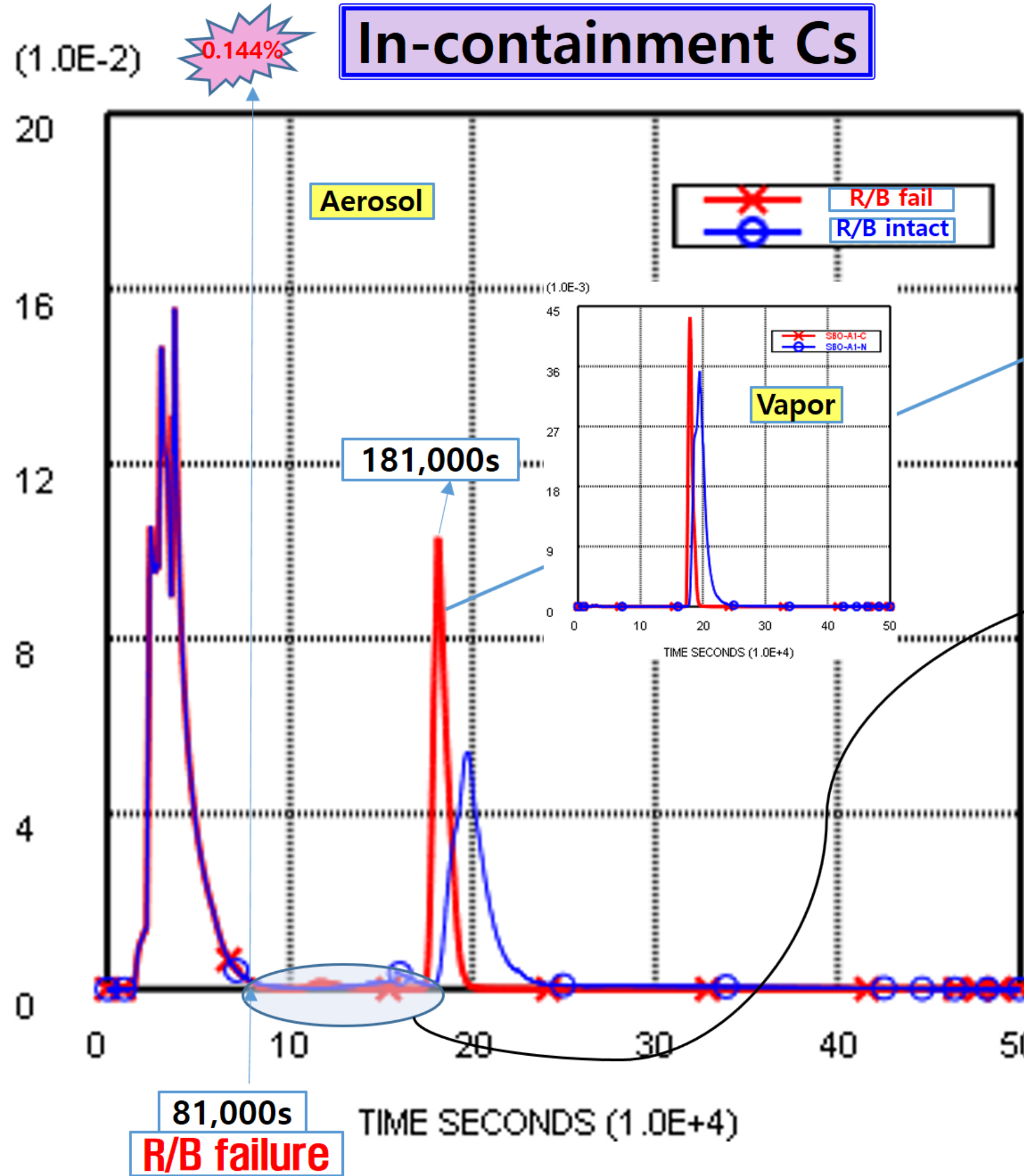


R/B Temperature Prediction



In-/Out-Containment Source Term Evaluation for Cs

In-containment Cs



Ex-containment Cs

