

Effect of Insulation Material on Boil-off Gas in Cryogenic Tank for LAES coupled with SMR

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LAES coupled with SMR



Fig. 1. Energy shift

- Increase in renewable generation \rightarrow need for flexible operation of SMR
- Suggest LAES coupled with SMR
 - \rightarrow Improve load following by connecting with LAES
- LAES(Liquid air energy storage system) is a large-scale energy storage system
- LAES stores energy by liquefying air with surplus power

 \rightarrow high energy density, low geographical constraints, eco-friendly

working fluid, and long service time



Fig. 2. layout of LAES

LAES coupled with SMR





- LAES and the nuclear steam cycle can be coupled mechanically by using a Steam Turbine driven-compressor (STDC)
- The STDC is used to compress air for the LAES charging cycle.
 → liquid air is produced for energy storage

Fig. 3. Schematic diagram of nuclear integrated LAES

LAES coupled with SMR

- LAES Charging during off-peak, discharging for extra power.
 - \rightarrow (liquid form) high energy density, reducing thermal fluid volume
 - \rightarrow maintaining cryogenic temperature for sufficient time in the liquid air tank is

essential to achieve good round-trip efficiency of the LAES



Cryogenic fluid in the tank

• In cryogenic engineering, BOG (Boil-Off Gas) occurs because of heat transfer from the surrounding environment, causing LNG to warm up and turn into gas.

 \rightarrow potentially raising the tank's pressure

 \checkmark "Need for a study on time-dependent BOG variations in liquid air tanks.



Fig. 4. Property and composition changes in the interior design of LNG tank



Thermal analysis model for a Liquid air tank

- Partial Equilibrium Model(PEM) to model the storage tank
- Evaporation rate, inner pressure
 - \rightarrow affected by heat ingress
 - \rightarrow conduction, convection, and conjugate heat transfer





Thermo-modeling for a Liquid air tank

- PEM (Partial Equilibrium Model)
- Mass balance

$$\frac{dm_L}{dt} = \dot{m}_c - \dot{m}_e, \frac{dm_v}{dt} = \dot{m}_e - \dot{m}_c - \dot{m}_{BOG}$$

 m_L : liquid mass, m_v : vapor mass, \dot{m}_c : condensation rate \dot{m}_e : evaporation rate, \dot{m}_{BOG} : boil – of f gas

• Energy balance

$$\frac{dU_L}{dt} = \dot{Q}_{liq} + \dot{Q}_{bottom} + \dot{Q}_{v-l} + (-\dot{m}_e + \dot{m}_c)h_{fg}$$

$$\frac{dU_v}{dt} = \dot{Q}_{vap} + \dot{Q}_{top} - \dot{Q}_{v-l} + (\dot{m}_e - \dot{m}_c)h_{fg} - \dot{m}_{BOG}h_g$$

$$\dot{Q}_L: heat \ transfer \ to \ liquid, \dot{Q}_v: heat \ transfer \ to \ vapor$$

$$\dot{Q}_{v-l}: heat \ transfer \ from \ vapor \ to \ liquid, U: internal \ energy$$

• Boil-off gas (BOG) rate

$$\dot{m}_{BOG} = \frac{m_v - m_{real}}{dt} + \dot{m}_e - \dot{m}_c$$

$$m_{real} = m_v + (\dot{m}_e - \dot{m}_c - \dot{m}_{BOG})dt$$

$$m_{real} = V_v * \rho_{v-target}$$

$$\rho_{v-target} = f(P_{relief}, T_v), P_{relief}: relief \ pressure$$





Thermal insulation for a liquid air tank



Fig.10 Schematic of the thermal resistance cross-section inside the tank

Thermal insulation type

- Thermal insulation type
- 1. Foam insulation
- 2. Vacuum insulation
- Difference of cost & thermal conductivity
 → need thermal insulation ability comparison
- ✓ In this study, polyurethane foam and vacuum insulation (P=0.01 Pa) were analyzed.





(d)

Fig. 11 (a) polyurethane foam (b) foam spray (c) Liquid gas tank insulated vacuum (d) schematic diagram of vacuum insulation tank

Thermal resistance for insulation material

• Heat transfer type : conduction, convection and radiation

 \rightarrow Apply Thermal resistance model to the top, bottom and wall of the tank



Fig.12 Schematic of the thermal resistance cross-section inside the tank with foam insulation



Conduction

Fig.13 Schematic of the thermal resistance cross-section inside the tank inside the tank

$$R_{total} = R_{conduction} + R_{radiation} + R_{convection}$$

Design for a Liquid air tank

- Tank pressure rises due to BOG
 - \rightarrow vented by the relief value
 - \rightarrow maintain the inner pressure of the tank
- Insulation thickness is designed using scaling method and fixed the value as 0.04m
 - \rightarrow to observe the effect of the insulation
 - material on the BOG of the cryogenic tank

Table.1 Design parameters for tank modeling

parameters		
Height	9.0	m
Diameter	3.0	m
Side thickness	0.005	m
Top thickness	0.005	m
Insulation thickness	0.04	m

Thermal conductivity			
Foam	0.0285	W/m-K	
Vacuum	0.003	W/m-K	

- Assumptions used for the modeling
- The Partial Equilibrium model (PEM) is used for liquid and vapor in the cryogenic tank.
- The heat flux is calculated for top, bottom, and wall sections of the tank due to the different thermal properties at different location.
- 3) The total duration of analysis is 10 hours.
- The temperature of the insulation is determined by thermal conductivity, and the temperature distribution within the insulation is not considered.
- 5) The BOG is assumed to be vented to maintain pressure at 108 kPa.



Results

- BOG rates for foam and high vacuum insulation.
- Pressure converges to target pressure of $108 \text{ kPa} \rightarrow BOG$ rate converges to a certain value.
- 10 times difference in thermal conductivity
 - \rightarrow foam insulation (k = 0.0285) reaches 1.23%/hr converged BOG rate
 - \rightarrow vacuum insulation (k = 0.003) reaches 0.61%/hr converged BOG rate
- Non-linear relationship between thermal conductivity and converged BOG rate.

 \rightarrow The choice of insulation material is crucial for BOG rate control.



Fig. 14 Boil-off gas rate of cryogenic tank insulated (a) foam and (b) high vacuum

Fig. 15 Boil-off gas rate of the cryogenic tank and thermal conductivity insulated foam

Geometry design for Liquid air tank

• Insulation of the cryogenic tank is important for the tank design and how long the liquid air tank can hold liquid air for storing energy

 \rightarrow Tank geometry is also crucial indicator for modeling



• Aspect ratio

$$AR = \frac{H}{D}$$

 \rightarrow Variation of aspect ratio influences Nusselt number

• Vapor-liquid heat transfer

$$\dot{Q}_{\nu-l} = h_{\nu-l}A(T_{\nu ap} - T_{liq})$$

$$\frac{1}{h_{\nu-l}} = \frac{1}{h_{\nu ap}} + \frac{1}{h_{liq}}$$

$$Nu_{\nu ap} = 0.54Ra^{0.25}$$

$$Nu_{liq} = 0.27Ra^{0.25}$$

$$Ra = Gr * Pr, Pr = \frac{\mu C_p}{k}, Gr = \frac{g\beta\Delta T D_{eq}^3}{a\nu}$$

Results

- Aspect ratio change
 - \rightarrow interface area change \rightarrow Nusselt number change
 - \rightarrow heat amount change \rightarrow BOG rate change
- Total heat ingress into the tank reaches its minimum when the aspect ratio is 1
 - \rightarrow BOG rate also reaches its minimum at an aspect ratio of 1
- Heat ingress to the top, bottom, and walls of the tank varies with changes in the aspect ratio



Fig. 17 Heat ingress and BOG rate of cryogenic tank for aspect ratio (*H/D*)



Summary

- Growing renewable energy \rightarrow SMR flexibility needed
- Propose coupling SMR with LAES → Enhance load-following via LAES connection
- LAES (Liquid Air Energy Storage) charges during off-peak, discharges during high demand.

 \rightarrow Liquid form = high energy density, reduced thermal fluid volume

 \rightarrow Maintaining cryogenic temps in tank is important for LAES efficiency

- In cryogenic engineering, BOG (Boil-Off Gas) is a critical issue due to rising tank pressure.
- BOG rates for foam vs high vacuum insulation

 \rightarrow Converge at 108 kPa target pressure

 \rightarrow Foam insulation, 1.23% converged BOG rate

- \rightarrow High vacuum insulation, 0.61% converged BOG rate
- \rightarrow Non-linear relation between thermal conductivity and BOG rate
- Aspect ratio variation \rightarrow interface area change \rightarrow Nusselt number change \rightarrow Heat amount change

 \rightarrow BOG rate change

- Minimum total heat ingress and BOG rate at aspect ratio 1
- Heat ingress to tank top, bottom, and walls varies with aspect ratio changes



Thank you

The Secret to success is to never give up -

