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# Evaluation of Depletion Uncertainty for Spent Fuel Storage Pool using Monte Carlo Random Sampling by Considering Boron Concentration in Depletion Calculation

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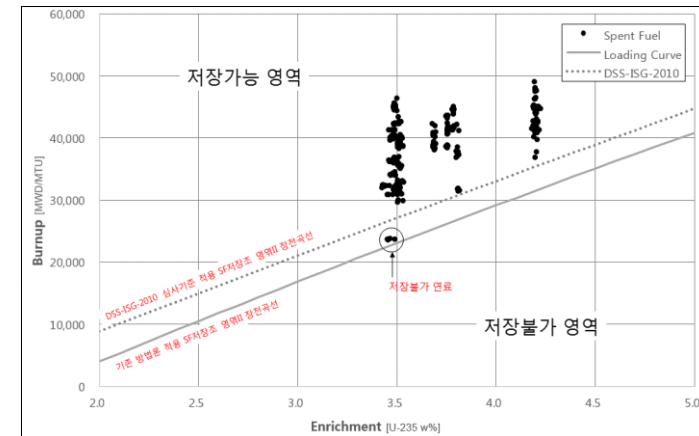
- 1) Isotopic inventory estimation of SNFs
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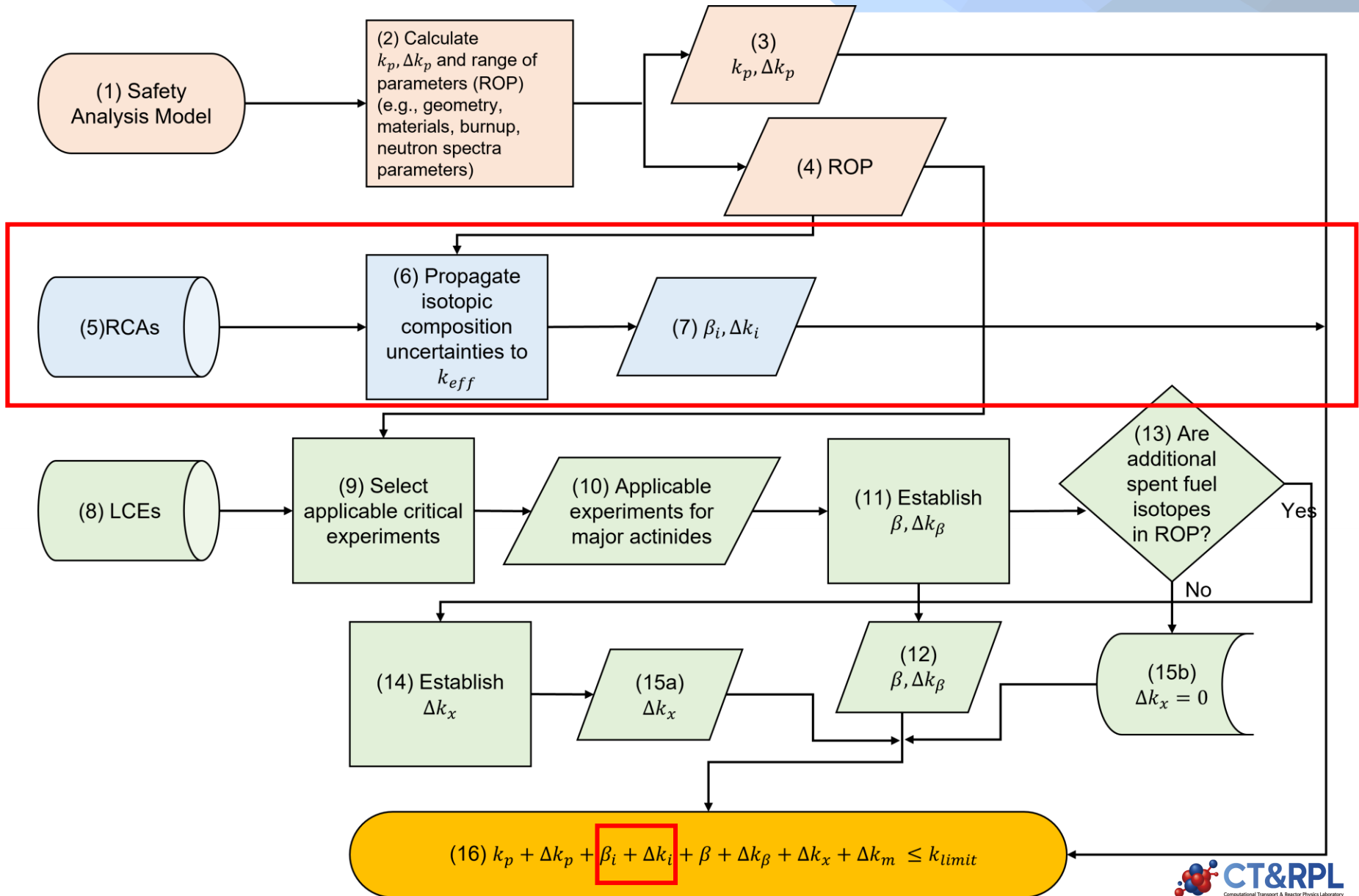
## □ Revised standard review plan by U.S. NRC (DSS-ISG-2010-01)

- The U.S. NRC requires the application of revised guidance for spent fuel pool nuclear criticality analyses and operations from 2011.
- Domestic regulatory body requires application of the revised guidance of the U.S. NRC from 2015.
- The  $k_{\text{eff}}$ , including all biases and uncertainties at a 95% confidence level, should not exceed 0.95 under all credible normal, off-normal, and accident conditions for all storage operations.

	DSS-ISG-2010-01	Current state in our country	Safety Margin
Boron credit	Yes	No	Up
Axial burnup profile	NUREG/C R-6801	Uniform profile	Down
Code validation – $k_{\text{eff}}$	NUREG/C R-6698	Yes	Down
Code validation – Isotopic depletion	NUREG/C R-7108	No or excessive conservatism	Down

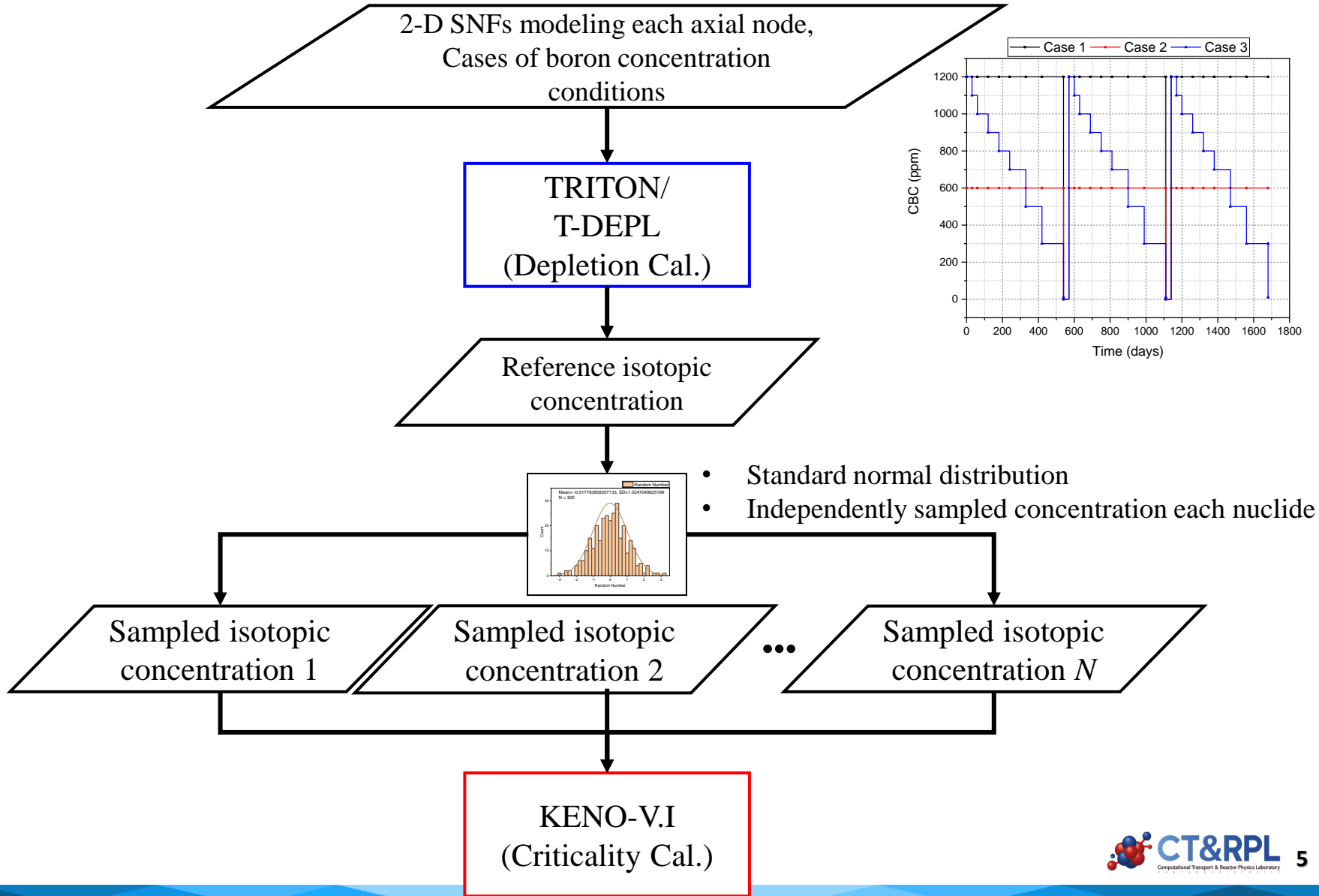


## Overview of the burnup credit validation process



# Methods and Results

- Workflow of the evaluation of depletion uncertainty by considering boron concentration



## □ Computer code system

### SCALE6.2.4/TRITON

- Neutron transport, depletion calculation, estimation of inventory
- ENDF/B-VII.1 based 252-group neutron cross section library
- 17×17 (17V5H) fuel assembly 2D modeling
- Axial burnup profile for each 18 nodes

### SCALE6.2.4/KENO-VI

- Monte Carlo criticality transport calculation
- The region II spent fuel pool 3D modeling
- Criticality calculations with the sampled nuclide concentration sets

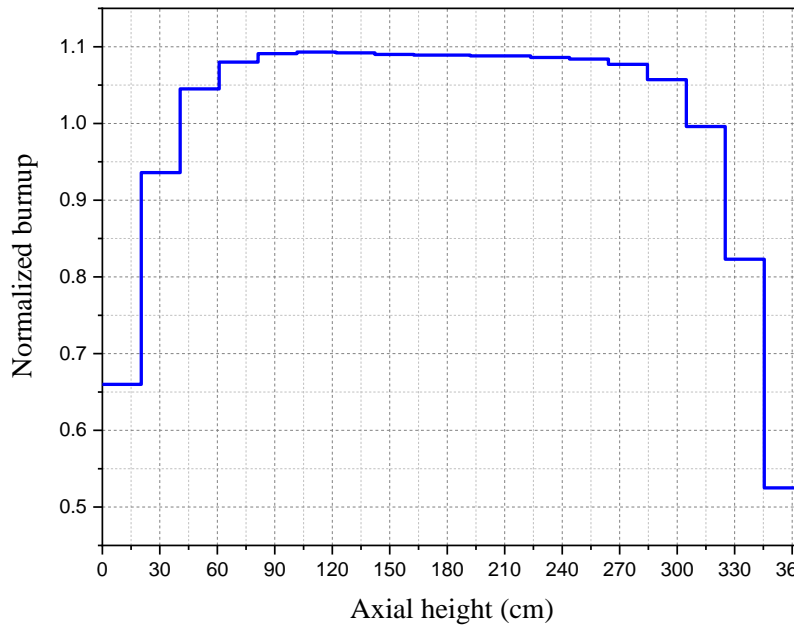
#### Major Actinides (9)

$^{234}\text{U}$   $^{235}\text{U}$   $^{238}\text{U}$   $^{238}\text{Pu}$   $^{239}\text{Pu}$   $^{240}\text{Pu}$   $^{241}\text{Pu}$   $^{242}\text{Pu}$   $^{241}\text{Am}$

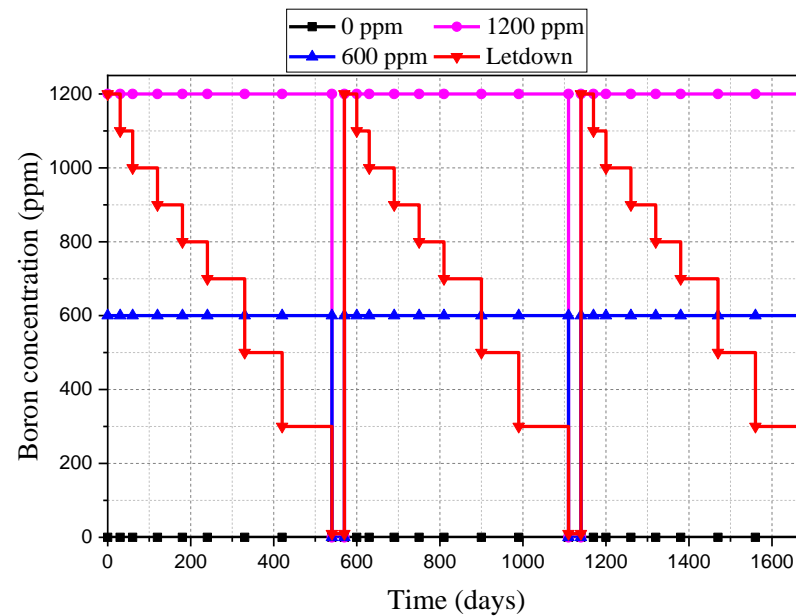
#### Fission Products (19)

$^{95}\text{Mo}$   $^{99}\text{Tc}$   $^{101}\text{Ru}$   $^{103}\text{Rh}$   $^{109}\text{Ag}$   $^{133}\text{Cs}$   $^{147}\text{Sm}$   $^{149}\text{Sm}$   $^{150}\text{Sm}$   $^{151}\text{Sm}$   
 $^{152}\text{Sm}$   $^{143}\text{Nd}$   $^{145}\text{Nd}$   $^{151}\text{Eu}$   $^{153}\text{Eu}$   $^{155}\text{Gd}$   $^{236}\text{U}$   $^{243}\text{Am}$   $^{237}\text{Np}$

## □ Fuel assembly depletion modeling

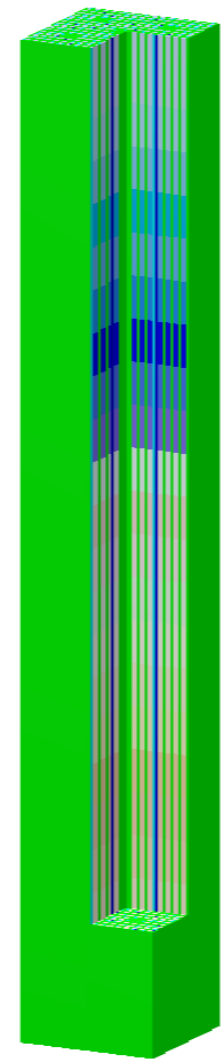


[Fig. Bounding axial burnup profile\*]



[Fig. Boron concentration conditions]

[Table. Modeling parameters]

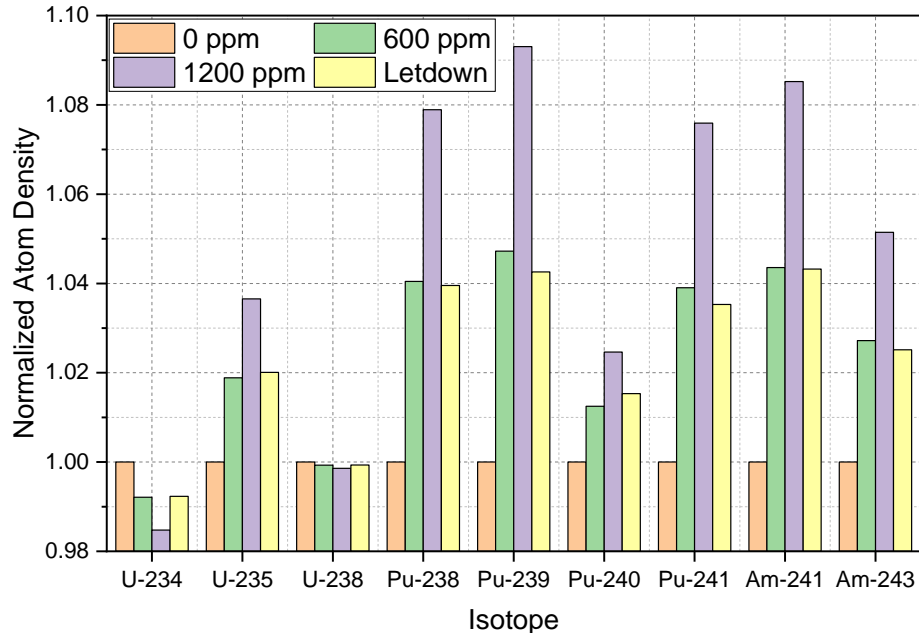


### Parameters

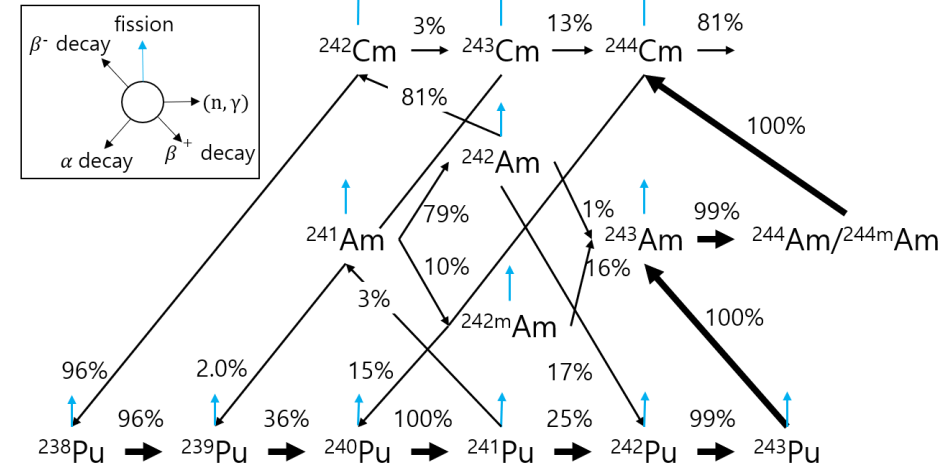
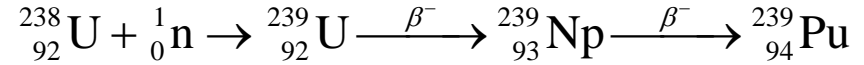
### Values

$^{235}\text{U}$ enrichment (wt%)	5.0
Burnup (MWd/kg)	40.0
Number of cycles	3
Cycle period (days)	540
Total cycle period (days)	1680
O/H period (days)	30

## Isotopic inventory estimation of SNFs



[Fig. Actinides inventory for different boron conditions]



[Fig. Predominant path up to 244Cm and transmutation ratio\*]

[Table. Comparison of keff for boron condition]

Boron condition (ppm)	Values	$\Delta\rho$ (pcm)
0	0.83620	-
600	0.84063	630
1200	0.84721	1554
Letdown	0.84054	671

- The SNFs depleted under high boron concentration conditions have a high fissile content.
- The result obtained with the *letdown* concentration is similar to that with 600 ppm.

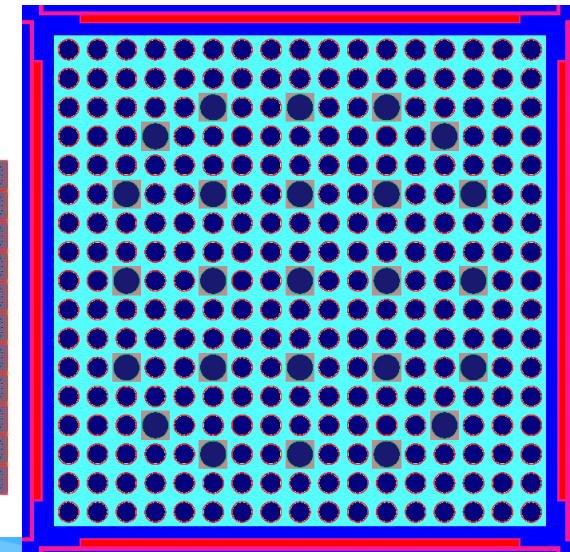
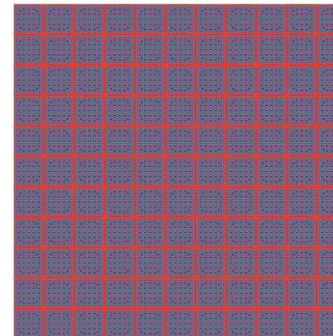
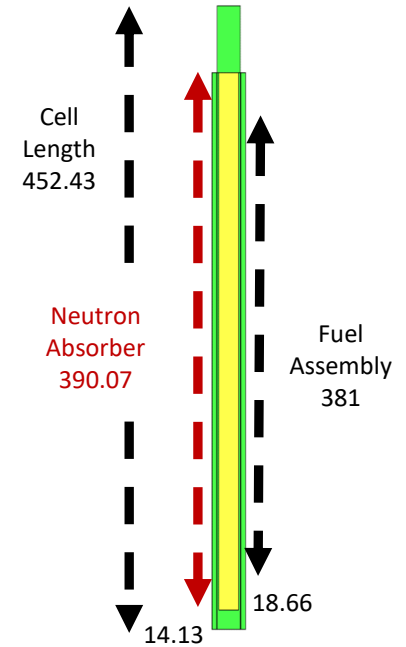
\* Akihiro SASAHARA, Tetsuo MATSUMURA, Giorgos NICOLAOU & Dimitri PAPAIOANNOU Neutron and Gamma Ray Source Evaluation of LWR High Burn-up UO<sub>2</sub> and MOX Spent Fuels, Journal of Nuclear Science and Technology, Vol 41, No. 4, pp. 448-456, 2004.



## Spent fuel storage rack (SF SR) model

[Table. Design parameters of the spent fuel storage rack region II]

Parameter	Value
Storage cell wall material	SS304
Storage cell inner dimension(cm)	21.511
Storage cell wall thickness(cm)	0.1905
Storage cell length(cm)	425.43
Neutron absorber material	Metamic
Neutron absorber width(cm)	18.36
Neutron absorber thickness(cm)	0.27
Neutron absorber length(cm)	390.07
Distance between neutron absorbers(cm)	14.13
Fuel assembly pitch(cm)	18.66



[Fig. Configuration of the spent fuel storage rack region II]

## □ Calculation of Bias and Bias Uncertainty in Calculated Nuclide Concentrations

- The measured-to-calculated nuclide concentration ratio,  $X_n^j$  (M/C ratio)

$$X_n^j = M_n^j / C_n^j$$

- Sample mean  $\overline{X}_n$ , and sample standard deviation  $s_n$

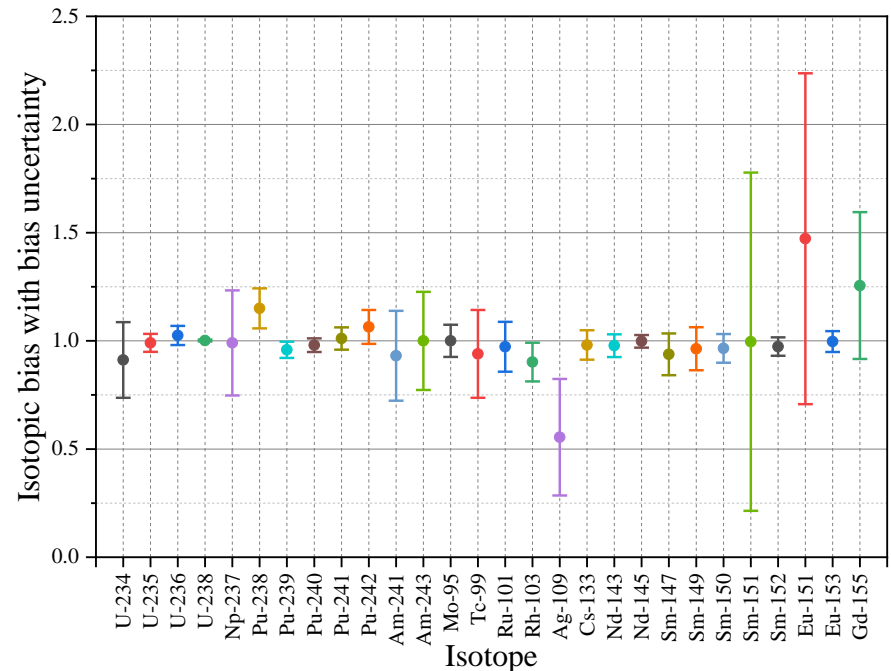
$$\overline{X}_n = \sum_{j=1}^{N_n} X_n^j / N_n \quad \text{Bias}$$

$$s_n = \sqrt{\sum_{j=1}^{N_n} (X_n^j - \overline{X}_n)^2 / (N_n - 1)}$$

- The isotopic bias uncertainty  $\sigma_n$

$$\sigma_n = \begin{cases} s_n \cdot tf_2^n, & N_n \geq 10 \\ s_n \cdot tf_1^n, & N_n < 10 \end{cases} \quad \text{Uncertainty}$$

$tf_2^n$  The two-sided tolerance limit factor



[Fig. Isotopic bias and bias uncertainty values for PWR SNF compositions\*]

\*Georgeta Radulescu, Ian C. Gauld, Germina Ilas & John C. Wagner (2014) Approach for Validating Actinide and Fission Product Compositions for Burnup Credit Criticality Safety Analyses, Nuclear Technology, 188:2, 154-171, DOI: [10.13182/NT13-154](https://doi.org/10.13182/NT13-154)

## □ Nuclide Concentration for $k_{eff}$ Calculations

- Nuclide concentration random sampling

$$C_{n,b}^k = \begin{cases} C_{n,b}(\overline{X}_n^b + \sigma_n^b \cdot R_n^k |_{normal\ dis.}), & N_n \geq 10 \\ C_{n,b}(\overline{X}_n^b + \sigma_n^b \cdot R_n^k |_{uniform\ dis.}), & N_n < 10 \end{cases}$$

- $k_{eff}$  mean  $\bar{k}_{eff}$ , and  $k_{eff}$  standard deviation  $\sigma_{k_{eff}}$

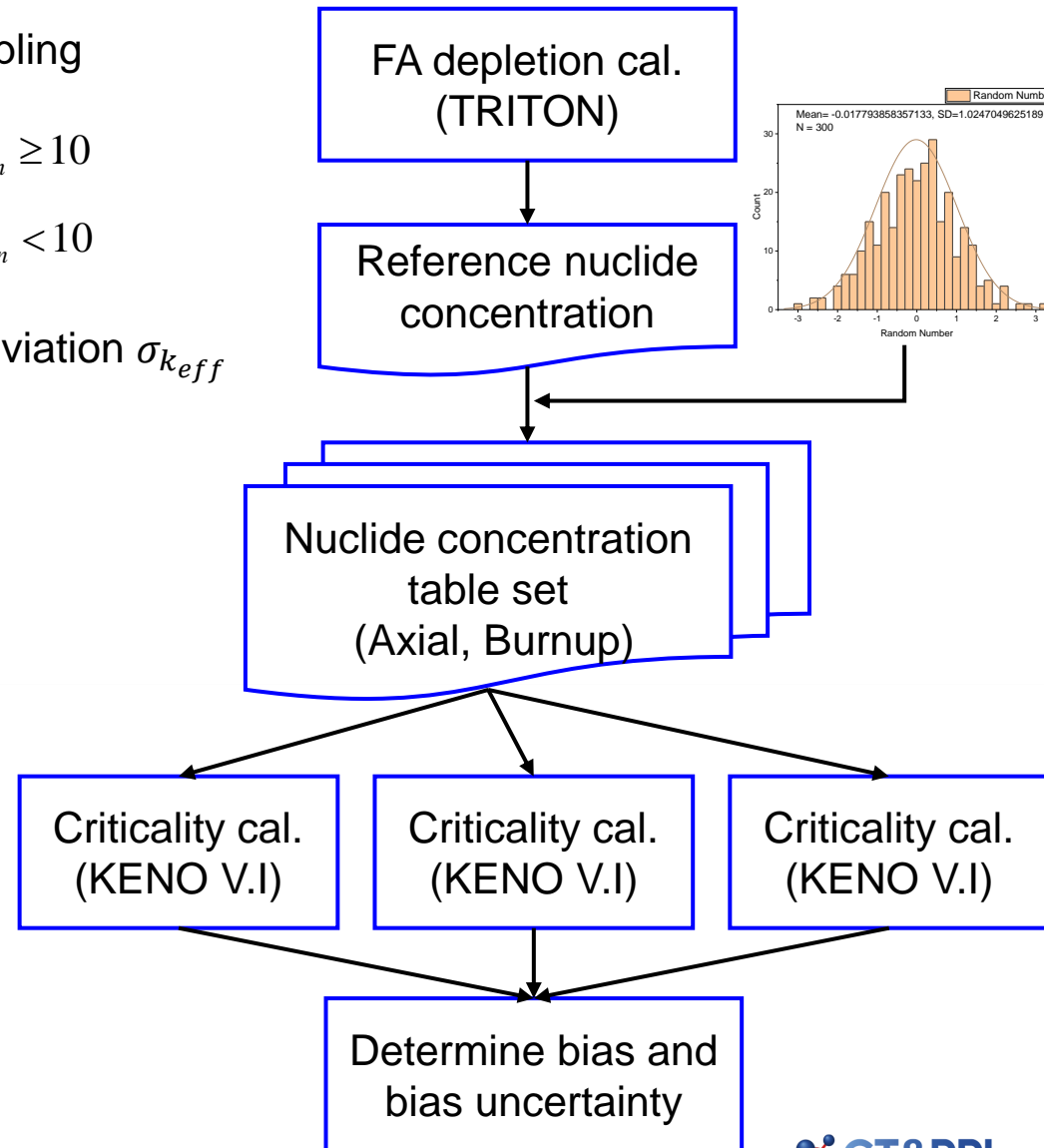
$$\bar{k}_{eff} = \sum_{i=1}^{N_c} k_{eff}^i / N_c$$

$$\sigma_{k_{eff}} = \sqrt{\sum_{i=1}^{N_c} \frac{(k_{eff}^i - \bar{k}_{eff})^2}{N_c - 1}}$$

- Bias and bias uncertainty of  $k_{eff}$

$$\beta_{depl} = \bar{k}_{eff} - k_{eff}^{REF} \quad \text{Bias}$$

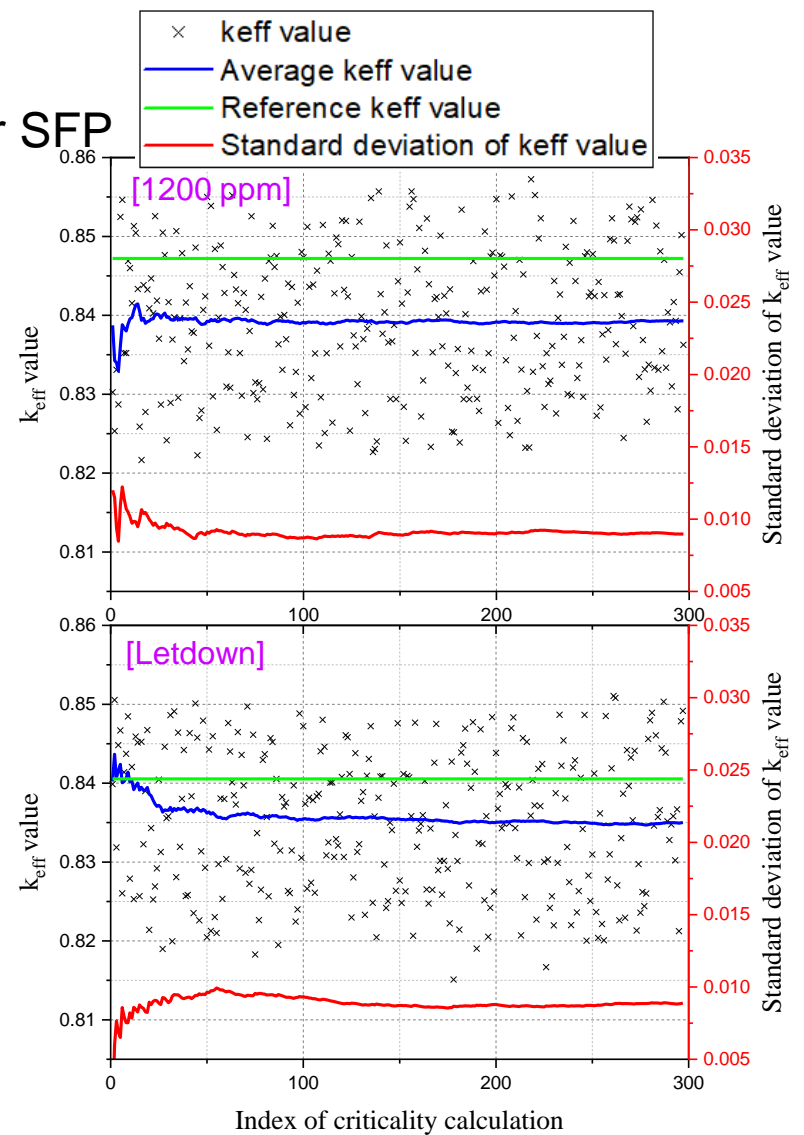
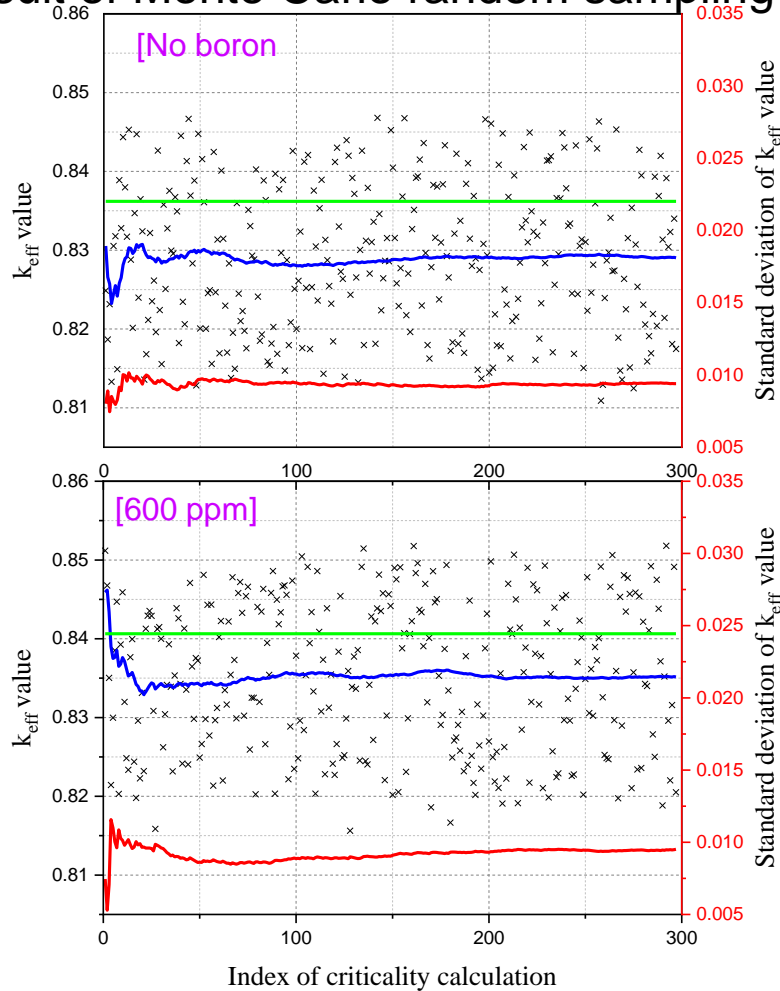
$$\Delta k_i = \sigma_{k_{eff}} \cdot tf^{N_c} \quad \text{Uncertainty}$$



[Fig. Workflow of calculation of bias and bias uncertainty in  $k_{eff}$ ]

# Methods and Results

## Result of Monte Carlo random sampling for SFP



	Reference $k_{eff}$	Average $k_{eff}$	S/D of $k_{eff}$	Bias of $k_{eff}$	Bias uncertainty of $k_{eff}$	Total depletion uncertainty
<b>0 ppm</b>	0.83620	0.82905	0.00940	-0.00715	0.01941	0.01941
<b>600 ppm</b>	0.84063	0.83515	0.00951	-0.00548	0.01964	0.01964
<b>1200 ppm</b>	0.84721	0.83929	0.00896	-0.00792	0.01850	0.01850
<b>Letdown</b>	0.84054	0.83502	0.00888	-0.00552	0.01834	0.01834

- ❑ This study evaluated depletion uncertainty for SNF pool using Monte Carlo random sampling by considering boron concentration in depletion calculation.
- ❑ If the inventory of fissile material in the SNFs is large, the reactivity of the SF SR increases.
- ❑ Because high boron concentration leads to spectrum hardening.
- ❑ Depletion uncertainty for SF SR was estimated using Monte Carlo random sampling.
- ❑ Bias of  $k_{\text{eff}}$  were estimated negative values for each boron conditions and total depletion uncertainty (include bias and bias uncertainty) values were estimated from 0.0183 to 0.0196  $\Delta k$ .
- ❑ If the inventory of fissile material in the SNFs is large, the reactivity of the SF SR increases.



**Thank you for your attention**