

Preliminary Analysis of Coupling **SCO₂ Cycle** and **Natural Draft Dry Cooling** Tower for **SMR Application**

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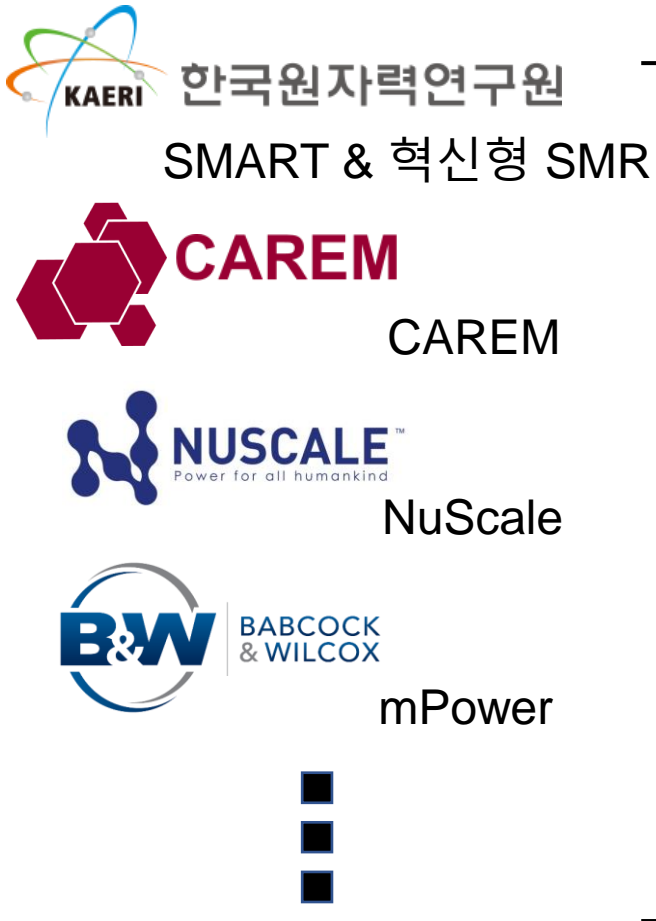
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Background

Small Modular Reactor (iPWR)

Recent trend in SMR technology development : iPWR | integrated PWR



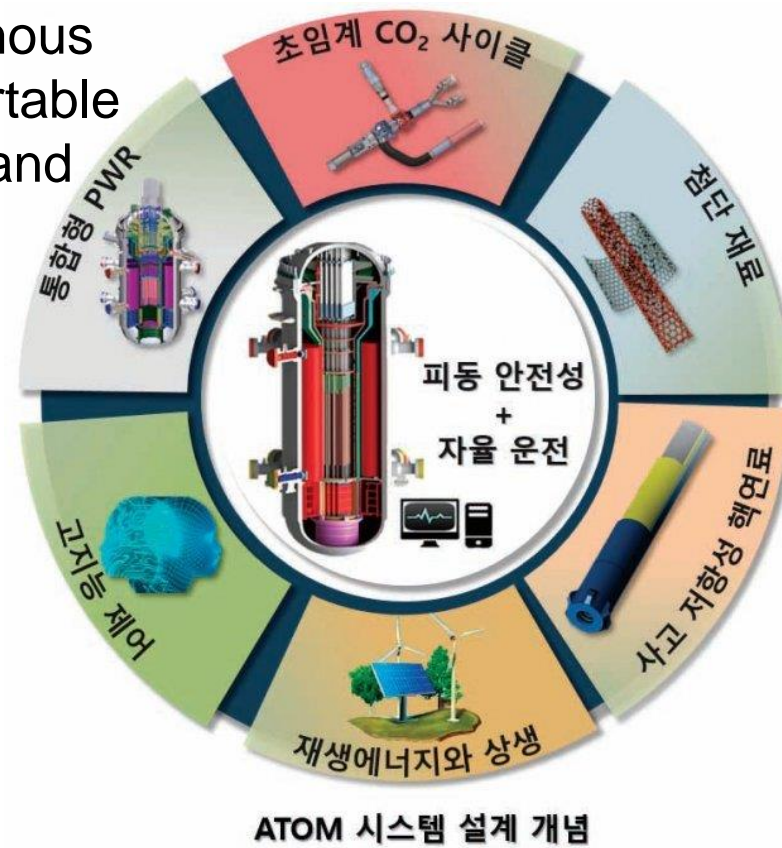
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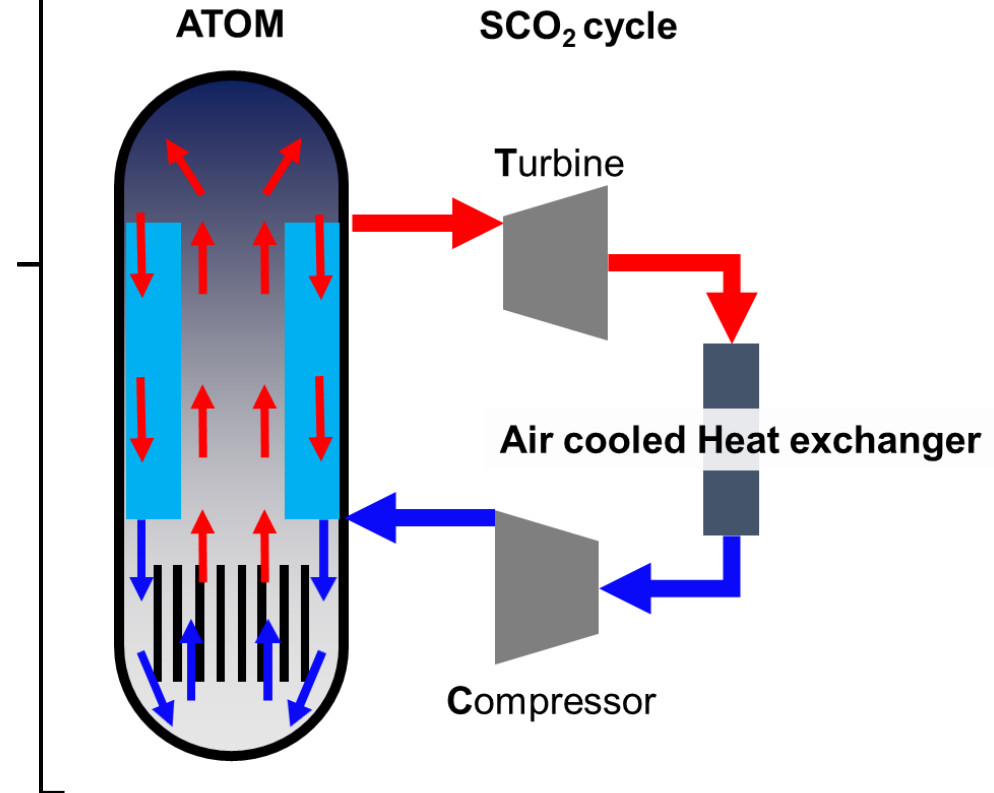
Steam Rankine cycle

- ✓ Multi-stage of the turbines
- ✓ Large scale condenser
- ✓ Evaporative loss of water for air-cooling system

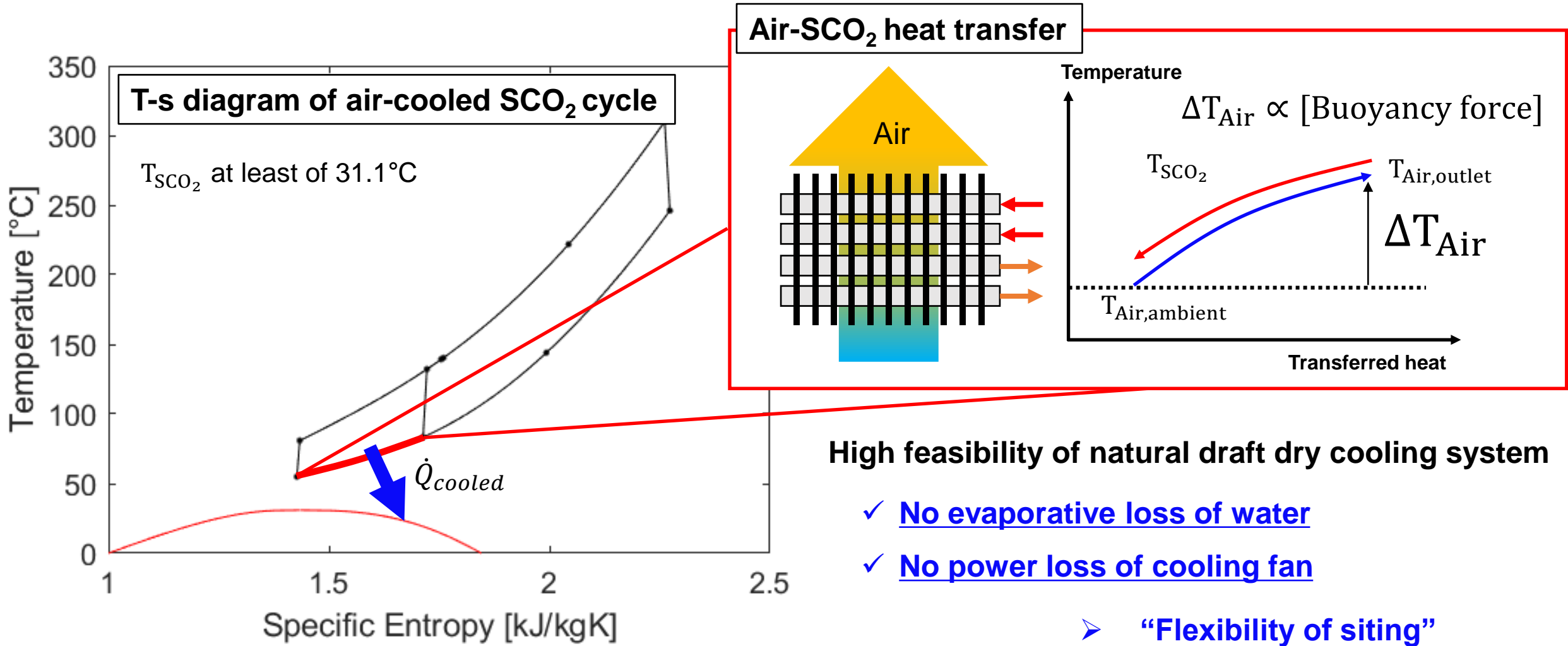
SCO₂ Brayton cycle

- ✓ High operation pressure
- ✓ Compact size of turbomachinery
- ✓ Simple configuration

SCO₂ Brayton cycle



Feasibility of dry air-cooled SCO₂ cycle



Disadvantages of the SCO_2 cycle for iPWR

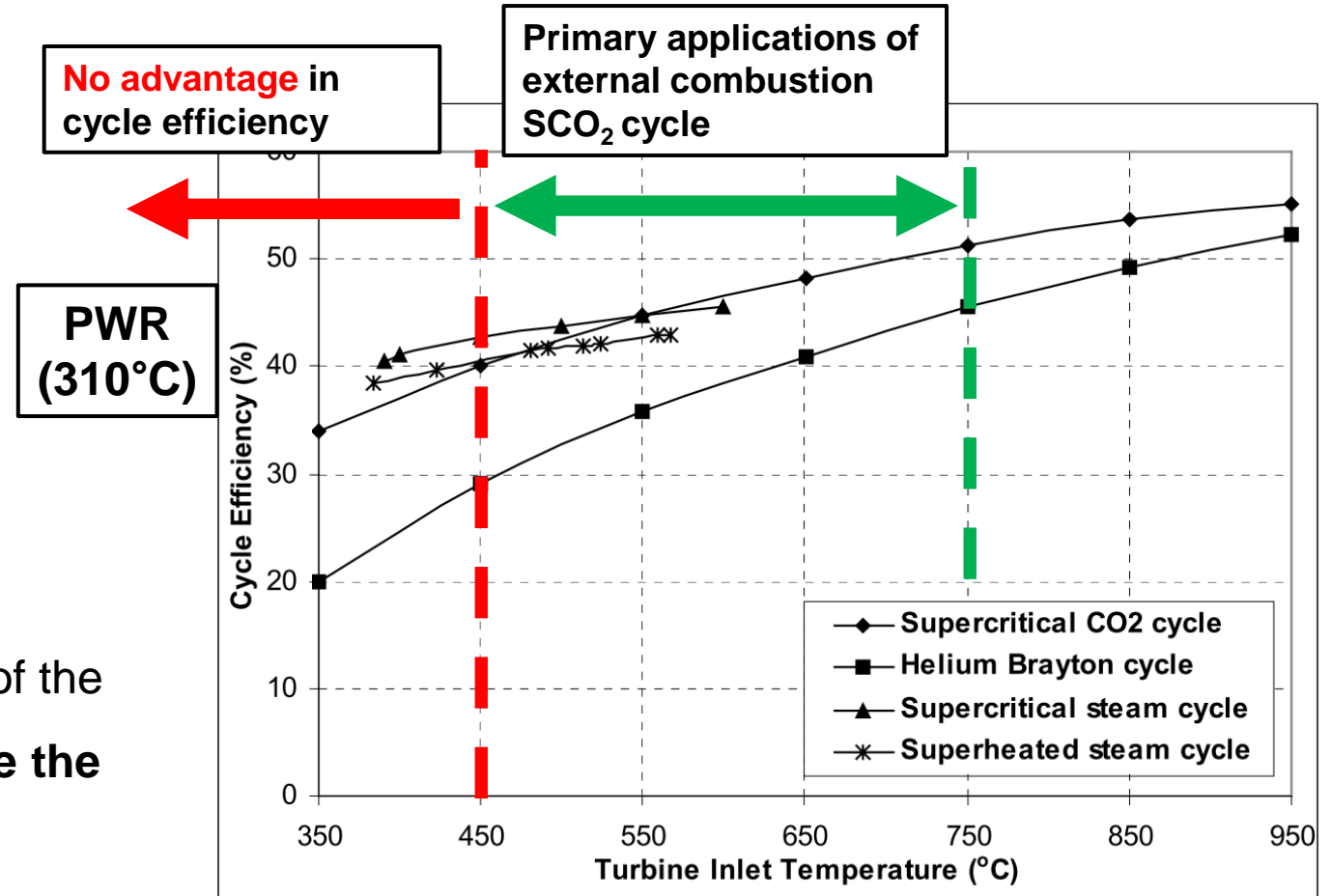
Low efficiency compared to superheated steam cycle

$$Q_{out} = Q_{in}(1 - \eta)$$

✓ the low efficiency increases the **heat rejection duty**.

✓ **Lack of information & interest** in applications where *no advantage in cycle efficiency*.

➤ *It is not clear* whether the advantages of the SCO_2 cycle in air cooling can **overcome the decreased efficiency**.

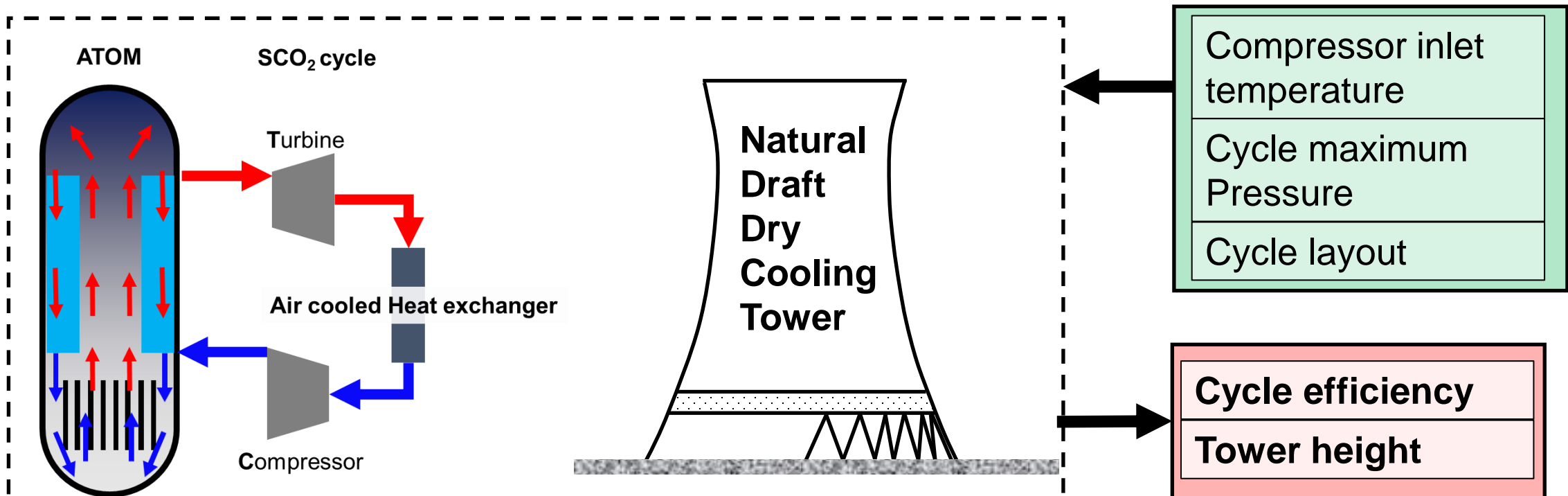


1st Stage of designing dry air-cooling SCO_2 system for iPWR

Main objective of this study:

To investigate effect of design parameters of SCO_2 cycle on the dry air-cooling system for iPWR type SMR

Main contents of this study : Sensitivity analysis



NDDCT solver : Air side approximation

- Elevation effect of atmosphere

- ✓ Pressure gradient in gravity field

$$dP/dz = -\rho_a g$$

- Isentropic expansion according to the z-direction

$$\frac{d}{dz} \left(\frac{P}{\rho^k} \right) = 0$$

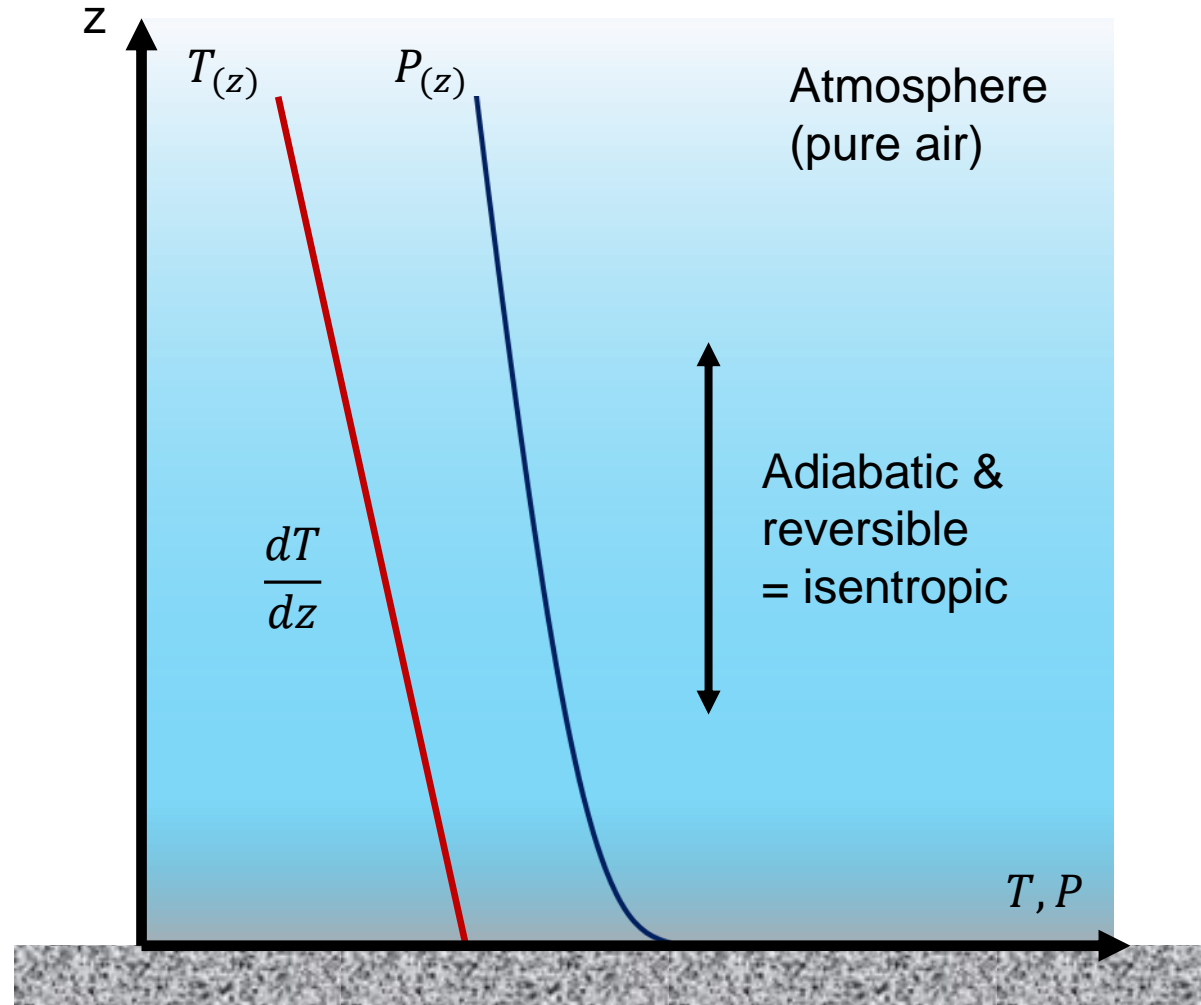
- Ideal gas assumption

$$\rho = P/RT$$

$$\frac{T_2}{T_1} = \left(\frac{P_2}{P_1} \right)^{\frac{k-1}{k}}$$

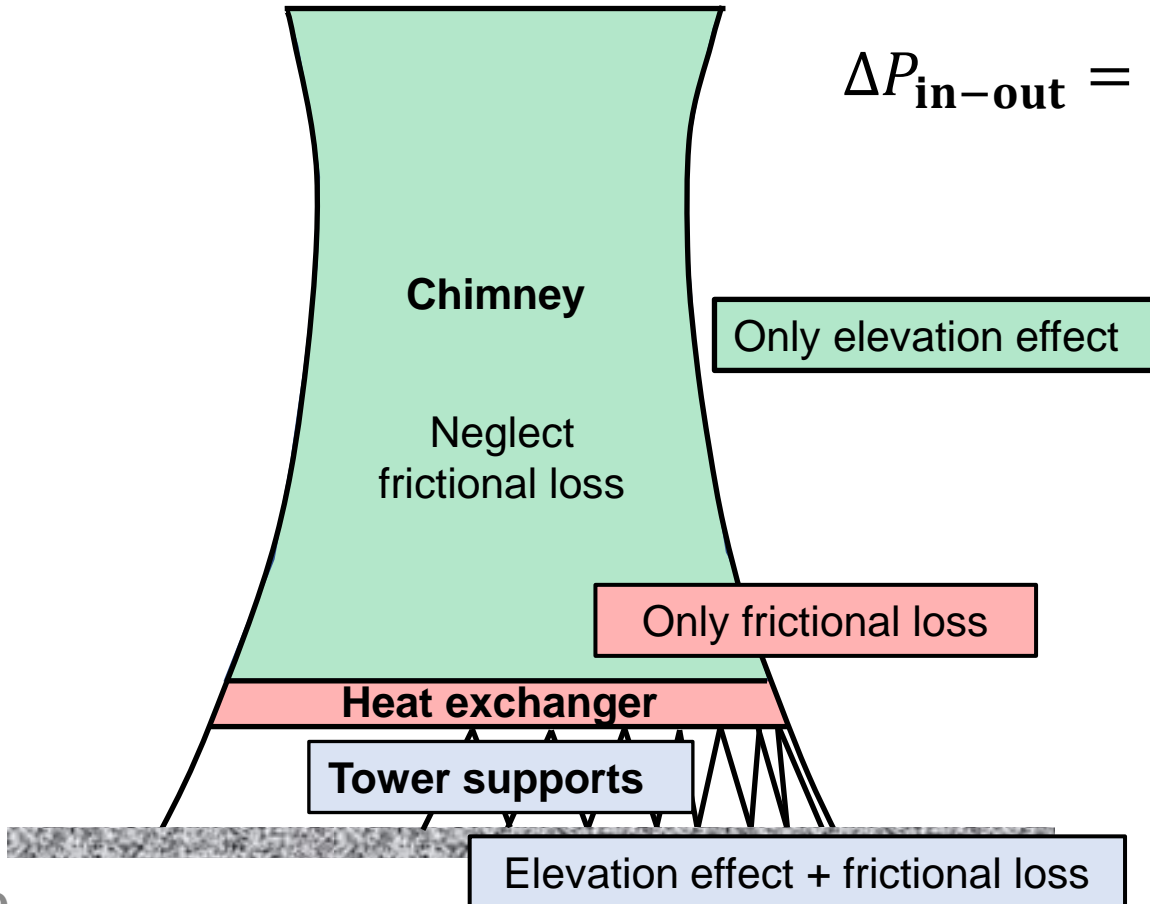
$$\frac{(1-k)}{kP} \frac{dP}{dz} + \frac{1}{T} \frac{dT}{dz} = 0$$

$$\therefore \frac{dT}{dz} = -\frac{g(k-1)}{kR} \quad \therefore P = P_1 \left(1 + \frac{z}{T_1} \frac{dT}{dz} \right)^{\frac{k}{k-1}}$$

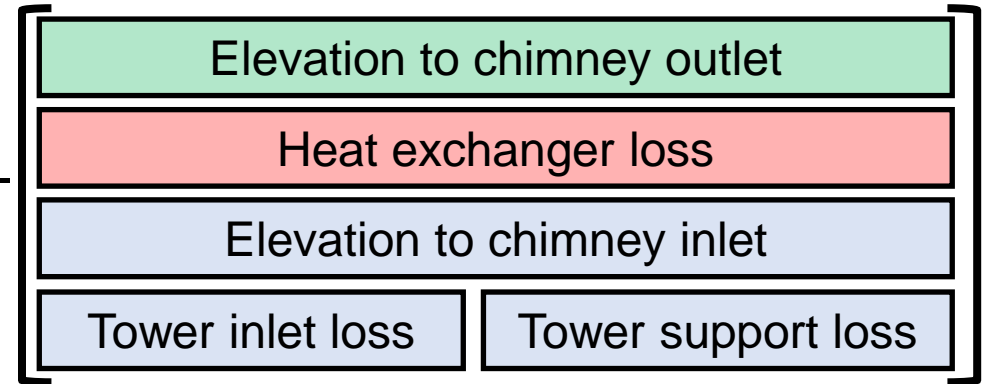


NDDCT solver : Tower side approximation

- Pressure balance of NDDCT



$$\Delta P_{\text{in-out}} = \Delta \rho g H_c -$$

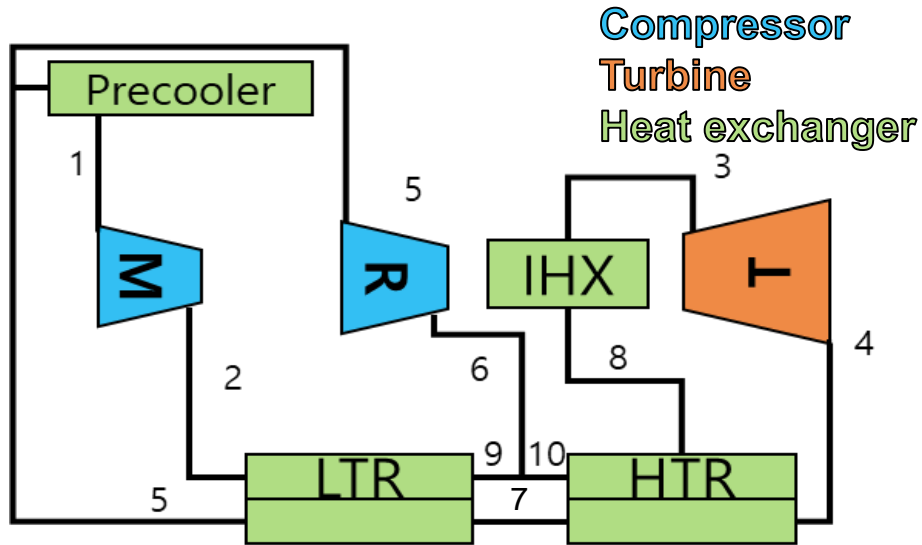


- Tower geometrics

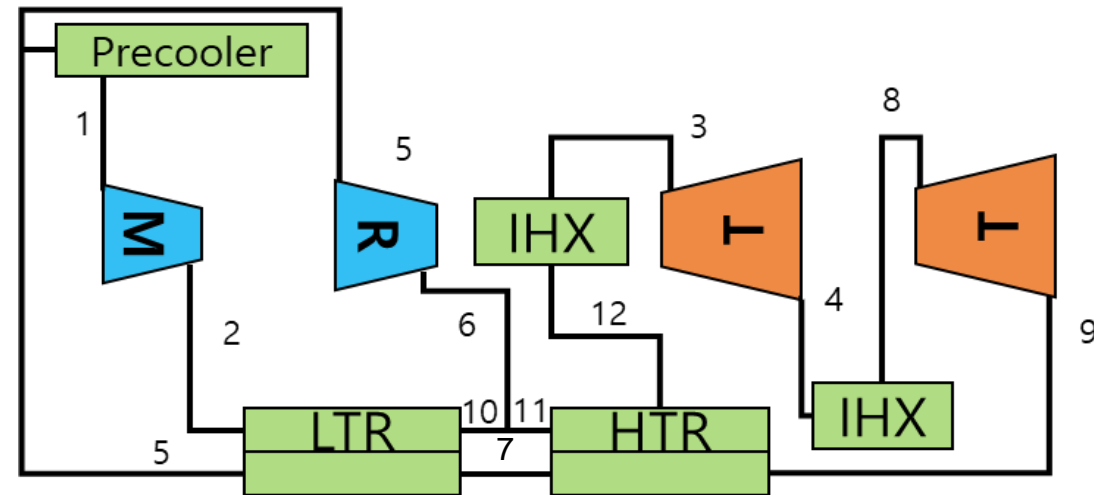
Parameters	Value
The aspect ratio (H_5/d_3)	1.4
Tower inlet height (H_3)	10 m
Diameter ratio (d_5/d_3)	0.7
Heat exchanger coverage ratio (A_{fr}/A_3)	0.65
Length & diameters of tower supports	10.5 & 0.5 m

Thermodynamic solver : SCO2 cycle layout

● Recompression Cycle



● Recompression Reheating Cycle



Turbine & Compressor

✓ Turbomachinery : isentropic efficiency

$$\Delta h_{comp} = \frac{\Delta h_s}{\eta_{comp}}, \Delta h_{turb} = \Delta h_s * \eta_{turb}$$

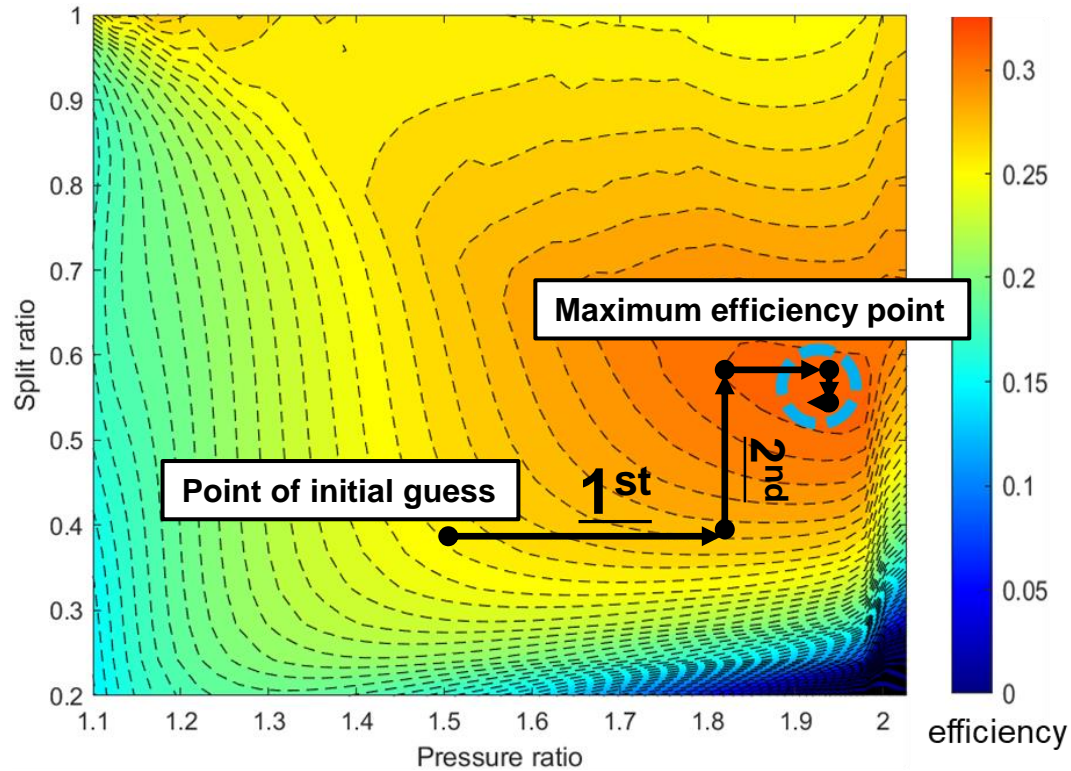
Heat exchanger

✓ Heat exchanger : effectiveness method

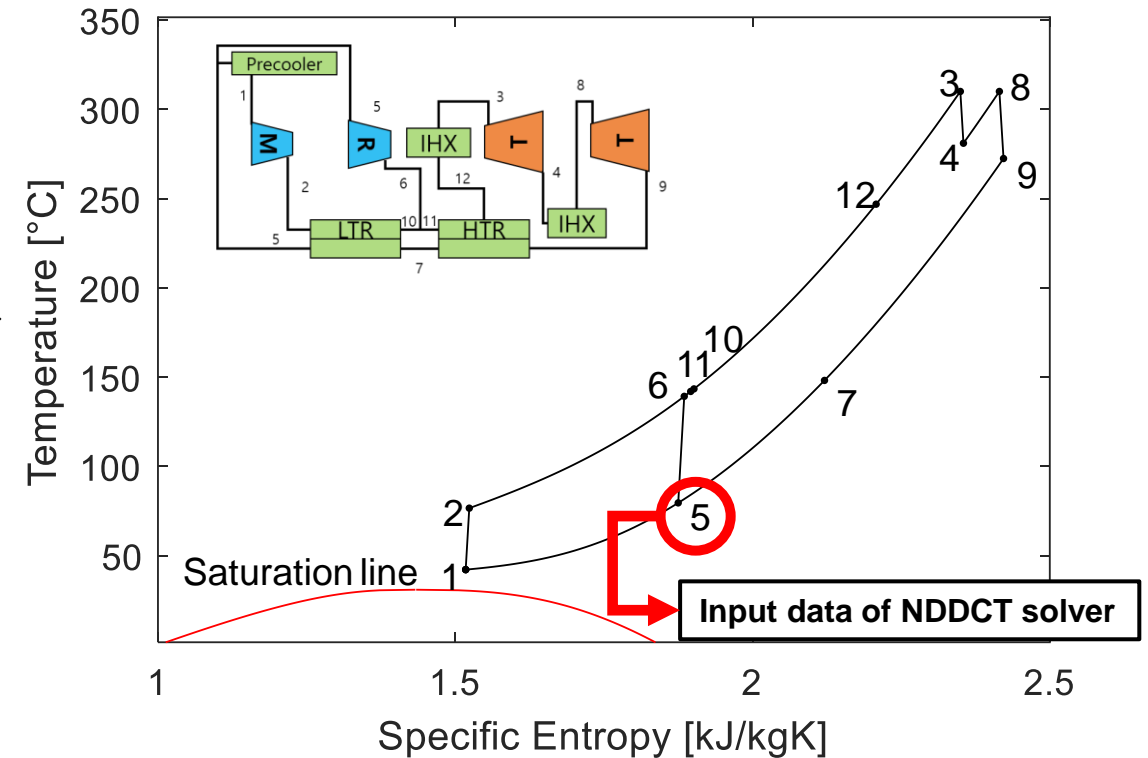
$$q_{req} = \epsilon_{HTR,LTR} * \Delta h_{max}$$

● Optimization of operating parameters : Flow split ratio & Pressure ratio

✓ Optimization process of operating parameter



✓ Calculation results of the thermodynamic solver



Sensitivity parameters & Fixed parameters

- **Sensitivity parameters**

Compressor inlet temperature	32°C – 55 °C
Cycle maximum Pressure	15MPa – 25 MPa
Cycle layout	Simple RC cycle & Single stage reheating

✓ Parameters with high sensitivity to efficiency are selected as sensitivity parameters for this preliminary analysis.

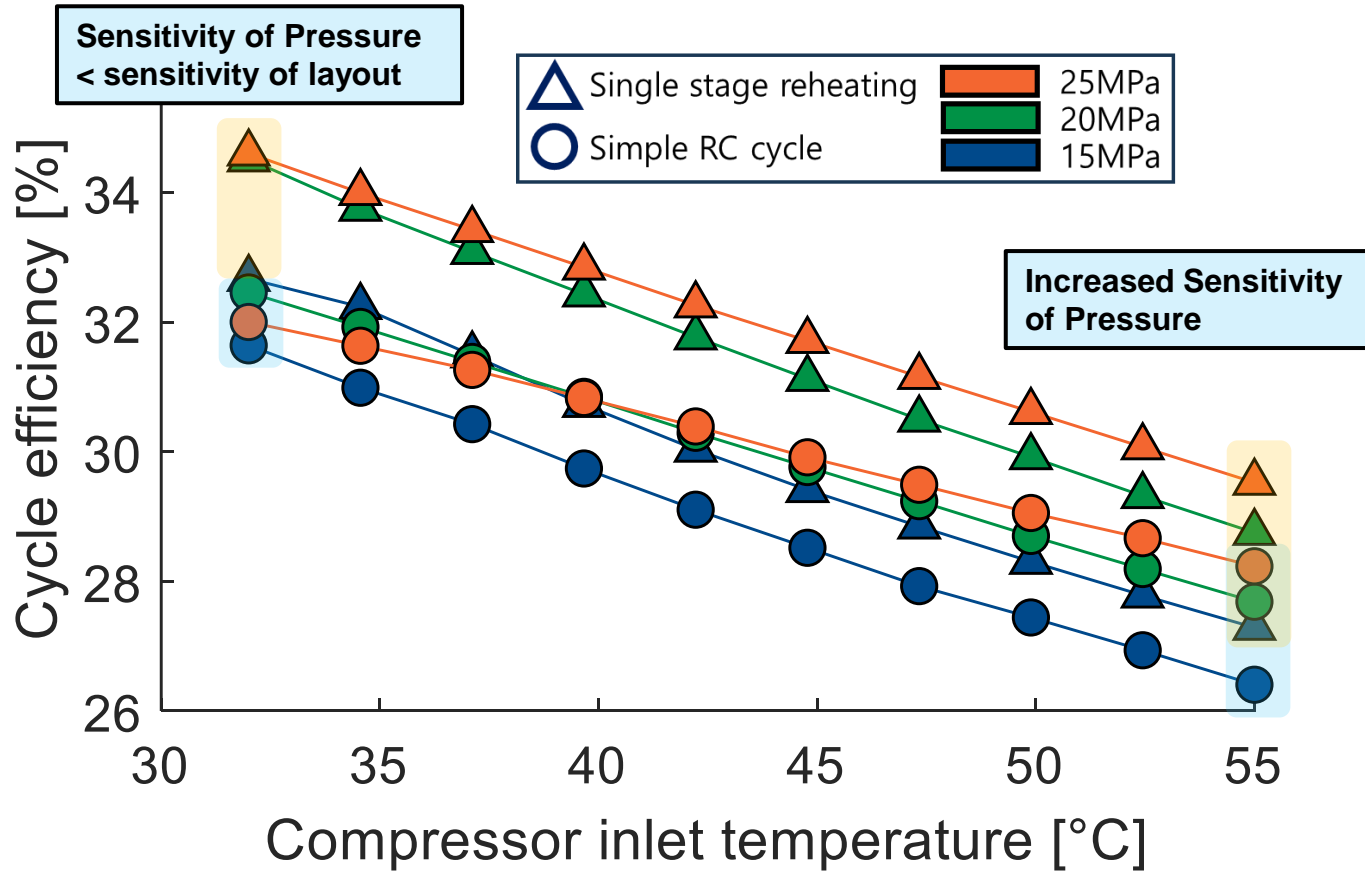
- **Fixed parameters of SCO₂ cycle for 470MWt iPWR**

Parameters	Value (or range)	Consideration
Turbine inlet temperature.	310°C	PWR condition
Compressor efficiency	0.89	Literature reference
Turbine efficiency	0.9	Literature reference
Maximum heat exchanger effectiveness	~0.95	Literature reference
Ambient air temperature	25°C	Assumption
Ambient air pressure	103kPa	Assumption

Results & Discussion

Sensitivity analysis of the cycle

● Cycle efficiency results



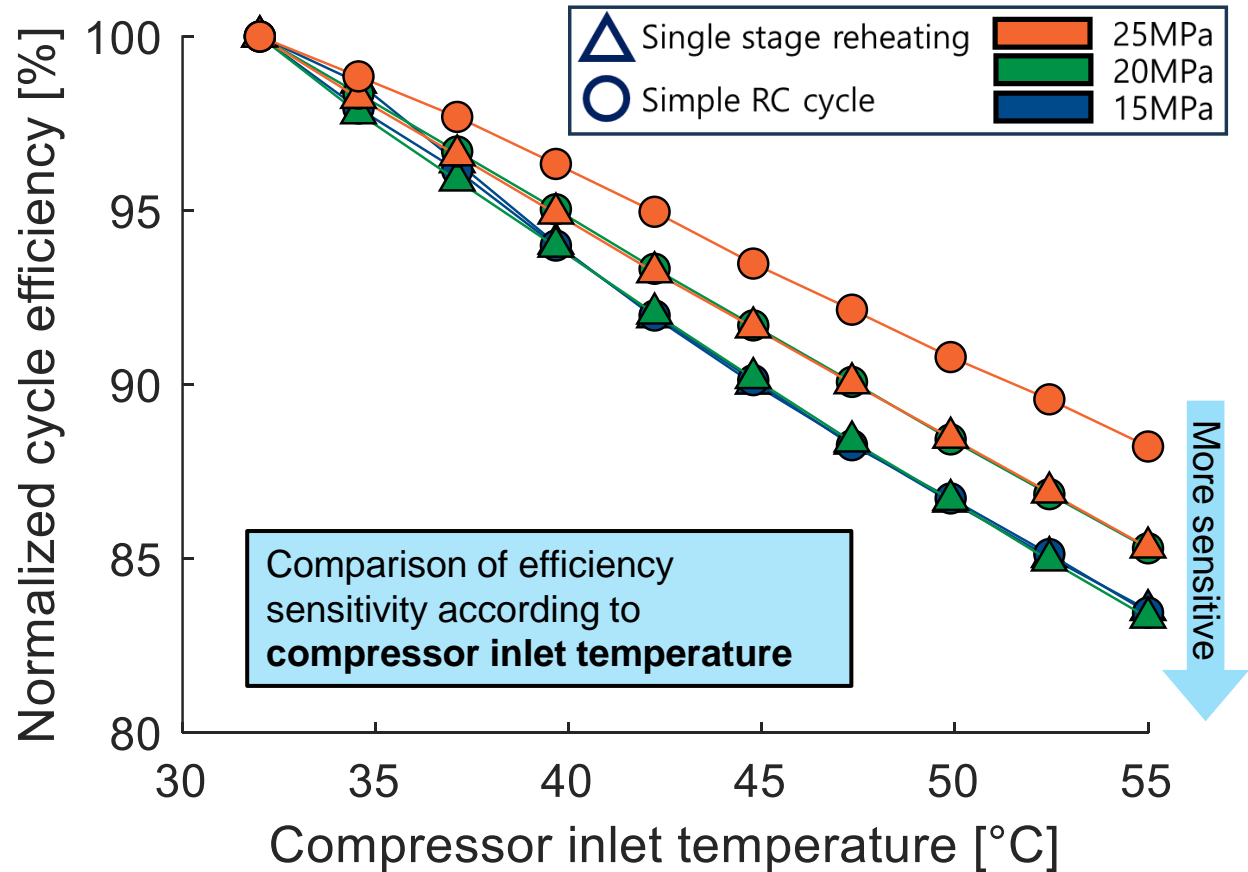
- ✓ In **25MPa with reheating case**, it shows the **best efficiency** over the whole cases.
- ✓ In **reheating cases**, the **effect of cycle maximum pressure is greater** than that of simple RC cases.
- ✓ In the **case of 25 MPa**, the **sensitivity according to temperature** was the smallest.

Results & Discussion

Sensitivity analysis of the cycle

● Normalized cycle efficiency :

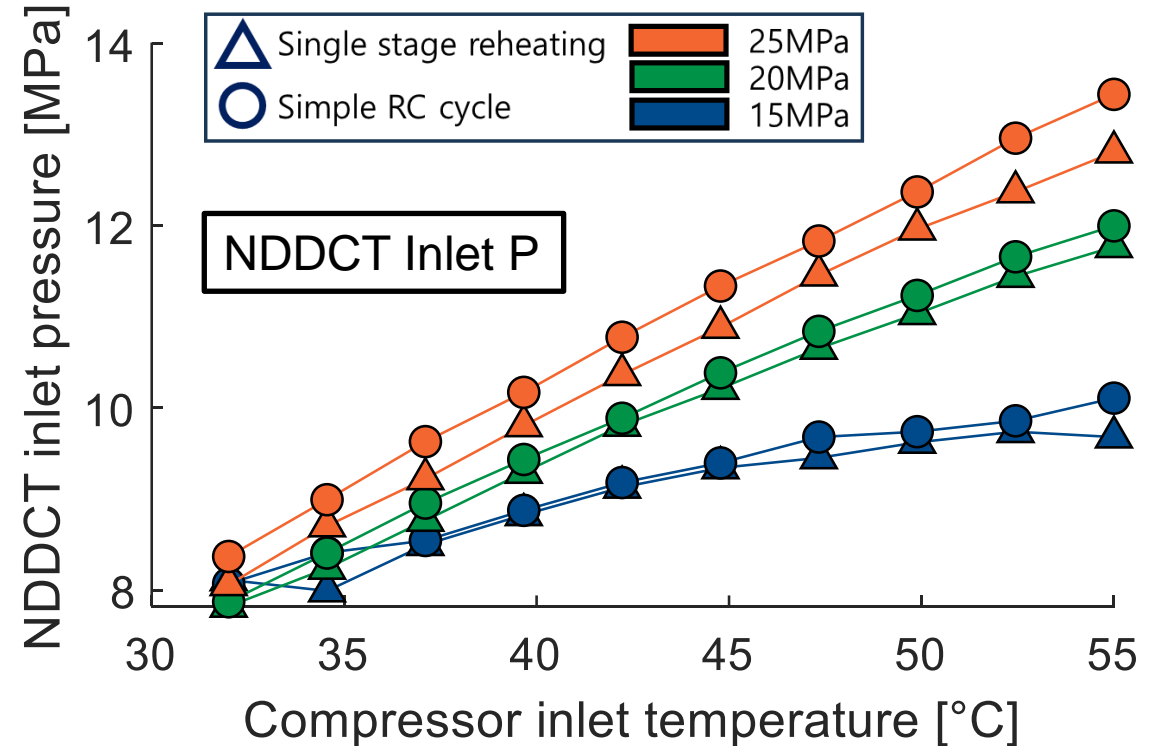
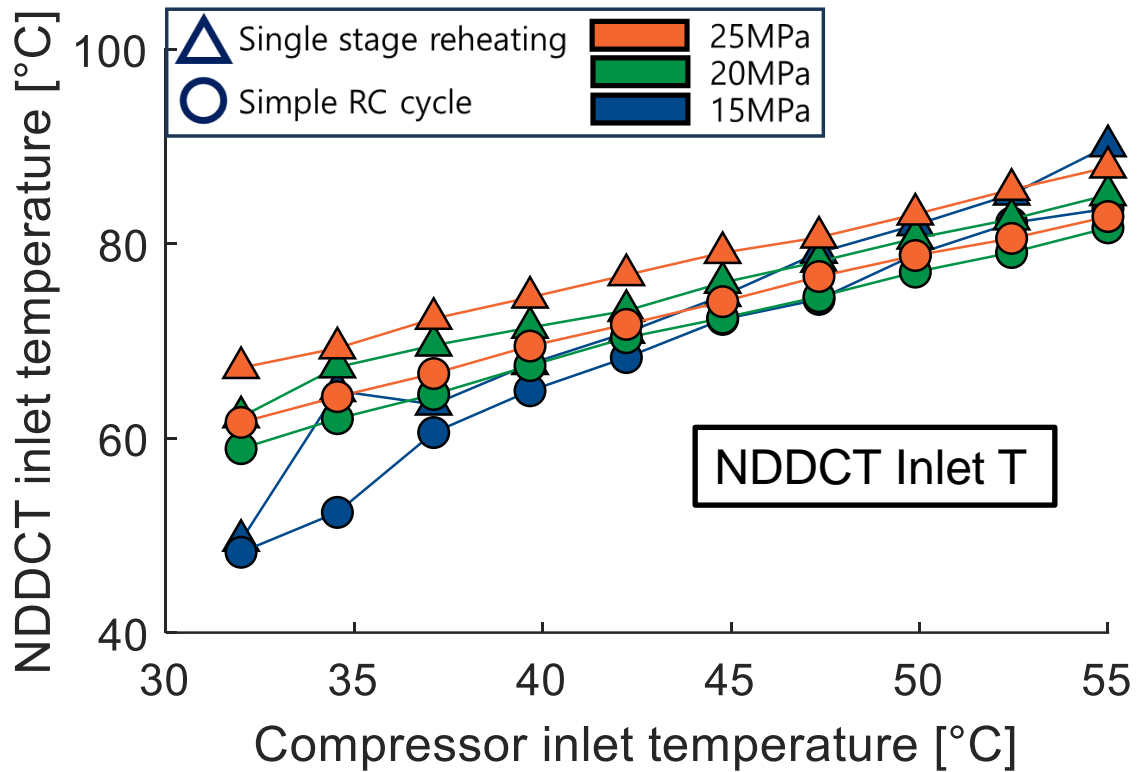
$$\frac{\eta}{\eta_{@T=32^{\circ}\text{C}}}$$



- ✓ In the case of 20 MPa and 25 MPa, it was found that the temperature sensitivity of the system increased as reheating system was applied.
- ✓ At 15 MPa case, the sensitivity due to the difference of layout was not observed.

NDDCT Input data from thermodynamic solver

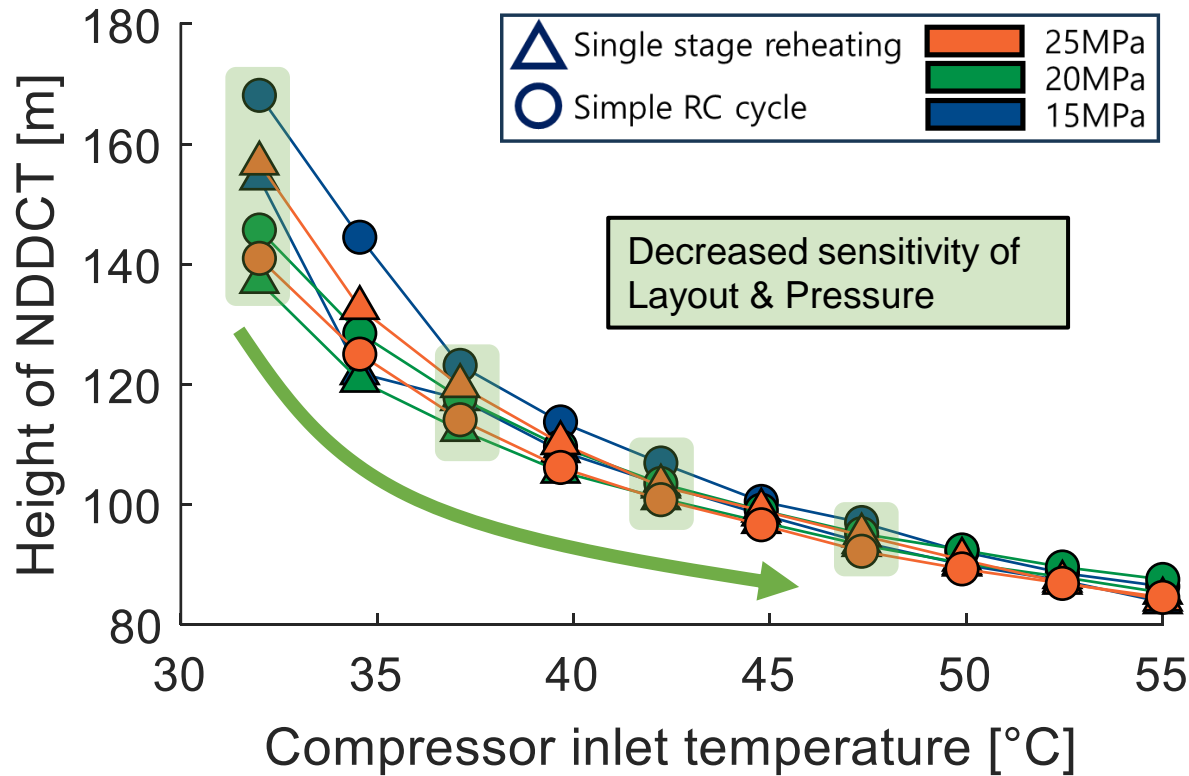
- NDDCT Input data from thermodynamic solver



Results & Discussion

Sensitivity analysis of the cycle

● Evaluated height of NDDCT



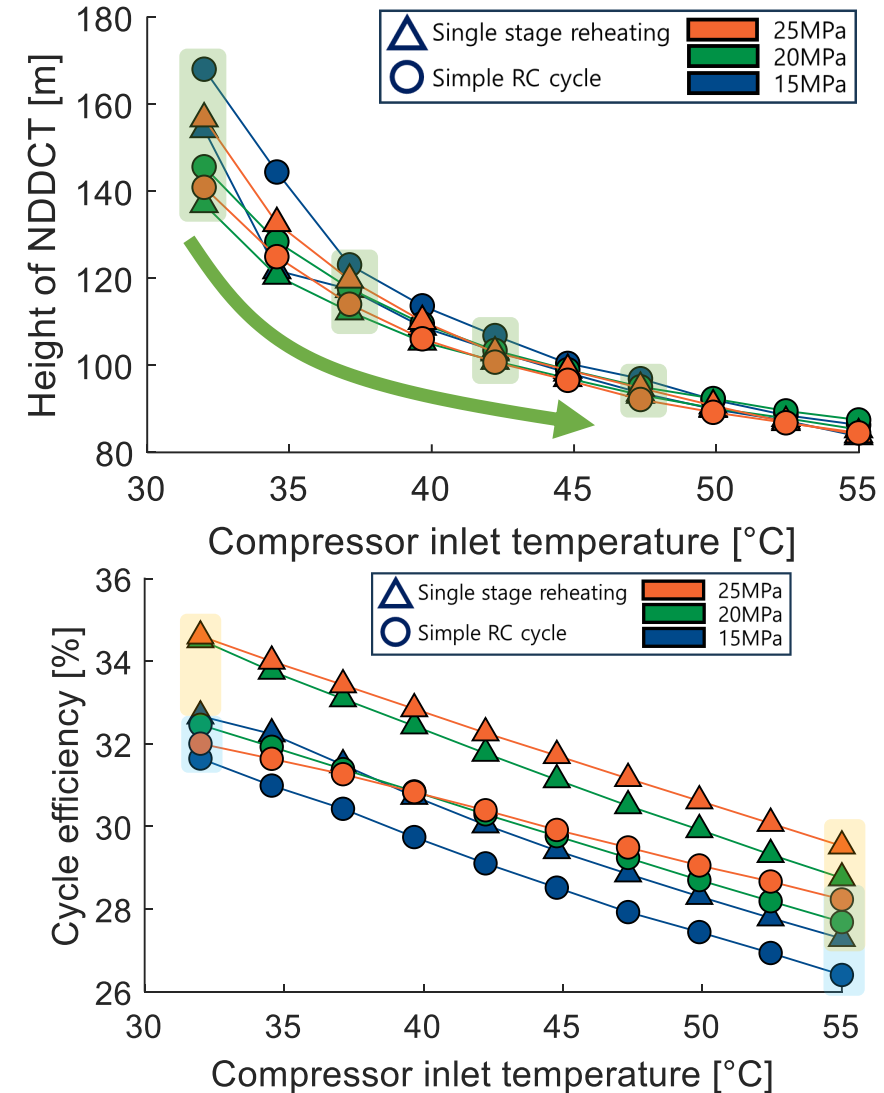
- ✓ In the case of compressor inlet temperature of 32°C, **20MPa reheating case** was found to be **the most advantageous for air-cooling.**
- ✓ Sensitivity of **all design parameters** decreases with increasing system minimum temperature.

Conclusion

Sensitivity analysis of the cycle

● Key finding :

1. In dry air-cooling conditions, although efficiency determines the amount of heat rejection duty, it did not have a significant effect on the height of NDDCT.
 2. Optimization of the compressor inlet temperature is essential.
- ✓ In the dry air-cooled SCO_2 cycle for iPWR-type SMR, it was found that the compressor inlet temperature is the most important variable through sensitivity analysis.
 - ✓ Finding a reference variable for optimizing compressor inlet temperature will be a key task of designing NDDCT.
 - ✓ It is necessary to find out the cause of the nonlinear sensitivity to the system maximum pressure.



Thank you for your attention

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