# Application of Trans-Critical CO<sub>2</sub> power conversion system in MicroURANUS

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## 1. Introduction

MicroURANUS is a 60 MW<sub>th</sub> lead-cooled micro modular reactor, which could be used for propulsion of ships sailing in Northern Sea Route. Because of the limited area on-board, power conversion system should only include small sized components with adequate thermal efficiencies. The power conversion system for the nuclear reactor consists of variety thermodynamic cycle designs, such as steam Rankine cycle and gas Brayton cycle. Due to the large sized components used in the steam Rankine cycle, the gas Brayton cycle was chosen for the power conversion system of MicroURANUS.

According to Dostal, supercritical carbon dioxide Brayton cycle (S-CO<sub>2</sub> cycle) is compact yet has suitable thermal efficiency [1]. Supercritical carbon dioxide has low compressibility near its critical point (7.38 MPa, 31°C), which causes the reduction of compressor work substantially compared to the existing gas Brayton cycle. As a result, the thermal efficiency of S-CO<sub>2</sub> Brayton cycle is higher than those of Brayton cycles using different gases, such as helium and nitrogen [2].

In the case of MicroURANUS, the ultimate heat sink is Northern Sea, with the average water temperature range from -2°C to 5 °C. Since the sea water temperature is far less than the critical temperature of supercritical carbon dioxide (31°C), trans-critical carbon dioxide (TC-CO<sub>2</sub>) Rankine cycle is more suitable for the power conversion system of MicroURANUS. In this paper, application of TC-CO<sub>2</sub> cooled power conversion system in MicroURANUS was analyzed using GAMMA<sup>+</sup>.

### 2. Methods and Results

#### 2.1 Cycle Layout Selection

Among the variety of different TC-CO<sub>2</sub> Rankine cycle layouts, three cycle layouts were selected as the candidates: simple recuperated, recompression, and precompression-recompression. These three candidates were evaluated by their simplicity, thermal efficiency, and control variables (i.e. number of components).





b) recompression cycle c) Precompressionrecompression cycle

In perspective of simplicity, the simple recuperated cycle is the simplest cycle among the candidates. Then, the recompression cycle and precompression-recompression cycle follow, respectively. To be used in the MicroURANUS, the simplicity of the cycle is considered to be an important factor due to the limited volume on the vessel. Therefore, the precompression-recompression cycle is not suitable.

For thermal efficiency and control variables, the recompression cycle is superior to the simple recuperated cycle, because the recompression cycle has two recuperators, while the simple recuperated cycle only has one. Thus, the recompression cycle was selected for the layout of the TC-CO<sub>2</sub> Rankine cycle.

# 2.2 Cycle Optimization

To calculate the design parameter of the recompression cycle, KAIST CCD, in-house MATLAB code for the cycle optimization, was used [3]. For the calculation, the effectiveness of the recuperators, compressors, and turbine were assumed to be 95%, 82% and 93%, respectively. The net efficiency of the cycle after the optimization process is 32.9%. The cycle efficiency seems quite low for the TC-CO<sub>2</sub> cycle, but considering that the reactor outlet temperature is about  $350^{\circ}$ C, which is similar to reactor outlet temperature of LWR, the cycle efficiency is reasonable. The detailed

result of the cycle optimization using KAIST CCD is compared with the result from  $GAMMA^+$  in Table 1 on the later section.

### 2.3 GAMMA<sup>+</sup> Model

GAMMA<sup>+</sup>, General Analyzer for Multi-component and Multi-dimensional Transient Application, is a code developed by Korea Atomic Energy Research Institute to analyze the Very High Temperature Reactor (VHTR) [5]. Originally, GAMMA<sup>+</sup> code was not capable of analyzing the S-CO<sub>2</sub> cycle, because it did not have corresponding fluid properties. Currently, the information required for the analysis of S-CO<sub>2</sub> and TC-CO<sub>2</sub> cycles are included in the GAMMA<sup>+</sup> code with work of Oh [4,6]. Consequently, GAMMA<sup>+</sup> code is now capable to analyze TC-CO<sub>2</sub> power conversion system in MicroURANUS.



Figure 2. Design parameter check points for the recompression cycle

Code	KAIST CCD		GAMMA <sup>+</sup>	
Point	Temp (°C)	Pres (MPa)	Temp (°C)	Pres (MPa)
1	350.0	-	350.0	-
2	250.0	-	251.8	-
3	327.0	14.7	327.1	14.7
4	243.6	6.5	243.6	6.5
5	114.5	6.33	116.4	6.23
6	35.4	6.2	35.8	6.18
7	35.4	6.2	35.8	6.18
8	15.0	6.15	15.1	6.16
9	25.4	14.85	25.6	14.96
10	107.4	14.85	109.2	14.94
11	109.0	14.85	110.8	14.93
12	207.3	14.72	208.2	14.88
13	35.4	6.2	35.8	6.18
14	110.3	14.9	112.3	14.93

Table 1. Results from KAIST CCD and GAMMA<sup>+</sup>

As shown in Figure 2, design check points 1 and 2 are in the primary side. It is given that the inlet and outlet temperature of the intermediate heat exchanger is  $250^{\circ}$ C and  $350^{\circ}$ C, respectively. Because the full analysis of primary side of MicroURANUS is out of scope for this paper, the pressure of the primary side is removed from the result. The total mass flow rate of CO<sub>2</sub> is 412.0 kg/s and the split ratio between points 6 and 7 is 0.48345.

Table 1 indicates that the result from the GAMMA<sup>+</sup> corresponds to the result of KAIST CCD, which suggests the net efficiency of 32.9% for the power

conversion system with TC-CO $_2$  recompression Rankine Cycle.

## 3. Summary and Future works

To analyze TC-CO<sub>2</sub> power conversion system of MicroURANUS, GAMMA<sup>+</sup> code was applied. The analysis shows that the power conversion system reaches near the cycle optimization parameters, which allows the net cycle efficiency of 32.9% in MicroURANUS condition. For the future work, the primary side of MicroURANUS should be modeled using GAMMA<sup>+</sup>, so that the full transient of MicroURANUS can be simulated.

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