

# **Development of Trend Map on the Plant Initial Condition Using Sensitivity Study in the Non-LOCAs**

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# Introduction

## 1. Determination of event scenario

## 2. Selection of plants

## 3. Making a PIRT

## 4. Specifying Codes

## 5. Codes Assessment

## 6. Defining NPP Modeling and Nodalization

## 7. Base Calculation of the NPP

## 8. NPP Sensitivity Calculations

## 9. Final Assessment of the Events

### 1 단계

#### 규제검증평가 모델 정의

불확실도 평가 :

Physical Model, Calibration parameter,  
Unknown constant.

민감도 분석 :

경계/초기 조건, 독립변수

### 2 단계

#### 규제검증코드 검증 및 평가

불확실도 평가 : 실험자료(SET\*, IET\*\*)를  
이용하여 범위와 분포 도출, 산업 전반적으  
로 널리 알려진 방법 이용

### 3 단계

#### 원전 안전여유도 평가

민감도 분석 :

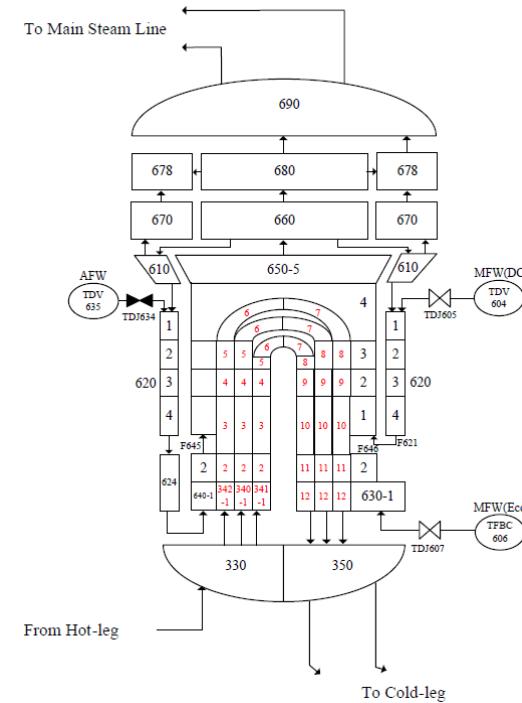
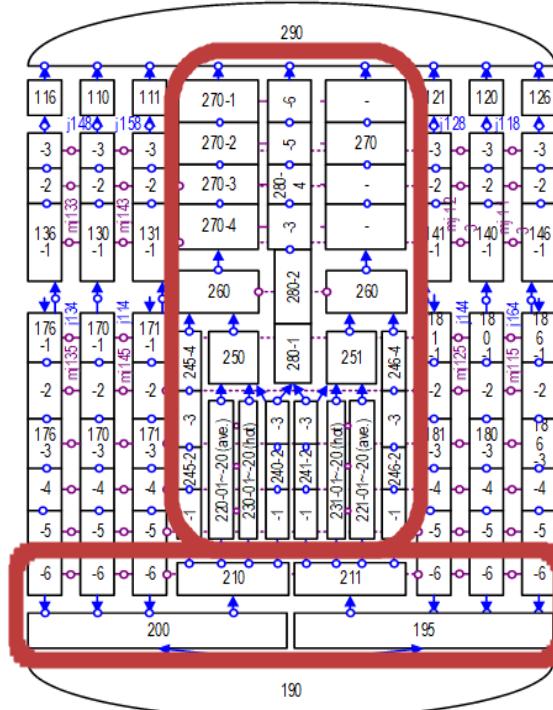
Pearson 계수 또는 Spearman 순위 계수

정량화 :

Wilk's Formula (95/95)

In step 8 of Non-LOCA methodology by KINS, sensitivity study can be the best way to compensate on the bias and error  
for regulatory conservatism from the unknown parameters or methodology

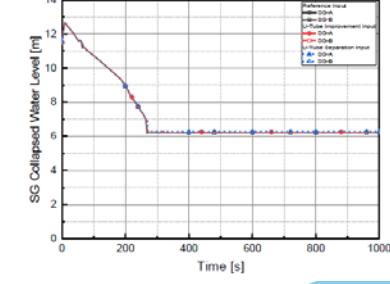
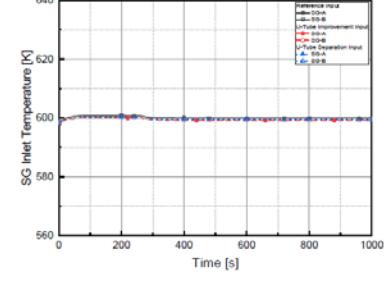
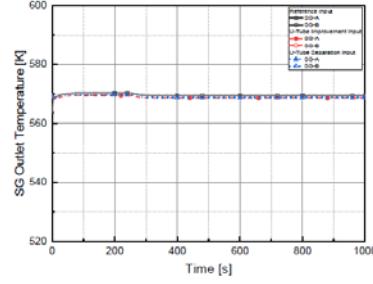
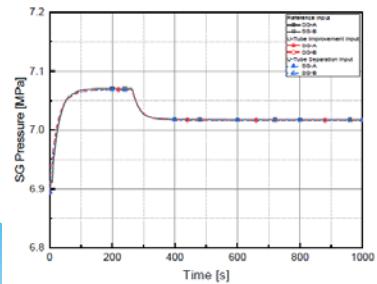
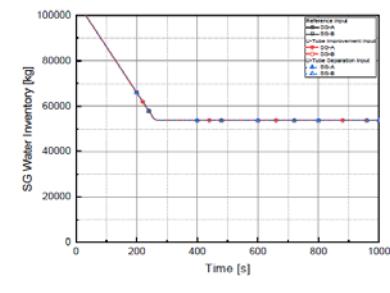
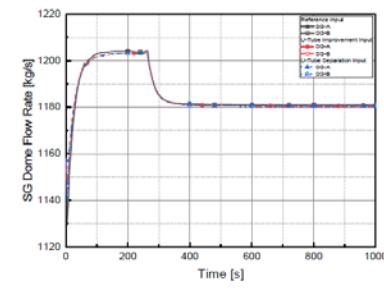
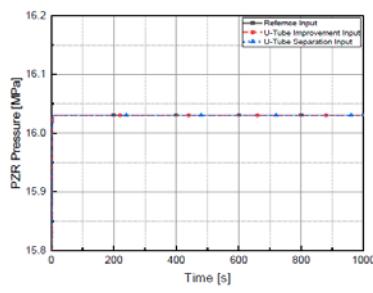
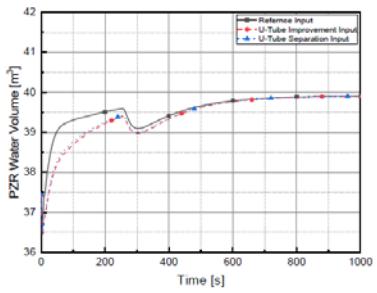
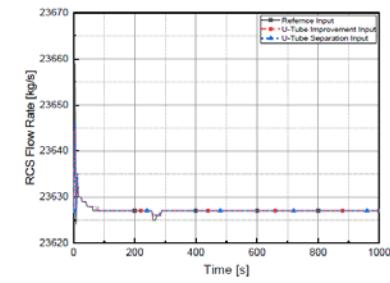
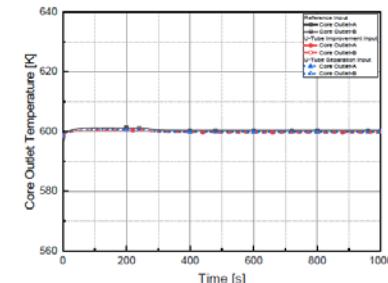
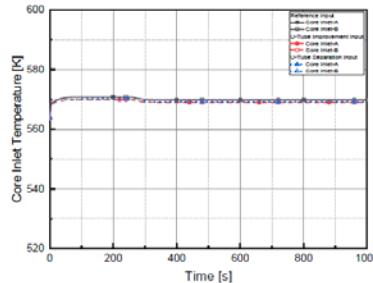
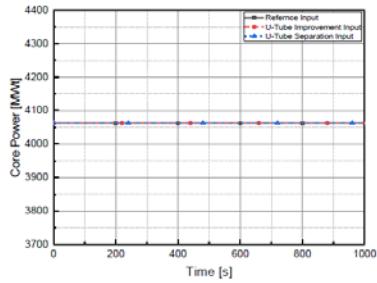
# Modeling applied to multiple channel



**Reactor core** : in order to analyze the core asymmetry, core is consist of 2 hottest channels, 2 hot channels and 2 average cores

**Steam Generator** : U-tubes in the SG is divided into three-part considering the length of U-tubes with the latest design data

# Steady state results of ARP1400



# Sensitivity Matrix – MSLB

- Initial condition focusing on fuel damage in the range of LCO

TEST No.	Parameter			Remark
	RCS Flow (%)	Core inlet Temp. (K)	FTC	
Reference	112.56	569.25	EOC	RCS flow-High / core inlet temp. -High
Case 1	112.56	569.25	BOC	
Case 2	95.0	569.25	EOC	RCS flow – Low
Case 3	97.5	569.25	EOC	
Case 4	100.0	569.25	EOC	RCS flow – Normal
Case 5	102.5	569.25	EOC	
Case 6	105.0	569.25	EOC	
Case 7	108.0	569.25	EOC	RCS flow – High
Case 8	112.56	560.95	EOC	Core inlet temp. – Low
Case 9	112.56	562.0	EOC	
Case 10	112.56	564.0	EOC	
Case 11	112.56	566.0	EOC	
Case 12	112.56	567.53	EOC	Core inlet temp. – Normal

# Sensitivity Matrix – MFLB

- Initial condition focusing on fuel damage in the range of LCO

TEST No.	Operating Parameters			MDNBR	
	RCS Flow (%)	PZR Pr.	Inlet Temp. (K)		
Case 1	92	15.65	569.11	1.3994	RCS Flow
Case 2	<b>95</b>	<b>15.65</b>	569.36	<b>1.432</b>	
Case 3	<b>100</b>	<b>15.65</b>	569.78	<b>1.5089</b>	
Case 4	<b>105</b>	<b>15.65</b>	570.17	<b>1.5502</b>	
Case 5	<b>110</b>	<b>15.65</b>	570.54	<b>1.6058</b>	
Case 6	<b>115</b>	<b>15.65</b>	570.89	<b>1.6582</b>	
Case 7	92	15.0	569.25	<b>1.3214</b>	PZR Pr.
Case 8	<b>92</b>	<b>15.25</b>	<b>569.2</b>	<b>1.3399</b>	
Case 9	<b>92</b>	<b>15.5</b>	<b>569.14</b>	<b>1.3716</b>	
Case 10	<b>92</b>	<b>15.75</b>	<b>569.09</b>	<b>1.4113</b>	
Case 11	<b>92</b>	<b>16.0</b>	<b>569.04</b>	<b>1.436</b>	
Case 12	<b>92</b>	<b>15.65</b>	<b>560.83</b>	<b>1.5649</b>	Inlet Temp.
Case 13	<b>92</b>	<b>15.65</b>	<b>562.86</b>	<b>1.5258</b>	
Case 14	<b>92</b>	<b>15.65</b>	<b>564.91</b>	<b>1.5009</b>	
Case 15	<b>92</b>	<b>15.65</b>	<b>567.07</b>	<b>1.4469</b>	

# Sensitivity Matrix – Seized RCP Rotor

- Initial condition focusing on fuel damage in the range of LCO

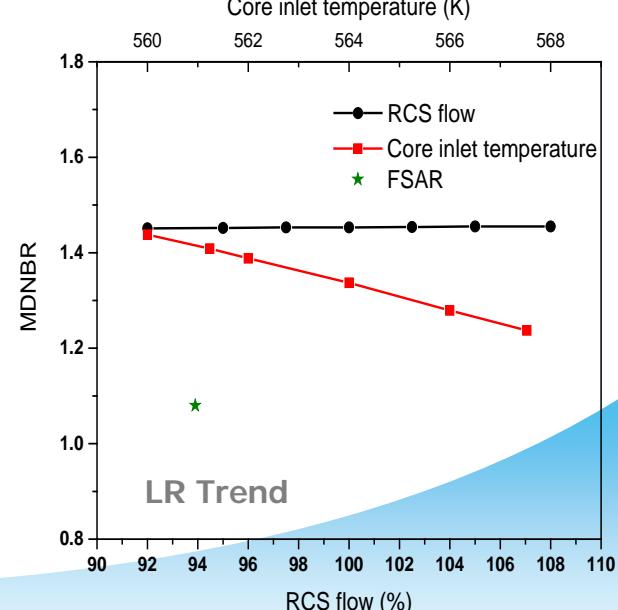
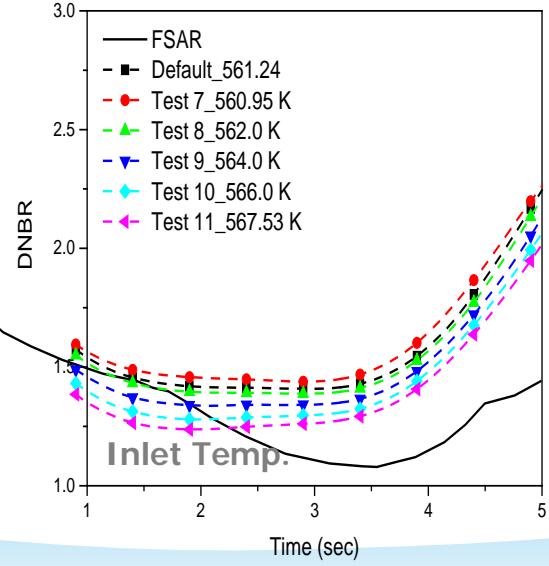
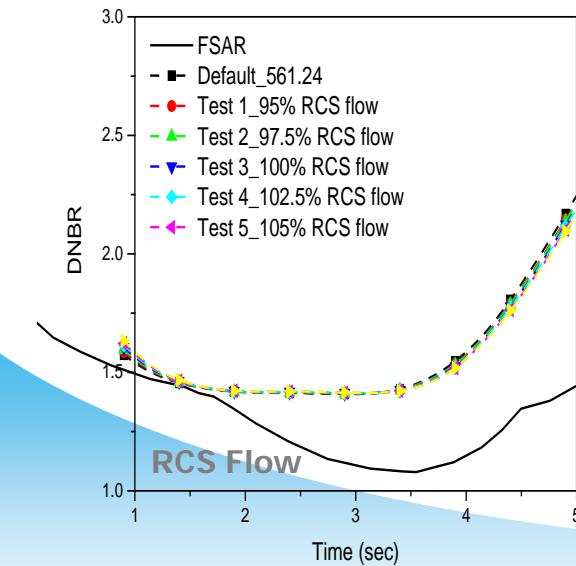
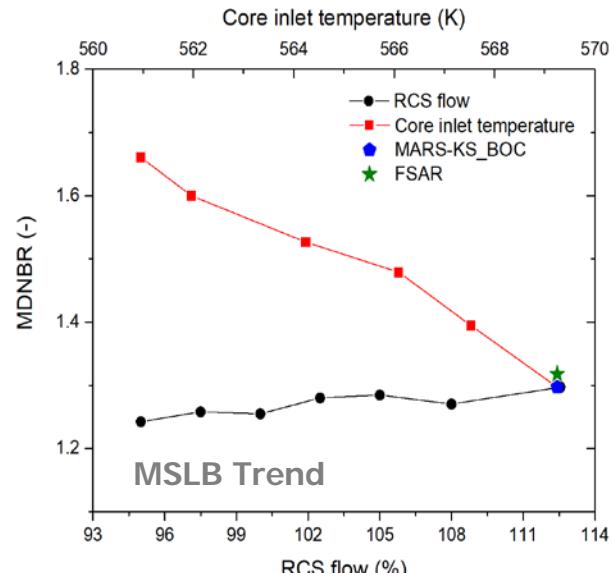
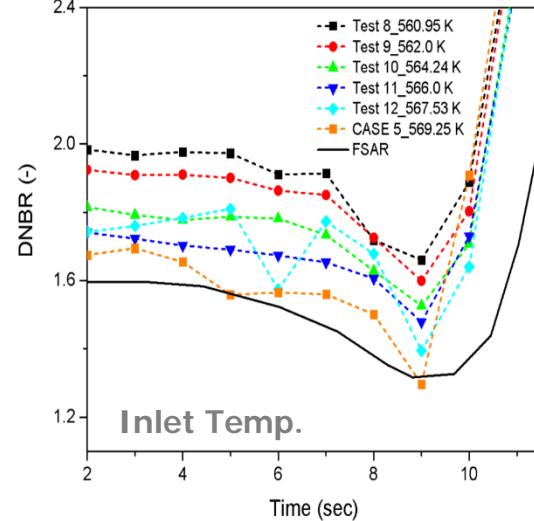
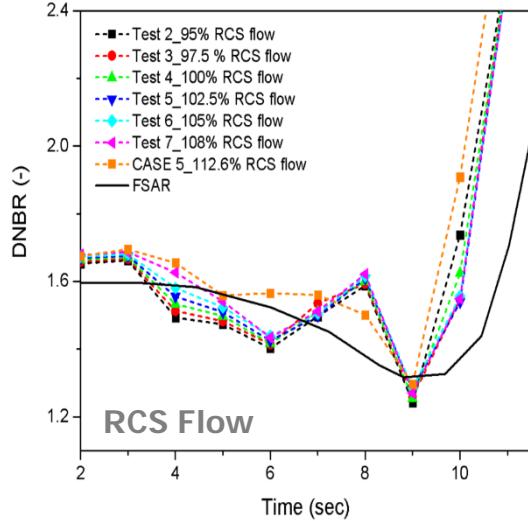
TEST No.	Parameter		Remark
	RCS flow (%)	Core inlet temp. (K)	
Reference	92.0	561.24	
Test 1	<b>95.0</b>	561.47	RCS flow – Low
Test 2	<b>97.5</b>	561.66	
Test 3	<b>100.0</b>	561.84	RCS flow – Normal
Test 4	<b>102.5</b>	562.02	
Test 5	<b>105.0</b>	562.19	
Test 6	<b>108.0</b>	562.39	RCS flow – High
Test 7	92.0	<b>560.95</b>	Core inlet temp. – Low
Test 8	92.0	<b>562.0</b>	
Test 9	92.0	<b>564.0</b>	
Test 10	92.0	<b>566.0</b>	
Test 11	92.0	<b>567.53</b>	Core inlet temp. – Normal

# Sensitivity Matrix – SGTR

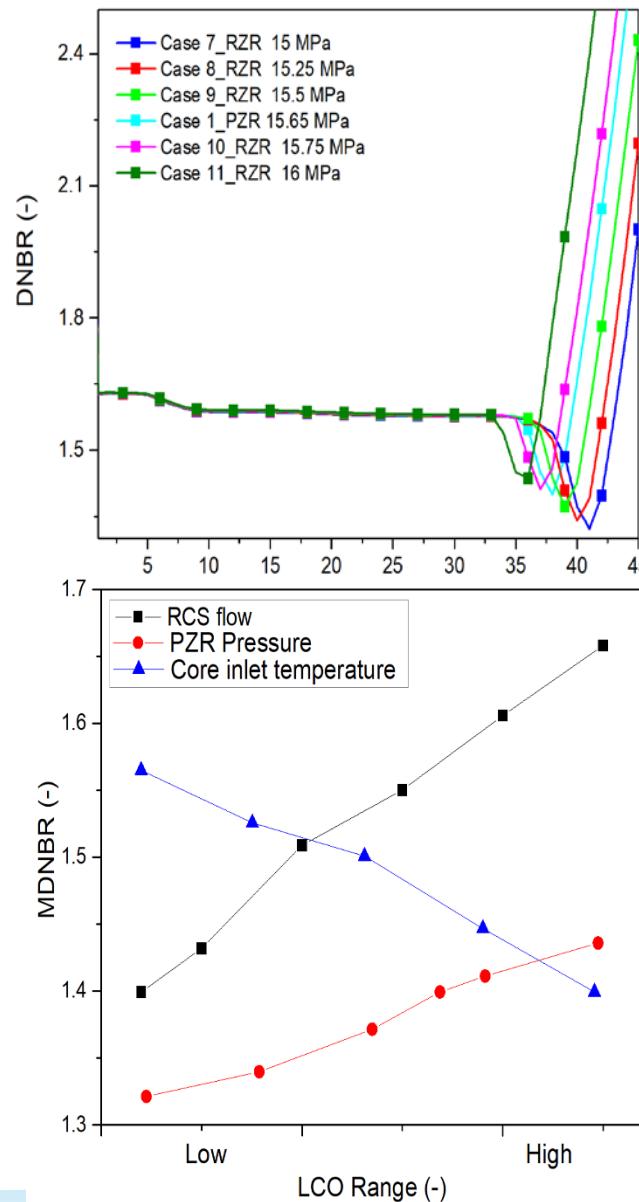
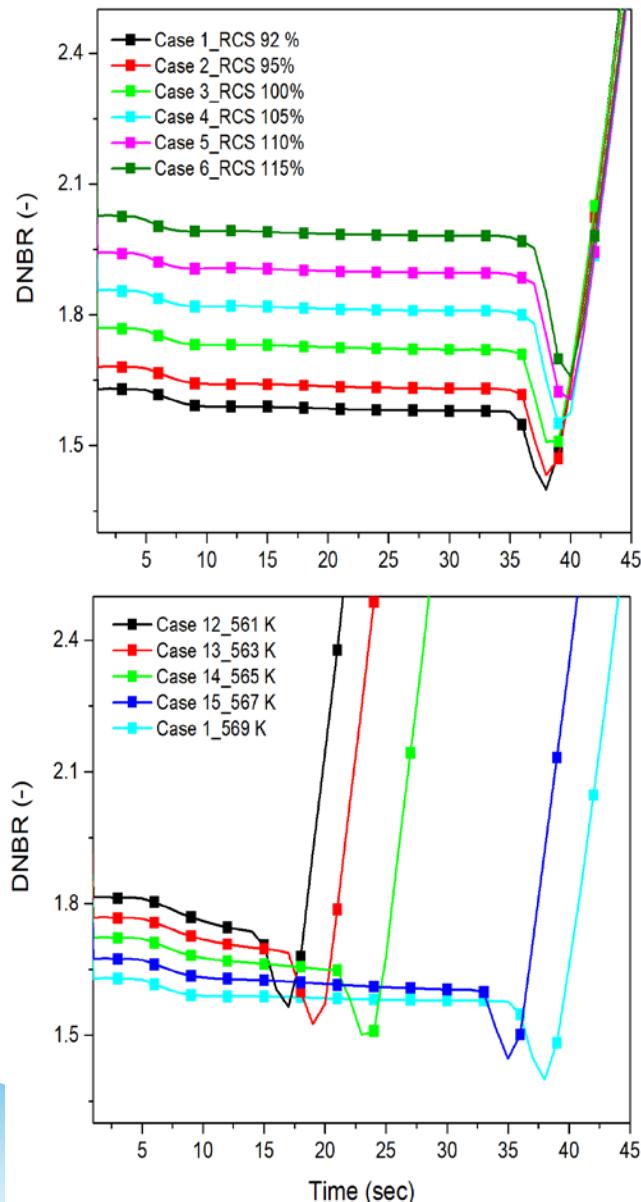
- Initial condition focusing on fuel damage in the range of LCO**

TEST	Parameter						MDNBR (-)
	F <sub>R</sub> (-)	P <sub>PRZ</sub> (MPa)	T <sub>c,i</sub> (C)	W <sub>c,i</sub> (kg/sec)	M <sub>SG</sub> (kg)	LOOP	
Default	1.8236	16.03	294.89	19344 (92%)	1.2E5	No	1.2053
2p1	-	15.80	294.94	-	-	-	1.2046
2p2	-	15.50	295.0	-	-	-	1.2035
2p3	-	15.30	295.05	-	-	-	1.2029
2t1	-	16.03	293.36	-	-	-	1.2300
2t2	-	-	292.11	-	-	-	1.2508
2t3	-	-	289.90	-	-	-	1.2868
2t4	-	-	286.94	-	-	-	1.3353
2w1	-	-	294.89	19942 (95%)	-	-	1.2428
2w2	-	-	-	20992 (100%)	-	-	1.3121
2w3	-	-	-	22041 (105%)	-	-	1.3861
2w4	-	-	-	23091 (110%)	-	-	1.4547
2m1	-	-	-	19344 (92%)	1.22E5	-	1.2020
2m2	-	-	-	-	1.18E5	-	1.2092
2l1	-	-	-	-	1.2E5	Yes	1.2053
3f1	1.50255	-	-	-	-	No	1.4629

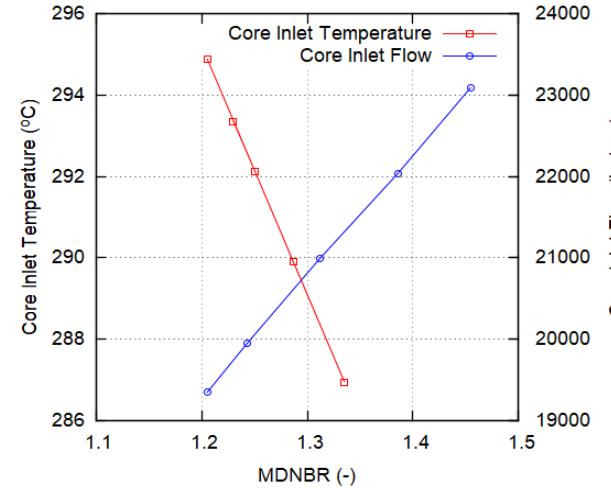
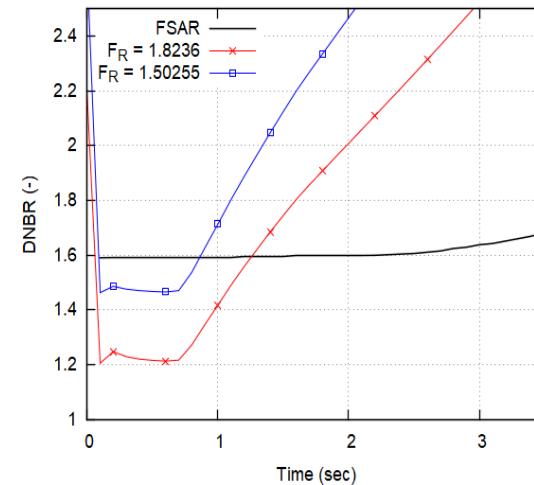
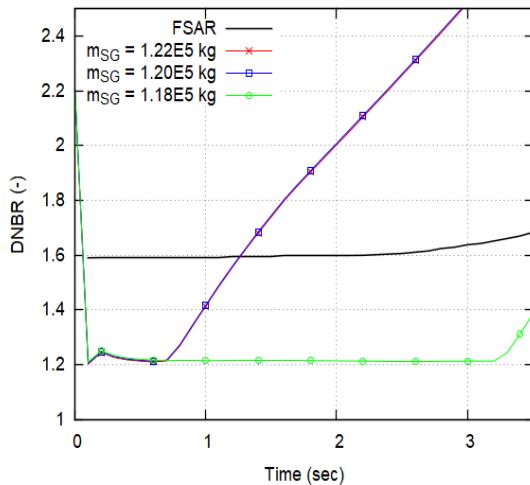
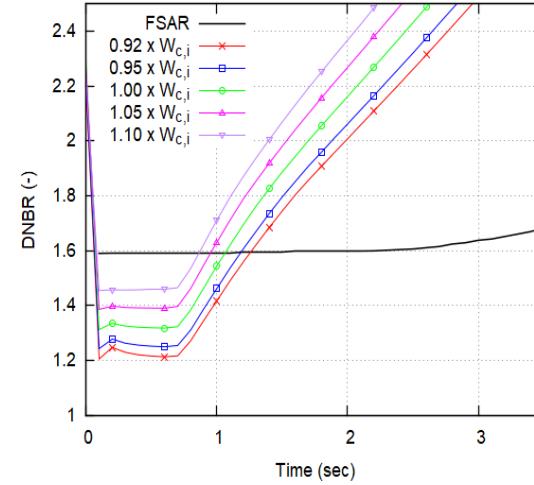
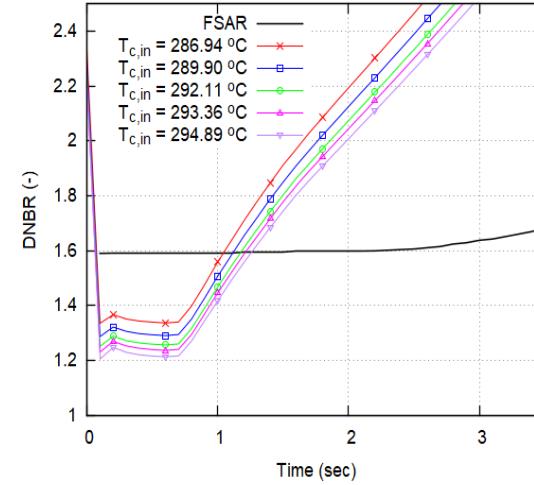
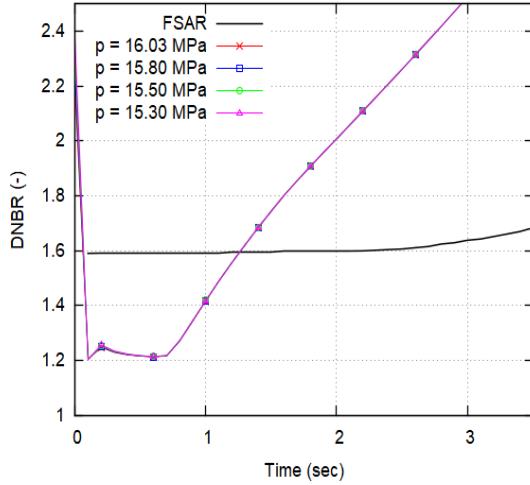
# Results – MSLB, Seized RCP Rotor



# Results – MFLB



# Results – SGTR



# Conclusion

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- **System code was unable to show the effect in detail on the RCS flow deviation in the MSLB and seized RCP rotor**
- **Thus, system code was not partially suitable to analyze the DNBR**
- **It is crucial to make sure the conservative initial and assumption for a regulatory safety review**
- **Thus, this study needs to analyze more operating parameters in the initial conditions to finalize the trend map in the near future**

원자력 안전  
KINS가 만들어 갑니다!



감사합니다



한국원자력안전기술원  
KINS KOREA INSTITUTE OF NUCLEAR SAFETY