

DHRS Cooling Effect Analysis of STELLA-2 using MARS-LMR



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01 Introduction

» STELLA Program Status

- ◆ Construction of large-scale integral effect test facility completed
- ◆ STELLA-2 facility is now operating and producing various experiment data
- ◆ Focus is on the DHRS performance

» Purpose



- ◆ To explore the limit and boundary condition of the facility
- ◆ To analyze the system behavior before actual experiment

» Scope

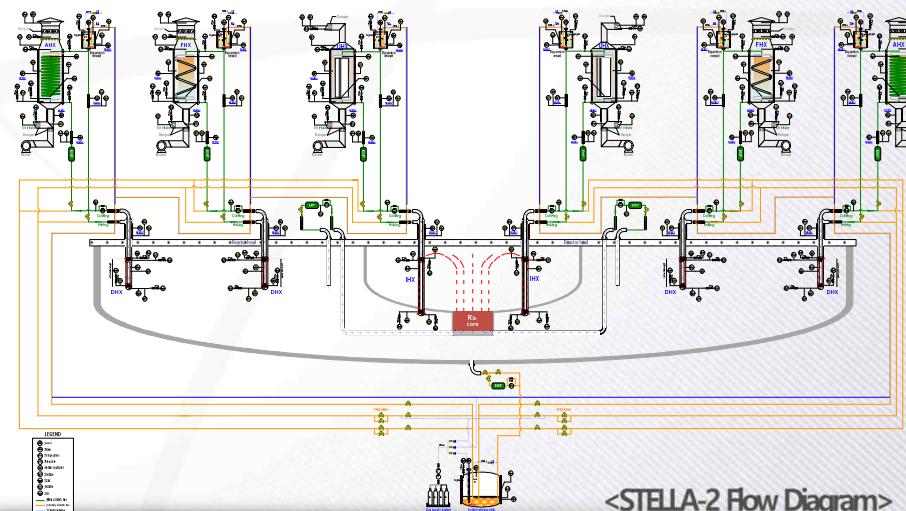
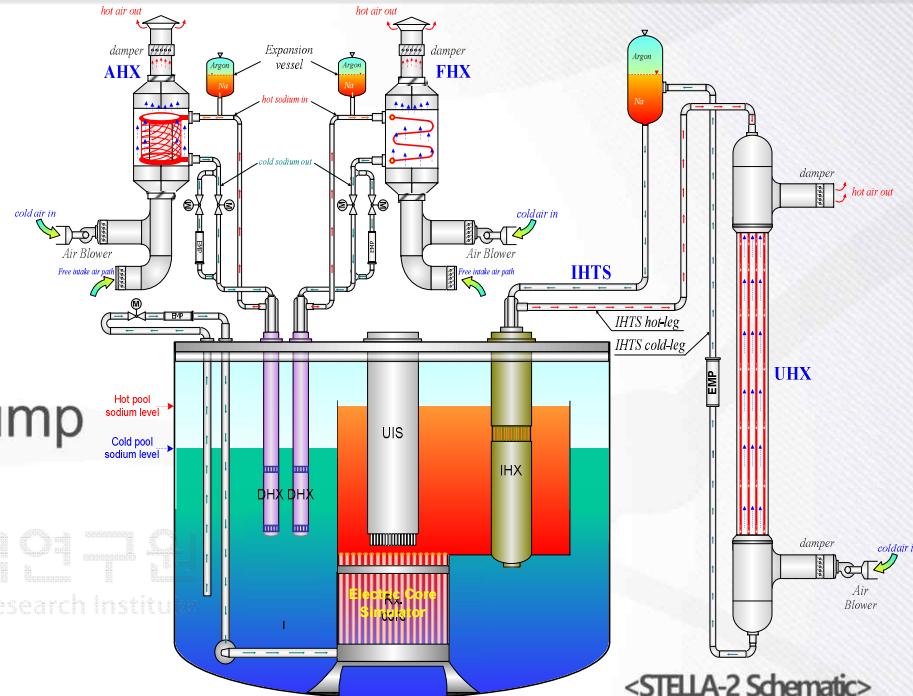
- ◆ DHRS cooling effect was analyzed using MARS-LMR code
- ◆ Scope of this study bounds in observation of the phenomena and discussion

02 STELLA-2 Facility

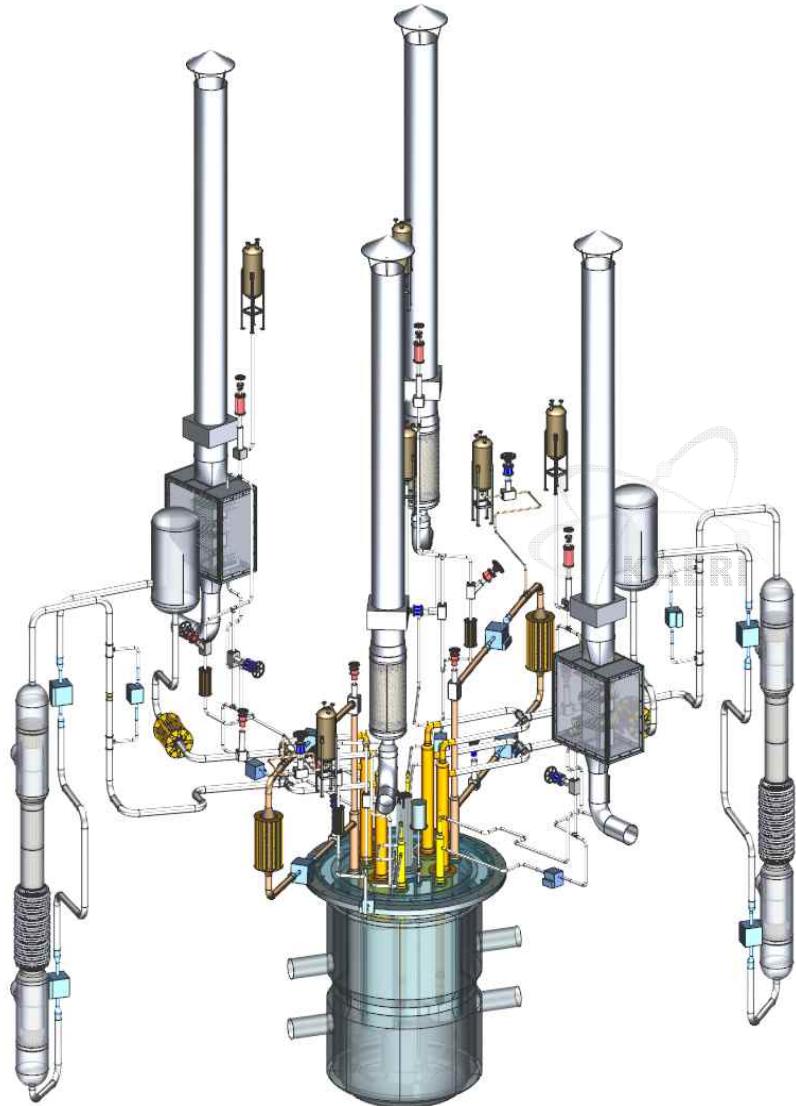
» General Description

- ◆ Conserves the transient behavior
- ◆ Includes all major components, except
 - (1) Nuclear fuel, (2) SG, (3) Mechanical pump

- ◆ Scale : 1/5 in length, 1/1 aspect ratio
- ◆ Sodium inventory : ~15 tons
- ◆ Design temp : 600°C
- ◆ Design press : 5 bar
- ◆ Total electric power : ~3 MW



02 STELLA-2 Facility



<STELLA-2 시험 장치 3D 모델링>



<STELLA-2 시험 장치 전경>

03 MARS-LMR Analysis

» Representative DBE : LOF + LOOP

- ◆ Loss of Flow (LOF) occurs when all primary pump power is lost
- ◆ Results in immediate temperature rise of coolant
- ◆ One of the main reason is Loss of Off-site Power (LOOP)

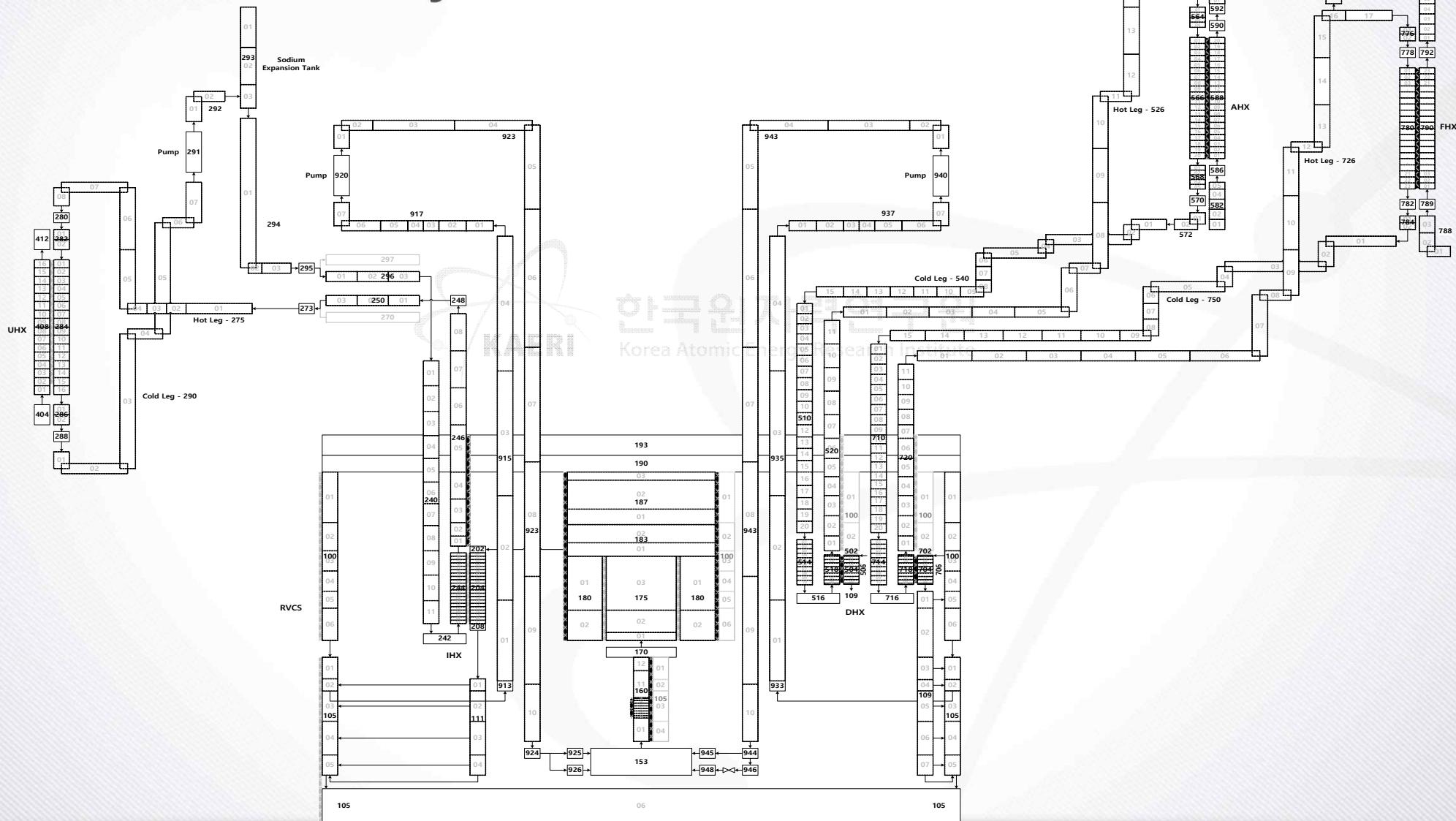
» Assumptions



- ◆ Steady-state point set to match the temperature distribution
- ◆ Transient starts with rapidly reducing the primary flow
- ◆ Intermediate loop flow also stops
- ◆ Core starts to follow decay heat curve
- ◆ Each one of HXs in ADHRS and PDHRS is not working
- ◆ Calculation done up to ~50,000 sec

03 MARS-LMR Analysis

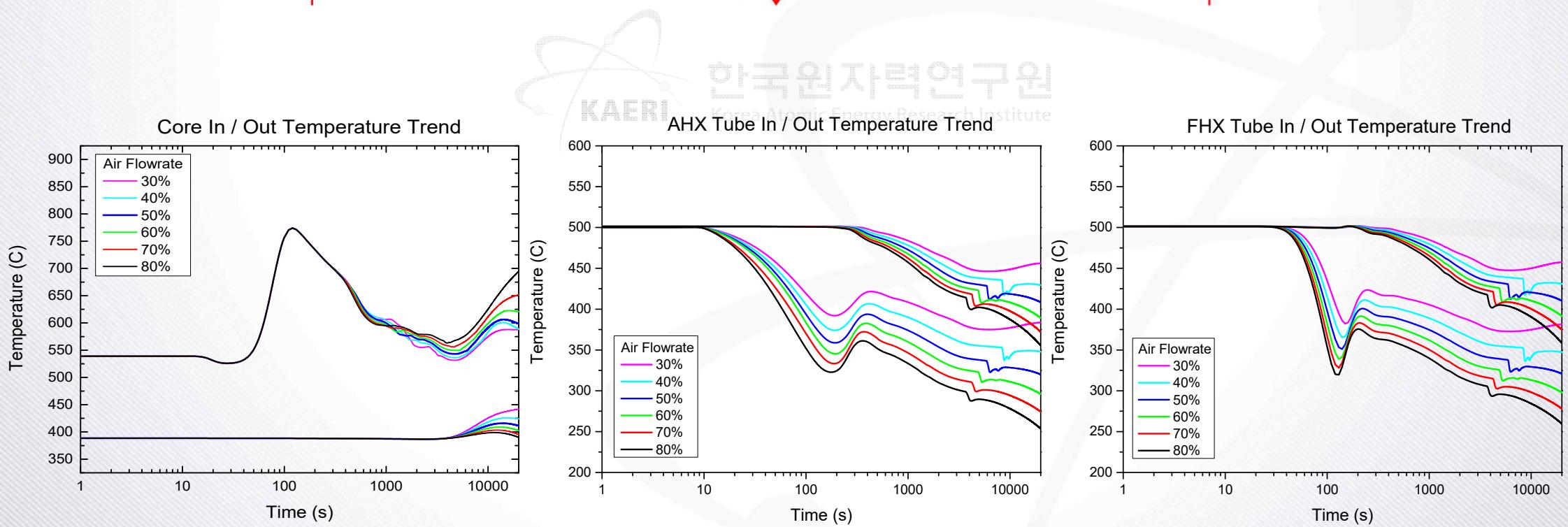
» MARS-LMR Node Layout



04 Results and Discussion

» Temperature Trend

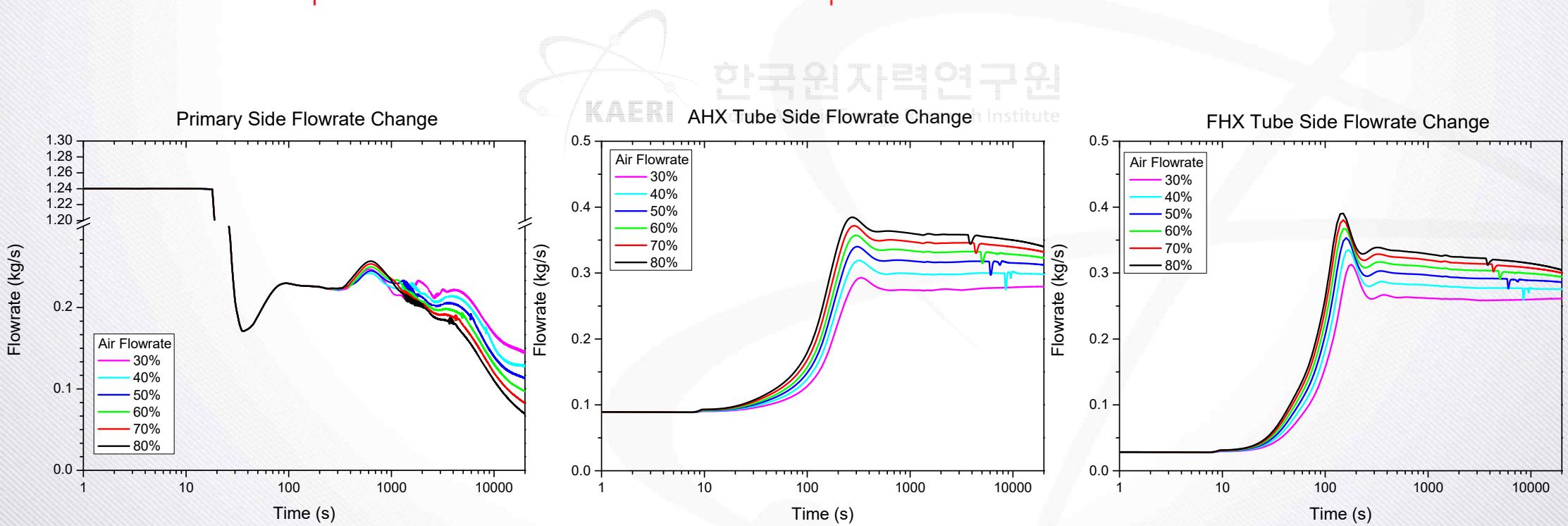
- ◆ Air flowrate of passive & active HXs controlled : 30 ~ 80 %
- ◆ Air flow $\uparrow \rightarrow$ core in/out $\Delta T \uparrow \rightarrow$ core out T \uparrow
- ◆ Air flow $\uparrow \rightarrow$ sodium T in DHRS $\downarrow \rightarrow$ HX tube in/out $\Delta T \uparrow$



04 Results and Discussion

» Flowrate Trend

- ◆ Air flowrate of passive & active HXs controlled : 30 ~ 80 %
- ◆ Air flow ↑ → natural circulation sodium(primary side) flow ↓
- ◆ Air flow ↑ → sodium flow in DHRs ↑



04 Results and Discussion

» Discussion

- ◆ Inconsistent with expectation on primary side
- ◆ Air flow ↑ \Rightarrow sodium flow ↓ \Rightarrow core out T ↑ (???)
- ◆ Cause of inconsistency
 - Thermal stratification at cold pool
 - From DHX shell out to the bottom of the pool
 - Axial conduction of coolant
 - High thermal conductivity of liquid sodium
 - 1D vs 3D
 - Node layout in code versus 3D mixing in real



05 Conclusion

- » STELLA-2 is ready for various transient experiments are on-going
- » DHRS cooling effect is one of the most important aspect
 - ◆ Observation by controlling the air flowrate of final HXs
 - ◆ The analysis results are inconsistent with the expectation
 - ◆ Cause of inconsistency
 - Thermal stratification
 - Axial conduction
 - 3D mixing effect
 - ◆ For verification, the experiment data will be needed



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06 Reference

- [1] J. Eoh et al., “Computer Codes V&V Tests with a Large-Scale Sodium Thermal-Hydraulic Test Facility (STELLA),” American Nuclear Society 2016 Annual Meeting, New Orleans, US, June 12-16, 2016.
- [2] J. Lee et al., “Design evaluation of large-scale sodium integral effect test facility (STELLA-2) using MARS-LMR”, Annals of Nuclear Energy, Vol. 120, pp.845-856, 2018.
- [3] J. Eoh, “Engineering Design of Sodium Thermal-hydraulic Integral Effect Test Facility (STELLA-2)”, KAERI SFR Design Report, SFR-720-TF-462-002Rev.00, 2015.

