

## Reactor System Technology D





# Derivation of Limit Stress Curve Equation

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# 01 Introduction

# 01 Introduction

## » Limit analysis

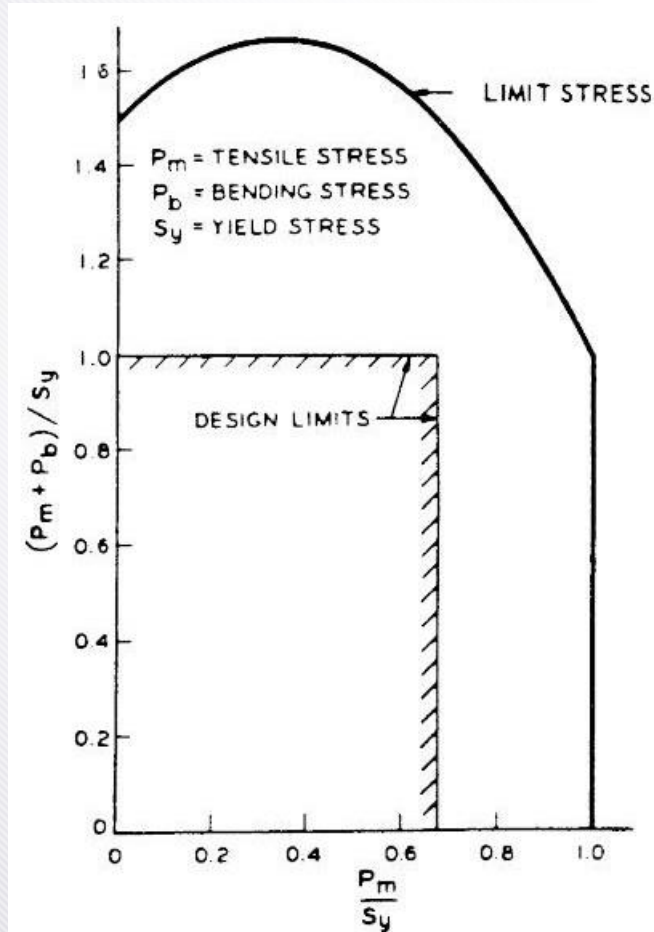
- For stress analysis, limit analysis is a special case of plastic analysis in which the material is assumed to be ideally plastic (nonstrain-hardening) [1].
- Using this assumption, the stress limit was developed by providing a margin on the actual limit load stress curve for combined tension and bending on a rectangular section [2].
- In this study, the limit stress curve equation is derived and the results are compared to reference.

# 02

## Methods and Results

# 02 Methods and Results

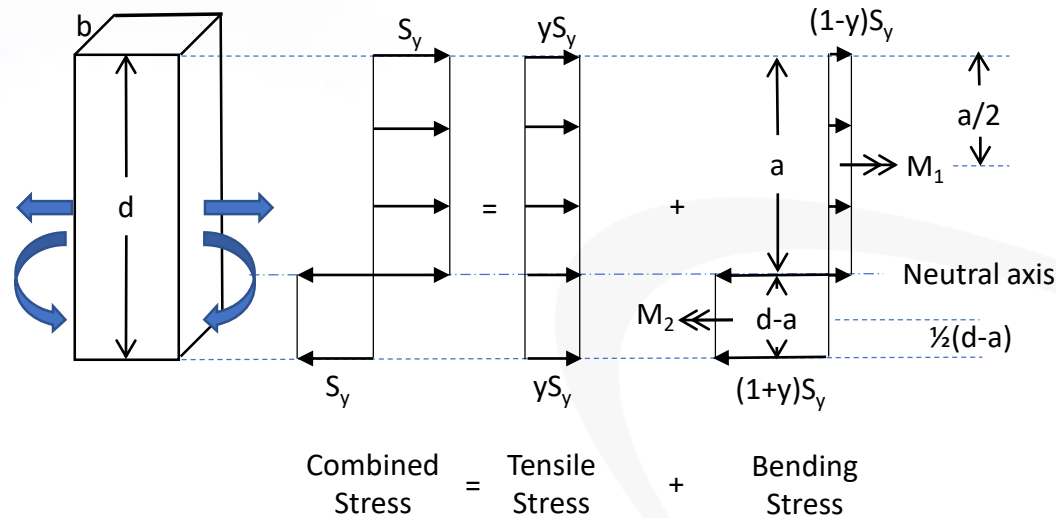
## » Limit stress curve



- Limit stress for combined tension and bending (rectangular section). (ASME, "Criteria," Courtesy of ASME)
- In limit analysis, the equilibrium and flow characteristics at the limit state are used to calculate the collapse load.
- In this figure, we can't know how the limit stress curve was drawn and what the exact coordinates were.
- From equilibrium equations, the limit stress curve equation can be derived.

# 02 Methods and Results

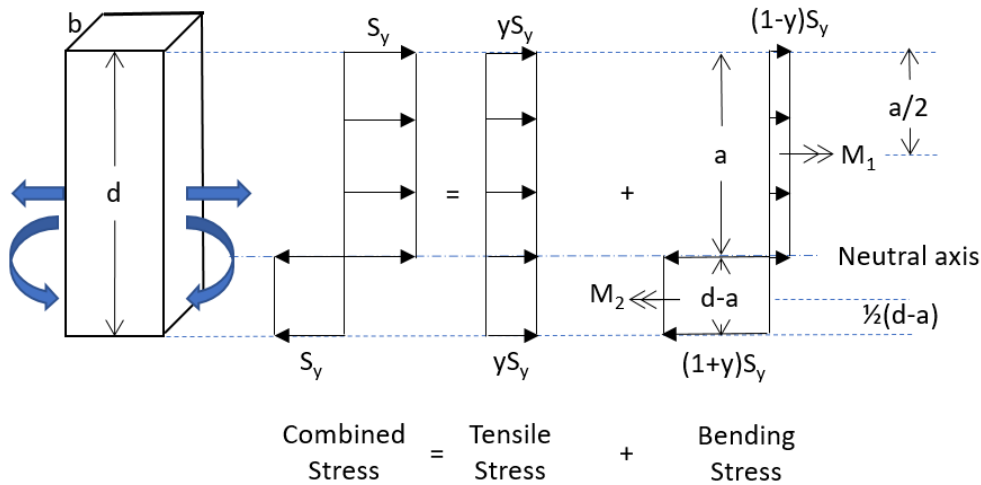
## » Decomposition of stress components



- A plastic hinge is an idealized concept used in Limit Analysis. In a beam or a frame, a plastic hinge is formed at the point where the moment, shear, and axial force lie on the yield interaction surface [1].
- In the perfectly plastic state, the cross section of the neutral axis is divided into two equal areas.

# 02 Methods and Results

## » Derivation of limit stress curve equation



$$(1-y)S_y \cdot a = (1+y)S_y \cdot (d-a) \quad (1)$$

$$\therefore a = \frac{d}{2}(1+y) \quad (2)$$

$$M_1 = (1-y)S_y \cdot ab \frac{a}{2} \quad (3)$$

$$M_2 = (1+y)S_y (d-a) \cdot b \frac{1}{2}(d-a) \quad (4)$$

$$\text{Moment } M = M_1 + M_2$$

$$= \frac{1}{2} S_y b \left\{ (1-y)a^2 + (1+y)(d-a)^2 \right\} \quad (5)$$

Substituting Eq. (2) in (5) gives

$$M = \frac{1}{4} S_y b d^2 (1-y^2) \quad (6)$$

$$\text{Tensile stress } P_m = yS_y, y = \frac{P_m}{S_y} \quad (7)$$

$$\text{Bending stress } P_b = \frac{M}{(bd^2)/6} \quad (8)$$

Substituting Eq. (8) in (6) gives

$$P_b = \frac{3}{2} S_y (1-y^2) \quad (9)$$

For the axes form of the limit stress curve, Eq. (7) and (9) gives

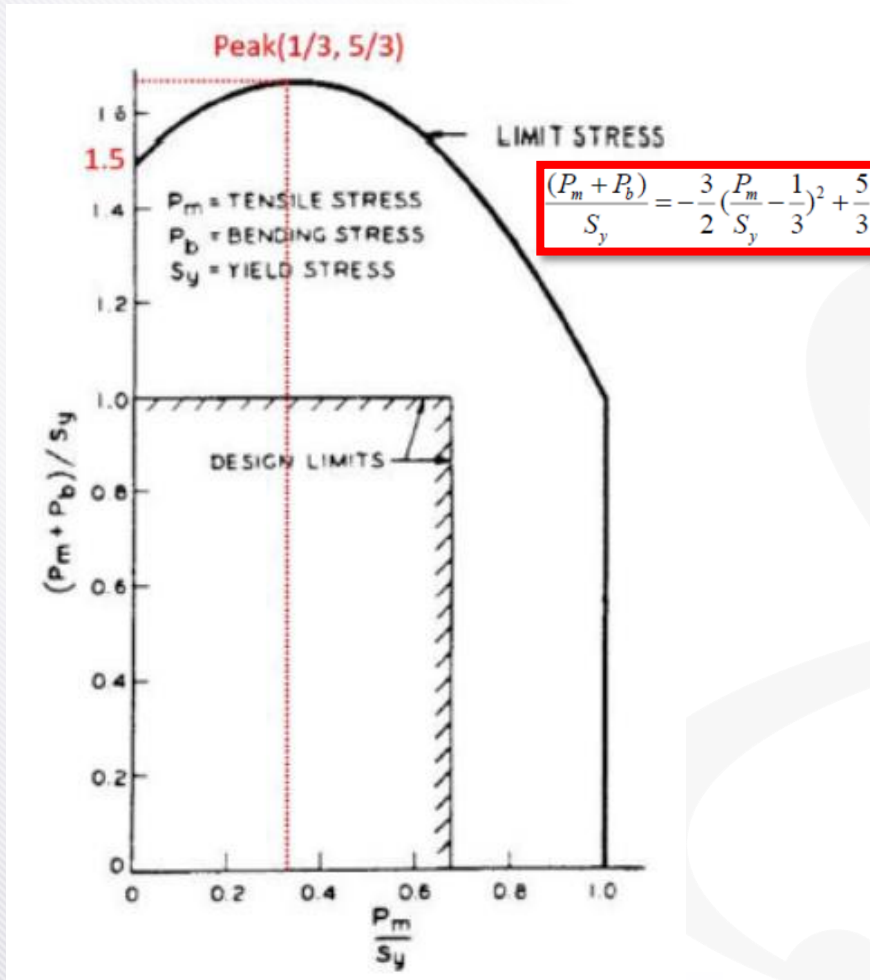
$$\frac{(P_m + P_b)}{S_y} = \frac{P_m}{S_y} + \frac{3}{2} \left\{ 1 - \left( \frac{P_m}{S_y} \right)^2 \right\} \quad (10)$$

$$\therefore \frac{(P_m + P_b)}{S_y} = -\frac{3}{2} \left( \frac{P_m}{S_y} - \frac{1}{3} \right)^2 + \frac{5}{3} \quad (11)$$



# 02 Methods and Results

## » Limit stress curve equation



- From this equation, we can understand the limit stress curve and analogize the whole out of a part.
- This figure indicates that the theoretical limit stress varies from 1.5  $S_y$  with no membrane stress present to 1.0  $S_y$  with only membrane stress present. It should be noted that the theoretical limit stress peaks at approximately 1.67 (=5/3) with a combination of bending and membrane stress when the membrane stress is approximately (1/3) $S_y$  [2].

# 03 Conclusions

# 03 Conclusions

- » In this study, the limit stress curve equation is derived from moment equilibrium and the results are compared to reference.
- » From the results, we can figure out the meaning and purpose of the limit stress.
- » This theoretical limit could be expanded to Class 2 and 3 Components.

# 04

## Acknowledgement & References

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## » Acknowledgements

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## » References

- [1] ASME Boiler and Pressure Vessel Code, Section III, Subsection NB, Class 1 Components, American Society of Mechanical Engineers, 2004.
- [2] K. R. Rao, Companion Guide to the ASME Boiler & Pressure Vessel Code, ASME Press, 2009.

**THANK YOU**