An Investigation into the Cause for the Hydrothermal Corrosion of Cr_xAl_{1-x} diffused CVD SiC

Hee Song_{a,b}, Dae-Jong Kim_a, Weon-Ju Kim_a, Ji-Yeon Park_a, Soon-Gil Yoon_b, Hyeon-Geun Lee_a*

^aNuclear Material Research Division, Korea Atomic Energy Research Institute,

111 Daedeok-daero-989, Yuseong-gu, Daejeon 34057

b Department of Materials Science and Engineering, Chungnam national University, Daejeon, Korea

*Corresponding author: hglee@kaeri.re.kr

1. Introduction

A silicon carbide (SiC)-based ceramics and their composites (SiC fiber-reinforced SiC matrix composite, SiC_f/SiC) have excellent high temperature strength, low neutron absorption cross-section, irradiation stability, and minimization of hydrogen generation. That is, they have excellent thermal and mechanical stability. Therefore, they have been studied for the application as an accident tolerant fuel cladding. However, the SiC composites have the critical problem, hydrothermal corrosion under normal operating conditions of LWR. It is known that SiC has excellent corrosion resistance at high temperature due to the formation of a SiO₂, protective layer. However, the hydrothermal corrosion of SiC in LWR environment is accelerated because the SiO₂ protective layer dissolves in the coolant with hightemperature and high-pressure conditions. [1, 2]

$$SiO_2 + 4H_2O \rightarrow HSiO_3^- + H^+ \rightarrow SiO_3^{2-} + 2H^+$$

$$Si(OH)^4 \rightarrow H_3SiO_2^- + H^+ \rightarrow H_2SiO_2^{2-} + 2H^+$$

The corrosion of SiC occurs in surface but in a grain boundary with relatively high energy. The corrosion is shown to accelerate while the grain boundary corrosion proceeds to selective dissolution of SiC grain. Thus, the corrosion resistance of SiC should be improved to apply SiC composites cladding. A metallic element with good corrosion resistance is diffused into CVD SiC to prevent changing from SiC into SiO₂. This study aims to investigate whether the diffused metal improves the corrosion resistance of CVD SiC.

2. Methods and Results

2.1 Material and specimen preparation

The SiC composite cladding to be applied to LWR is a CVD SiC-coated triplex or duplex structure to overcome corrosion resistance and safety. Therefore, the specimens used in the experiments was CVD SiC. Also, the metallic elements to be diffused were selected as Cr_xAl_{1-x} , Cr, and Al. The metals were coated on SiC substrates, and then diffused into SiC through heat treatment. [3] Table.1 specifies experimental conditions for manufactured specimens. The metal-coated SiC specimens were heat treated in Argon atmosphere for four hours at 1500-1800°C. [4, 5] The diffusion behavior of metallic elements in CVD SiC was investigated by SIMS, and the depth of diffusion was known through a depth analysis. The SIMS results are shown in Figure 1. All the specimens were confirmed that the diffusion of metallic elements occurred, and Al diffusion rate is Cr_xAl_{1-x} diffused SiC> Al diffused SiC at 1800°C> Al diffused SiC at 1500°C and Cr diffusion rate is Cr diffused SiC> Cr_xAl_{1-x} diffused SiC.

Table 1 Experimental conditions.

#	Coating materials	coating method	heating condition		corrosion condition
			(Ar atmosphere)		(360°C, 19MPa)
			temp.(°C)	time(hr)	time(hr)
1	CrAl	arc ion plating	1800	4	12
2	Cr	arc ion plating	1800	4	12
3	Al	sputtering	1500	4	12
4			1800	4	12



Figure 1 Depth profile of metallic elements diffused SiC.

2.2 Variation of Weight and Microstructure by Corrosion Experiment

The specimens were experimented using an autoclave, an accelerated corrosion simulation instrument without DO, DH control. Also, an experimental condition of autoclave is 360 °C, 19MPa, 12hr. Each specimen was separately tested with CVD SiC(reference) to prevent the interaction of metal ions produced by corrosion reactions. The weight loss by corrosion test is shown in Figure 2. The weight loss ratio was CVD SiC>Al diffused SiC at 1800 °C >Al diffused SiC at 1500 °C >Cr diffused SiC> Cr_xAl_{1-x} diffused SiC, and all specimens are showed lower weight loss than CVD SiC. Among them, Cr_xAl_{1-x} diffused SiC is showed the lowest weight loss. Figure 3 shown comparison of the corroded surface microstructure. It is shown that the corroded area of metallic elements diffused specimens is smaller than the CVD SiC.



Figure 2 Weight loss of CVD SiC in the hydrothermal corrosion environments.



Figure 3 SEM micrograph of as-SiC (a, b, c) and Cr_xAl_{1-x} diffused SiC (d, e, f) after corrosion test (360°C, 19Mpa, 12hr).

2.3 Analysis of XPS before and after corrosion



Figure 4 XPS spectra of CVD SiC before corrosion test. (a) Overview, (b) C1s, (c) O1s, (d) Si2p. XPS spectra of CVD

SiC after corrosion test (360°C, 19Mpa, 12hr). (e) Overview, (f) C1s, (g) O1s, (h) Si2p.

Figure 4 shows the chemical states at the surface of CVD SiC before and after the corrosion test by XPS analysis. After corrosion, the O1s peak is decreased. It able to interpret the dissolution of SiO2. The surface of CVD SiC is reacted with oxygen, and it is formed the thin SiO2 passive film. And in consequence, Figure 4 (c) shows the high intensity of peak of Si Oxide. However, the Si oxide layer is dissolved in the hydrothermal environment, O1s peak is decreased like Figure 4 (g). Figure 5 shows the XPS spectra of metallic elements diffused SiC (Cr_xAl_{1-x}) before and after corrosion test. In contrast to the results of the CVD SiC, the intensity of O1s increased. It is attributed the increase in intensity of oxygen to the oxidation of Cr and Al. Also, the metal peaks that existed before the corrosion were lost, and then the oxides and hydroxide were created or increased through corrosion test. These results are considered that a Si oxide containing Cr and Al is not soluble in hydrothermal environment and inhibit corrosion reaction of SiC.



Figure 5 XPS spectra of Cr_xAl_{1-x} diffused SiC before corrosion test. (a) Overview, (b) C1s, (c) O1s, (d) Si2p, (e) Cr2p, (f) Al2p. XPS spectra of Cr_xAl_{1-x} diffused SiC after corrosion test (360°C, 19Mpa, 12hr). (g) Overview, (h) C1s, (i) O1s, (j) Si2p, (k) Cr2p, (l)Al2p

2.4 Corrosion behavior analysis of CVD SiC



Figure 6 TEM image of CVD SiC(a, b) and Cr_xAl_{1-x} diffused SiC(c, d) after corrosion test (360°C, 19Mpa, 12hr).

The corrosion behavior of CVD SiC can be found in the thesis of K.A. Terrani et al. (2015). In the hydrothermal LWR coolant atmosphere, SiC is oxidized and the produced silica is dissolved in the coolant. In Figure 6(a, b), the oxide layer is not visible in the TEM image after corrosion of the CVD SiC. Because the dissolving rate is faster than the generation rate of silica. However, Cr_xAl_{1-x} diffused SiC can see a thin layer of oxidation throughout the surface (Figure 6(c, d)). It is judged that the diffusion of Cr_xAl_{1-x} has affected the corrosion behavior of the CVD SiC. In Figure 7, the oxide layer component is shown as the silica, but as a result of XPS, there is an oxide of Cr and Al. In addition, only the result of SiC, which diffused metal elements, remains an oxide layer after corrosion. These results are considered that an oxide in the form of Cr-Al-O and Si-Cr-Al-O inhibited corrosion reaction of SiC. Compared with the weight loss by corrosion of Cr diffused SiC, Al diffused SiC, and CrxAl1-x diffused SiC, the oxidation layer that made in CrxAl1-x diffused SiC more effective than Cr-O or Al-O. As a result, it is considered that oxidation in the form of Cr-Al-O and Si-Cr-Al-O has a good effect to improve the corrosion resistance of SiC.



Figure 7 TEM-EDS lining image of Cr_xAl_{1-x} diffused SiC after corrosion test (360°C, 19MPa, 12hr).

3. Conclusions

Under the conditions simulating LWR, the effect of Addition of Cr and Al into CVD SiC on Hydrothermal Corrosion Behavior was investigated. The SiC was corroded as Si oxide that forms in pressurized hot water environment had been dissolved. In addition, the sensitivity of grain boundaries to oxidation is high, the corrosion of SiC is accelerated the corrosion of SiC with grains detach. Thus, a trace element of Cr and Al was diffused into SiC to improve the corrosion resistance of SiC. Weight loss of metallic elements diffused SiC was reduced than CVD SiC. With the addition of Cr and Al into SiC, the oxide layer formed by the reaction with the coolant, Si oxide layer containing Cr and Al, is judged to inhibit the oxidation reaction of SiC. Thus, this study established that the diffusion of Cr_xAl_{1-x} into SiC inhibits corrosion of SiC.

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