A Proposed New Framework for Nuclear Reactor Physics Analysis with Transport Calculation

- Invited -

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- **1.** Nuclear Reactor Analysis Methods
- 2. HIRE-Theoretic Multigroup Transport Equations
- **3.** New Framework for Reactor Analysis
 - **General Sectrum Characteristics of Two Reactor Types**
 - Global / Local Decomposition
 - LWRs
 - FNRs
- 4. Summary and Concluding Remarks
- **5.** References



1. Nuclear Reactor Analysis Methods

Current Status

- Assembly or pincell transport (many-group) + Whole-core diffusion theory (few-group)
 - "Multigroup" cross section library
 - \checkmark Space is simplified.
 - $\checkmark\,$ Resonance self-shielding methods : suppositions and heuristics
- Assembly or pincell transport (many-group) + Whole-core transport theory (few-group)
- Whole-core Monte Carlo (continuous-energy) : emerging,

event-wise first principles, but brute force

- Time and memory
- Variance
- "Convergence" and acceleration



1. Nuclear Reactor Analysis Methods

Proposed New Framework

- Local : Continuous-energy MC (with albedo parameterized boundary conditions)
- Global : <u>H</u>omogeneity and <u>I</u>sotropy <u>Re</u>storation (HIRE)-theoretic
 "multigroup" (few-group) transport equations
- Two templates : LWRs

FNRs



□ Continuous-energy neutron transport equation is rigorously derived as:

$$egin{aligned} ec{\Omega} \cdot
abla arphi(ec{r},E,ec{\Omega}) + \sigma_t(ec{r},E)arphi(ec{r},E,ec{\Omega}) &= \int d\Omega' \int dE' \sigma_s(ec{r},E' o E,ec{\Omega}' o ec{\Omega}) arphi(ec{r},E',ec{\Omega}') \ &+ rac{\chi(E)}{k_{eff}} \int d\Omega' \int dE'
u \sigma_f(ec{r},E') arphi(ec{r},E',ec{\Omega}'). \end{aligned}$$

□ To obtain corresponding multigroup transport equations, Eq. (1) is integrated over an energy interval $E_g \leq E \leq E_{g-1}$ leading to:

$$egin{aligned} ec{\Omega} \cdot
abla arphi_g(ec{r},ec{\Omega}) + \sigma_{t,g}(ec{r},ec{\Omega}) arphi_g(ec{r},ec{\Omega}) &= \sum_{g'=1}^G \int d\Omega' \sigma_{s,gg'}(ec{r},ec{\Omega}' o ec{\Omega}) arphi_{g'}(ec{r},ec{\Omega}') \ &+ rac{\chi_g}{k_{eff}} \sum_{g'=1}^G
u \sigma_{f,g'}(ec{r}) \phi_{g'}(ec{r}), \end{aligned}$$

where the standard notations are used.



 \Box Note that the group total cross section in Eq. (2) becomes angle-dependent as:

$$\sigma_{t,g}(ec{r},ec{\Omega}) = rac{\int_{E_g}^{E_{g-1}} dE \sigma_t\left(ec{r},E
ight) arphi(ec{r},E,ec{\Omega})}{\int_{E_g}^{E_{g-1}} dE arphi(ec{r},E,ec{\Omega})}.$$
(3)

□ We note in Eq. (2) that $\sigma_{t,g}$ and $\sigma_{s,gg'}$ become also \vec{r} dependent, even in a homogenized region.



□ HIRE theory : On reaction terms in Eq. (2), we perform, over V_m of material region m,

$$\sigma_{t,g}(\vec{r},\vec{\Omega}) = \frac{\int_{E_g}^{E_{g-1}} dE \sigma_t(\vec{r},E)\varphi(\vec{r},E,\vec{\Omega})}{\int_{E_g}^{E_{g-1}} dE \varphi(\vec{r},E,\vec{\Omega})}, \qquad (3)$$

$$\sigma_{t,g}^m = \frac{\int_{\vec{r}\in V_m} dV \int d\Omega \int_{E_g}^{E_{g-1}} dE \sigma_t(\vec{r},E)\varphi(\vec{r},E,\vec{\Omega})}{\int_{\vec{r}\in V_m} dV \int d\Omega \int_{E_g}^{E_{g-1}} dE \varphi(\vec{r},E,\vec{\Omega})}, \qquad (3a)$$



□ HIRE theory : On reaction terms in Eq. (2), we perform, over V_m of material region m,

$$\sigma_{t,g}^{m} = \frac{\int_{\vec{r} \in V_{m}}^{} dV \int d\Omega \int_{E_{g}}^{E_{g-1}} dE \sigma_{t}(\vec{r}, E) \varphi(\vec{r}, E, \vec{\Omega})}{\int_{\vec{r} \in V_{m}}^{} dV \int d\Omega \int_{E_{g}}^{E_{g-1}} dE \varphi(\vec{r}, E, \vec{\Omega})},$$
(3a)

$$\sigma_{s,gg'}(\vec{r},\vec{\Omega}'\rightarrow\vec{\Omega}) = \frac{\int_{E_g}^{E_{g-1}} dE \int_{E_{g'}}^{E_{g'-1}} dE' \sigma_s(\vec{r},E'\rightarrow E,\vec{\Omega}'\rightarrow\vec{\Omega})\varphi(\vec{r},E',\vec{\Omega}')}{\int_{E_{g'}}^{E_{g'-1}} dE'\varphi(\vec{r},E',\vec{\Omega}')}, \quad (4)$$

$$\sigma_{s0,gg'}^{m} = \frac{\int_{\vec{r}\in V_{m}} dV \int d\Omega \int_{E_{g}}^{E_{g-1}} dE \int d\Omega' \int_{E_{g'}}^{E_{g'-1}} dE' \sigma_{s}(\vec{r},E'\to E,\vec{\Omega}'\to\vec{\Omega})\varphi(\vec{r},E',\vec{\Omega}')}{\int_{\vec{r}\in V_{m}} dV \int d\Omega \int d\Omega' \int_{E_{g'}}^{E_{g'-1}} dE' \varphi(\vec{r},E',\vec{\Omega}')},$$
(4a)



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$$\nu \sigma_{f,g'}(\vec{r}) = \frac{\int d\Omega' \int_{E_{g'}}^{E_{g'-1}} dE' \nu \sigma_f(\vec{r}, E') \varphi(\vec{r}, E', \vec{\Omega}')}{\int d\Omega' \int_{E_{g'}}^{E_{g'-1}} dE' \varphi(\vec{r}, E', \vec{\Omega}')}$$
(5)
$$\nu \sigma_{f,g'}^m = \frac{\int_{\vec{r} \in V_m} dV \int d\Omega \int d\Omega' \int_{E_{g'}}^{E_{g'-1}} dE' \nu \sigma_f(\vec{r}, E') \varphi(\vec{r}, E', \vec{\Omega}')}{\int_{\vec{r} \in V_m} dV \int d\Omega \int d\Omega' \int_{E_{g'}}^{E_{g'-1}} dE' \varphi(\vec{r}, E', \vec{\Omega}')},$$
(5a)

$$\chi_g^m = \frac{\int_{\vec{r} \in V_m} dV \int d\Omega \int_{E_g}^{E_{g-1}} dE \int d\Omega' \sum_{g'=1}^G \int_{E_{g'}}^{E_{g'-1}} dE' \chi(E) \nu \sigma_f(\vec{r}, E') \varphi(\vec{r}, E', \vec{\Omega}')}{\int_{\vec{r} \in V_m} dV \int d\Omega \int d\Omega' \sum_{g'=1}^G \int_{E_{g'}}^{E_{g'-1}} dE' \nu \sigma_f(\vec{r}, E') \varphi(\vec{r}, E', \vec{\Omega}')}.$$
(6a)



Multigroup Transport Equations

- Eq. (2) becomes, after averaging over each material region and integrating over angle,

$$\frac{1}{V_m} \int_{\partial V_m} dA \vec{n} \cdot \vec{J}(\vec{r}) + \sigma^m_{t,g} \phi^m_g = \sum_{g'=1}^G \sigma^m_{s0gg'} \phi^m_{g'} + \frac{\chi^m_g}{k_{eff}} \sum_{g'=1}^G \nu \sigma^m_{f,g'} \phi^m_{g'} .$$
(7)

$$ext{ where } ec{J}_{_g}(ec{r}) = \int \ d\Omega ec{\Omega} arphi(ec{r},ec{\Omega}), \ \ \phi^m_{_g} = rac{1}{V_{_m}} \int_{ec{r} \in V_m} dV \phi_{_g}(ec{r}) \ .$$

Eq. (2) is then recast in the following multigroup equations with cross sections of Eqs.
 (3a)-(6a):

$$ec{\Omega}\cdot
abla arphi_{g}(ec{r},ec{\Omega})+\sigma^{m}_{t,g}arphi_{g}(ec{r},ec{\Omega})=\sum_{g'=1}^{G}\sigma^{m}_{s0gg'}\phi_{g'}(ec{r})+rac{\chi^{m}_{g}}{k_{e\!f\!f}}\sum_{g'=1}^{G}
u\sigma^{m}_{f,g'}\phi_{g'}(ec{r}),$$

with albedo boundary condition $\varphi_g(ec{r},ec{\Omega}')=lpha_k arphi_g(ec{r},ec{\Omega})\;k=1\; ext{to}\;4.$

- Eq. (8) is the multigroup transport equations, derived in this paper.
- Only σ_{s0} term remains : a byproduct
- Eigenvalue and material region-wise flux distributions, as such obtained with the usual continuity conditions, will show discrepancies compared to those from the continuous-energy calculation. ⇔ PCDF

 Γ_2

 Γ_3

(8)

□ Partial Current Discontinuity Factor (PCDF)

- To preserve the reference neutron leakages, PCDF is introduced to each outgoing and incoming current with respect to material region surface k (Γ_k , k=1 to 8) as:

where $f_{g,k}^{\pm}$ are initially guessed and updated by PCDF iterations.







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 \Leftrightarrow

2. HIRE-Theoretic Multigroup Transport Equations

Update of PCDFs

Partial currents obtained from the multigroup transport solution:

$$egin{aligned} J_{g,k}^+ &= \int_{ec r \in \Gamma_k} dA {\int_{ec \Omega \cdot ec n_k > 0} d\Omega \left| ec n_k \cdot ec \Omega
ight| arphi_g(ec r, ec \Omega), } (10 \mathrm{a}) \end{aligned} \ J_{g,k}^- &= {\int_{ec r \in \Gamma_k} dA {\int_{ec \Omega \cdot ec n_k < 0} d\Omega \left| ec n_k \cdot ec \Omega
ight| arphi_g(ec r, ec \Omega). } (10 \mathrm{b}) } \end{aligned}$$

Discontinuity in partial currents:

$$ilde{m{J}}^{-}_{g,k} = m{f}^{-}_{g,k} m{J}^{-}_{g,k}, ext{(11a)}$$

$$ilde{m{J}}_{g,k}^+ = m{f}_{g,k}^+ m{J}_{g,k}^+. ext{(11b)}$$

Conditions on the updated PCDFs:

$$m{J}_{g,k}^{ref} = m{J}_{g,k}^+ - ilde{m{J}}_{g,k}^- = m{J}_{g,k}^+ - m{f}_{g,k}^- m{J}_{g,k}^-$$

$$m{J}_{g,k}^{ref} = ilde{m{J}}_{g,k}^+ - m{J}_{g,k}^- = m{f}_{g,k}^+ m{J}_{g,k}^+ - m{J}_{g,k}^-$$

Fig. 2. Leakage corrections based on PCDFs at interface k.

Reference surface net current $J_{a,k}^{ref}$ from the continuous-energy MC calculation

$$\Leftrightarrow \qquad f_{g,k}^{-} = \frac{J_{g,k}^{+} - J_{g,k}^{ref}}{J_{g,k}^{-}}, \qquad (12a)$$
$$\Leftrightarrow \qquad f_{g,k}^{+} = \frac{J_{g,k}^{-} + J_{g,k}^{ref}}{J_{g,k}^{+}}. \qquad (12b)$$



PCDF Iteration Scheme







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- □ Spectrum Characteristics of Two Reactor Types
 - Spectrum characteristics



Fig. 4. Comparison of neutron energy spectra.

– Mean free paths

 $\lambda_{\scriptscriptstyle LWR} < \lambda_{\scriptscriptstyle FNR}$



Global/Local Decomposition

– LWR



Fig. 5. Unit problem in a light water reactor.

- Local problem : Continuous-energy MC on a square pin-cell (with parameterized albedos)
- Global problem : Two-group

MOC (2-D), $MOC/S_N 2D/1D$ Fusion (3-D) Two-Level p-CMFD acceleration



3. New Framework for Reactor Analysis

– FNR



Fig. 6. Unit problem in a fast reactor.

- Local problem : Continuous-energy MC on a hexagon (with parameterized albedos)
- Global problem : Eight (possibly four) group

 S_N method (2-D, 3-D) + KBA parallel sweep procedures Two-Level p-CMFD acceleration



4. Summary and Concluding Remarks

Summary

- Homogeneity and Isotropy Restoration (HIRE) theory:
 - Provides "multigroup" transport equations with PCDFs
 - ✓ Angle-independent total XS
 - ✓ Material region-wise homogeneous XS (restoration of homogeneity)
 - \checkmark In scattering terms, only σ_{s0} term remains in the multigroup transport equations.
 - Partial current discontinuity factors (PCDFs) are introduced to preserve the neutron leakages at material interfaces.
- Global/Local Decomposition Framework
 - Local: Continuous-energy MC: square pin-cell for LWRs

hexagonal fuel assembly for FNRs

• Global: HIRE-"multigroup" transport: G = 2 for LWRs, G = 8 for FNRs

4. Summary and Concluding Remarks

Concluding Remarks

- The volume of integration for material region (V_m) can be chosen as:
 - 1) A multi-region such as pin-cell homogenization or baffle-reflector homogenization
 - 2) Resolved regions such as rings in a fuel rod for i) rim effect in depletion
 - ii) fuel temperature feedback effect
- HIRE-multigroup cross sections and PCDFs could be tabulated or functionalized in :
 - 1) α values (representing the environment)
 - 2) Burnup
 - 3) Fuel and moderator temperatures
- The resulting "multigroup" transport equations can be solved by existing numerical methods: MOC, S_N method

Sweeping procedures

Acceleration methods



5. References

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Thank you!