
The Rationale of Leakage Parameters adopted in Leakage Feedback Method

KNS 2018 Autumn Meeting at Yeosu

2018. 10. 26. Fri.

Ban Young Suk* and Joo Han Gyu

Seoul National University

Reactor Physics Lab

***ysban0130@snu.ac.kr**

Contents

- **Introduction**
 - **Advanced Leakage Feedback Method**
 - **Topic: The Rationale of Leakage Parameters**

- **Leakage-to-removal ratio (Leakage Fraction)**

- **Fast-to-thermal flux ratio (Spectral Index)**

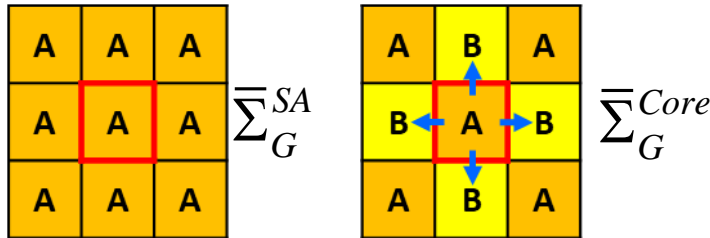
- **Evaluation of Fitting Formulas**

- **Conclusions**

Introduction

□ Concept of Leakage Feedback Method

- Group Constants (GC) difference proportional to leakage



SA: Single Assembly
All Reflective B.C.

$$\frac{\bar{\Sigma}_G^{Core} - \bar{\Sigma}_G^{SA}}{\bar{\Sigma}_G^{SA}} \propto Leakage$$

□ Advanced Leakage Feedback Method

$$\frac{\bar{\Sigma}_G - \bar{\Sigma}_G^{SA}}{\bar{\Sigma}_G^{SA}} = \alpha_G l_1 + \beta_G l_2 + \gamma_G \Delta\Gamma$$

- Inner Assembly (IA) : $\gamma = 0$
- Peripheral Assembly (PA)* : $\gamma \neq 0$
 - Special treatment on PA = PAT

Leakage Fraction (LF)
: leakage-to-removal ratio

$$l_G = \left(\sum_{surf} J_G^{surf} A_{surf} \right) / \left(\int_{Asy} \Sigma_{r,G} \phi_G dV \right)$$

Spectral Index Shift (SIS)
: fast-to-thermal flux ratio

$$\Delta\Gamma = \frac{\phi_1}{\phi_2} - \frac{\phi_1^{SA}}{\phi_2^{SA}}$$

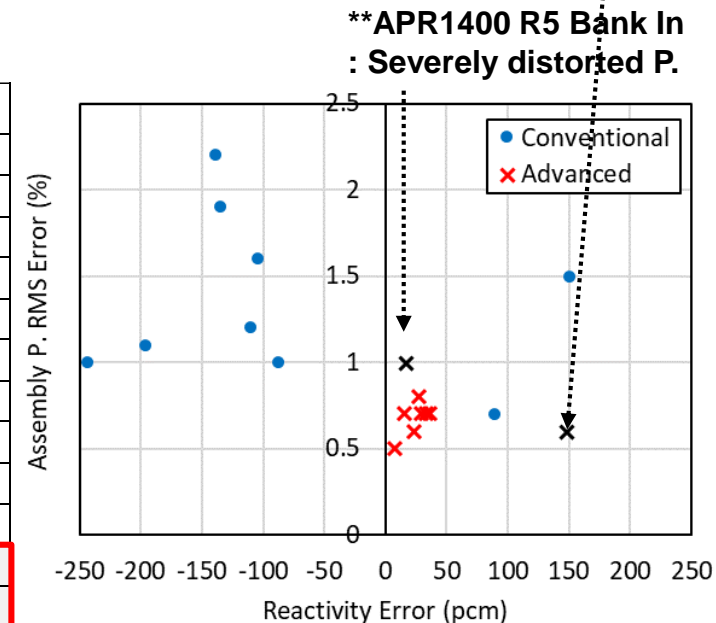
Validation of LFM for Various Cores

Targeted Cores Problems

- Assembly type: 16x16 pin (CE type), 17x17 pin (WH type: BEAVRS, VERA)
- Core size: 100 MW (SMR), 1000 MW (AP1000), 1400 MW (APR1400) *APR1400 EOC : Simplified depletion
- Core state: Depletion, HZP, HFP, Control rod insertion

Summary of Two-step Results compared with DWC results*

Case		$\Delta\rho$ (pcm)		RMS Error (%)		Max Error (%)	
		Conv.	Adv.	Conv.	Adv.	Conv.	Adv.
APR1400	BOC	-196	36	1.1	0.7	2.1	1.6
	*EOC	89	148	0.7	0.6	1.3	1.2
	HFP	-244	8	1.0	0.5	1.9	1.1
	HZP	-135	15	1.9	0.7	4.6	1.6
	**CR-R5	-139	16	2.2	1.0	7.8	4.4
VERA-2D		-110	23	1.2	0.6	2.9	1.6
BEAVRS-S2D		-88	29	1.0	0.7	2.2	1.9
AP1000-2D		150	27	1.5	0.8	2.7	2.0
SMR-2D		-105	33	1.6	0.7	3.2	1.0
*, **RMS Avg.		156	26	1.4	0.7	2.9	1.6
Ratio		6.0		2.0		1.9	



	Conventional Two-Step	Advanced Two-step
Time Cost	< 2 sec	< 2 sec
Reactivity	~ 150 pcm	~ 25 pcm
Assembly Power	RMS: 1.5 %, Max: 3.0 %	RMS: 0.7 %, Max: 1.5 %

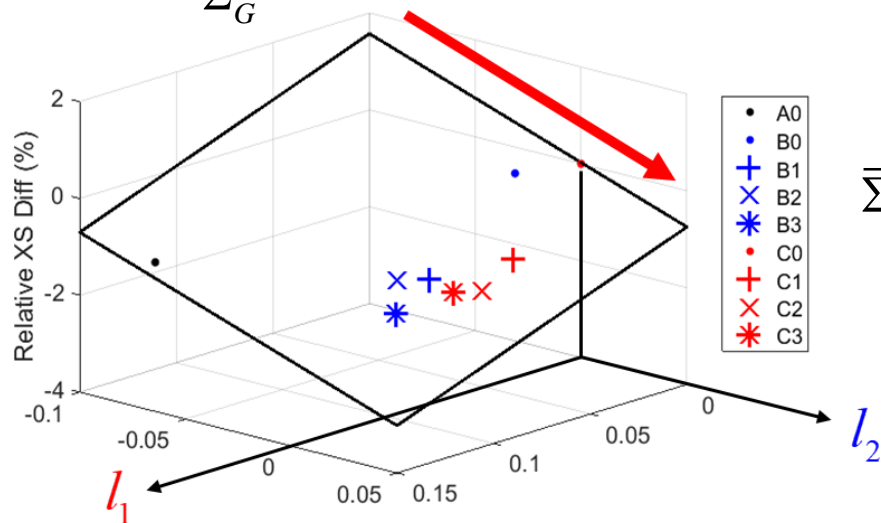
Motivation and Topic

□ Thermal LF dependency of Fast GCs

C0	X
X	C0

- APR1400 C0 assembly, down-scattering XS

$$\frac{\bar{\Sigma}_G^{CB} - \bar{\Sigma}_G^{SA}}{\bar{\Sigma}_G^{SA}} = \alpha_G l_1 + \beta_G l_2$$



$$\bar{\Sigma}_G^* = \sum_{g \in G} \bar{\Sigma}_g^* \tilde{\phi}_g^* \quad \text{Normalized flux within group G} \quad \sum_{g \in G} \tilde{\phi}_g^* = 1$$

$$\Delta \bar{\Sigma}_g = \bar{\Sigma}_g^* - \bar{\Sigma}_g^{SA}, \quad \Delta \tilde{\phi}_g = \tilde{\phi}_g^* - \tilde{\phi}_g^{SA}$$

$$\bar{\Sigma}_G^* = \sum_{g \in G} (\bar{\Sigma}_g^{SA} + \Delta \bar{\Sigma}_g) (\tilde{\phi}_g^{SA} + \Delta \tilde{\phi}_g)$$

$$= \sum_{g \in G} (\bar{\Sigma}_g^{SA} \tilde{\phi}_g^{SA} + \tilde{\phi}_g^{SA} \Delta \bar{\Sigma}_g + \bar{\Sigma}_g^{SA} \Delta \tilde{\phi}_g + \Delta \bar{\Sigma}_g \Delta \tilde{\phi}_g)$$

$$= \bar{\Sigma}_G^{SA} + E_G^{Hom} + E_G^{Con} + O(E^2)$$

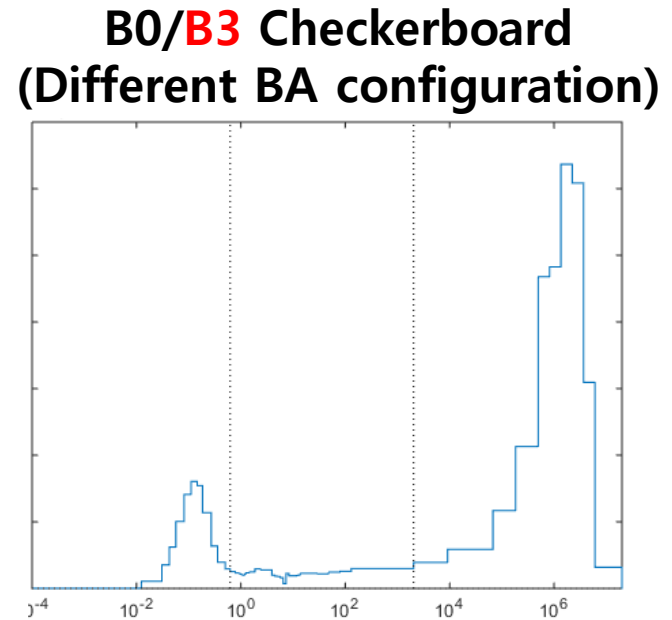
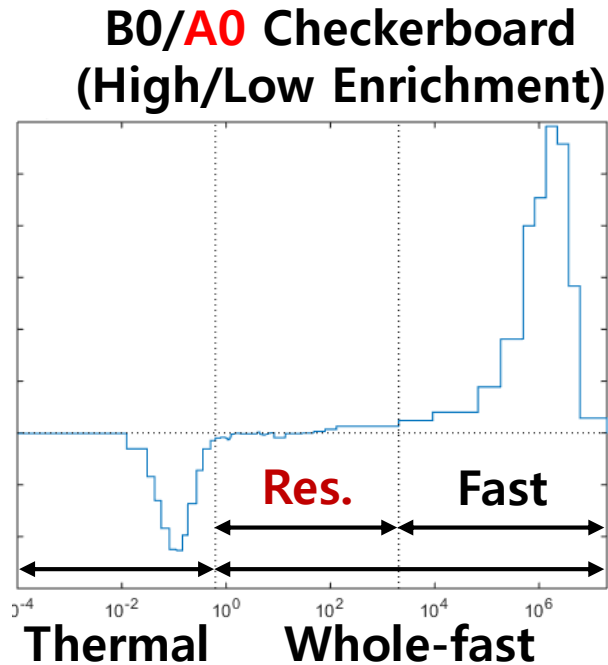
$$\bar{\Sigma}_G^{LFM} = \bar{\Sigma}_G^{SA} (1 + \alpha_G l_1 + \beta_G l_2 + \gamma_G \Delta \Gamma)$$

$g \notin G$ does not appear in the formula \rightarrow How thermal LF affect Fast GC?

Physical meaning of leakage parameters?

Intermediate Group Leakage

□ Leakage spectrum of B0 from checkerboards

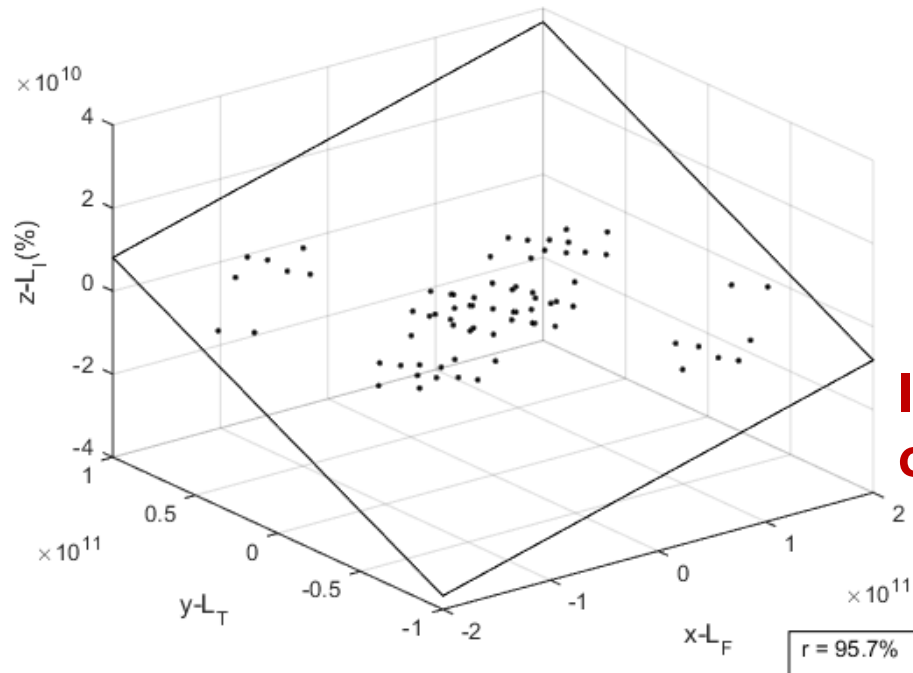


- Fast leakage : shape of fission spectrum
- Thermal leakage : shape of thermal peak
- Different characteristic of intermediate range leakage

Correlation of L_R with L_F , L_T

□ Leakage points from checkerboards

- X: Fast Leakage Fraction
- Y: Thermal Leakage Fraction
- Z: Intermediate(resonance range) Leakage Fraction



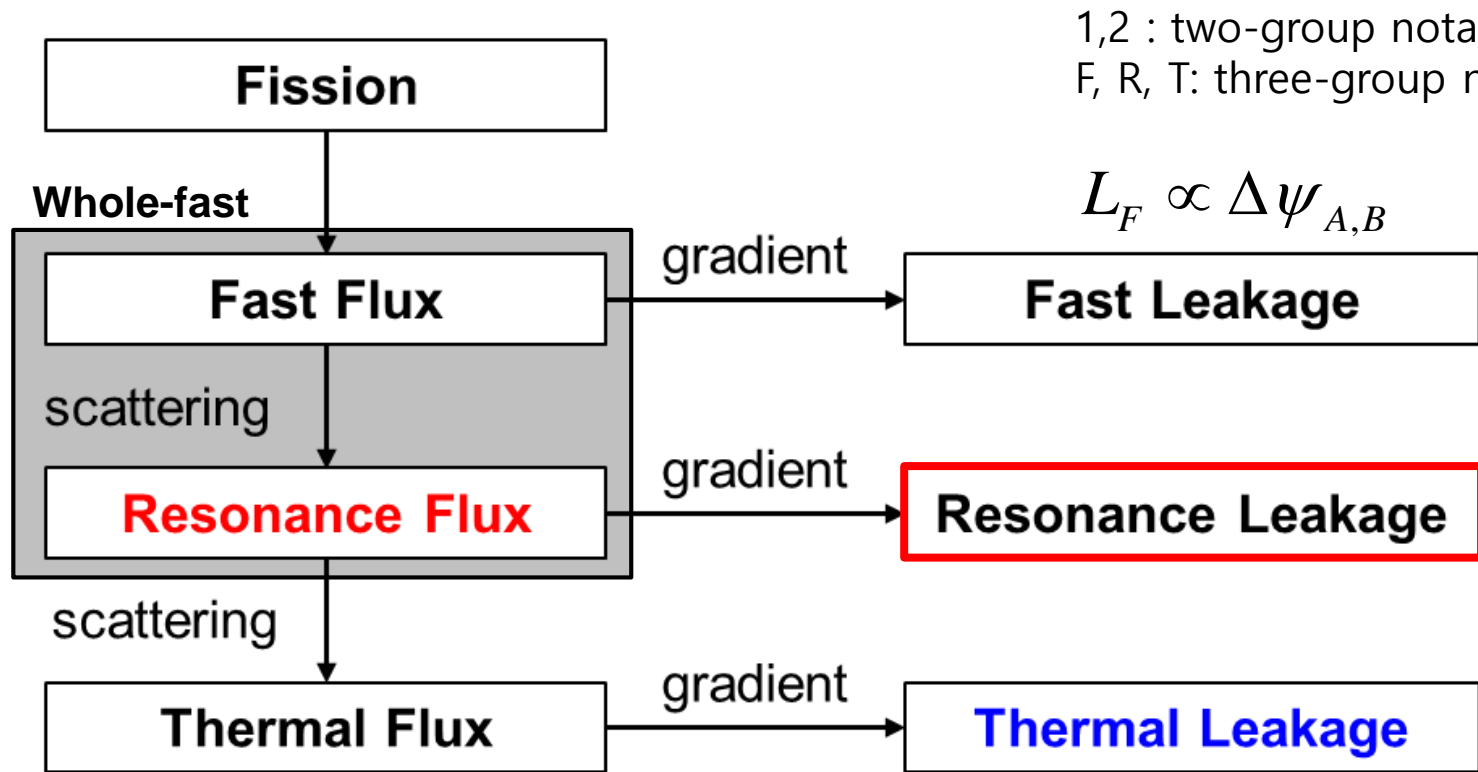
$$L_R \approx \alpha L_F + \beta L_T$$

$$\alpha = 0.0715$$

$$\beta = 0.2242, R^2 = 95.7\%$$

Intermediate leakage depends on fast and thermal leakage

Thermal Lkg. as Indirect Representation



* Thermal leakage = indirect representation of resonance flux or lkg. through its consequence

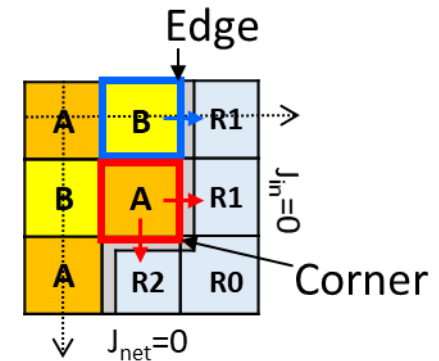
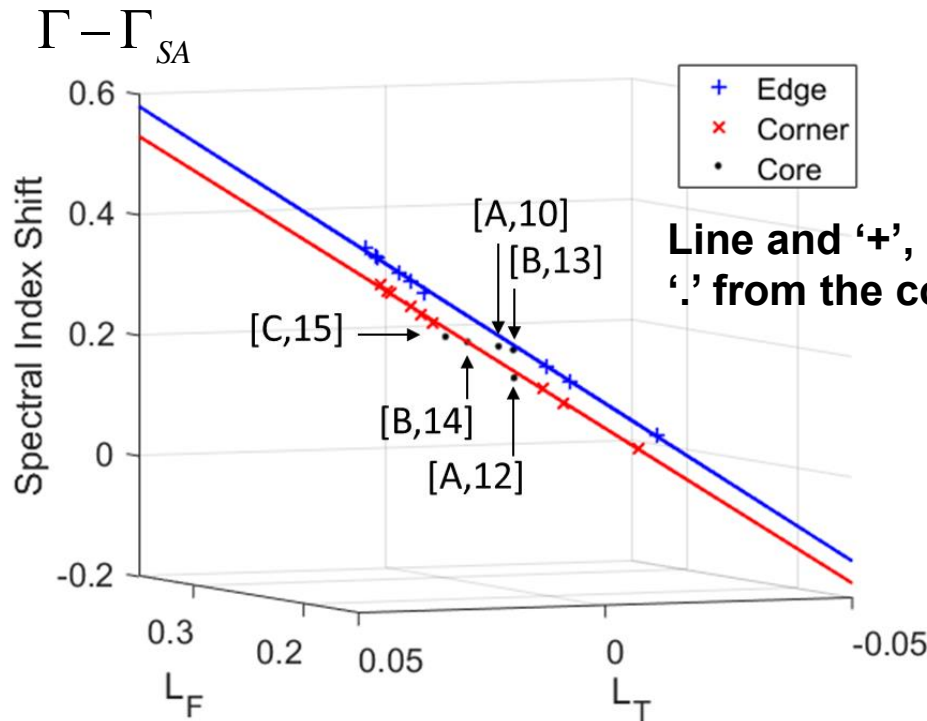
$$\Delta\Gamma = \frac{\phi_1}{\phi_2} - \frac{\phi_1^{SA}}{\phi_2^{SA}}$$

Spectral Index Shift for PAT

Peripheral Assembly Treatment

- Edge: facing 1 side toward reflector
 - Corner: facing 2 sides toward reflector
- Different SIS tendency

	J	H	G	F	E	D	C	B	A	R
9	A0	A0	C3	A0	B1	A0	B3	C2	B0	R1
10	A0	B3	A0	B3	A0	B1	A0	B3	C0	R1
11	C3	A0	C2	A0	C3	A0	C3	B1	B0	R1
12	A0	B3	A0	B3	A0	B3	A0	B2	C0	R1
13	B1	A0	C3	A0	C2	A0	B1	C0	R2	R0
14	A0	B1	A0	B3	A0	B3	C1	C0	R1	
15	B3	A0	C3	A0	B1	C1	C0	R2	R0	
16	C2	B3	B1	B2	C0	C0	R2	R0		
17	B0	C0	B0	C0	R2	R1	R0			
18	R1	R1	R1	R1	R0					



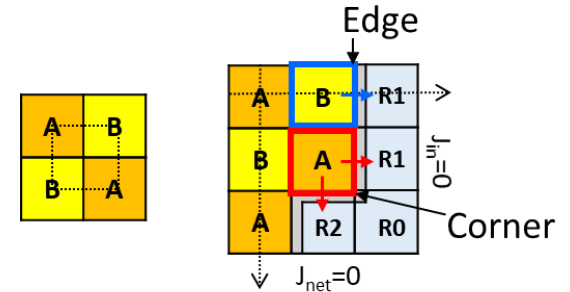
SIS = the index of leakage through reflector side

$$\frac{\bar{\Sigma}_G - \bar{\Sigma}_G^{SA}}{\bar{\Sigma}_G^{SA}} = \alpha_G l_1 + \beta_G l_2 + \gamma_G \Delta\Gamma$$

Evaluation of Fitting Formulas

□ Fitting of Few-Group Constants

- Least square fitting, linear
- Fitting base points from colorsets
 - N points from CBs, 5N points from 3x3 config.



□ Definition of GC Error

- Target problem: 2D APR1400 (B3, C0)
- Relative RMS error of evaluated XS

$$E = \sqrt{\sum_i^N \left(\frac{\Sigma_{Core}^i - \Sigma(L_{Core}^i)}{\Sigma_{Core}^i} \right)^2 / N}$$

□ Fitting Parameter Sets

- L_{F+R}, L_T (LFM)
- $L_{F+R}, \Delta\Gamma$ (SIS instead of L_T)
- L_F, L_R (Impractical)
- L_{F+R}, L_T, δ (Biased fitting)
- $L_{F+R}, L_T, \Delta\Gamma$ (LFM+PAT)

	J	H	G	F	E	D	C	B	A	R
9	A0	A0	C3	A0	B1	A0	B3	C2	B0	R1
10	A0	B3	A0	B3	A0	B1	A0	B3	C0	R1
11	C3	A0	C2	A0	C3	A0	C3	B1	B0	R1
12	A0	B3	A0	B3	A0	B3	A0	B2	C0	R1
13	B1	A0	C3	A0	C2	A0	B1	C0	R2	R0
14	A0	B1	A0	B3	A0	B3	C1	C0	R1	
15	B3	A0	C3	A0	B1	C1	C0	R2	R0	
16	C2	B3	B1	B2	C0	C0	R2	R0		
17	B0	C0	B0	C0	R2	R1	R0			
18	R1	R1	R1	R1	R0					

$\Sigma_{Core}^i, L_{Core}^i$

: Evaluated GCs and LF from the reference DWC solution

$\Sigma(L_{Core}^i)$

: Evaluated LFM GCs with LF from the reference

Errors of Evaluated GCs

□ Inner Assembly – B3

Goodness of Fitting

Fit. Para.	D_l	Σ_{al}	Σ_{fl}	Σ_{l2}
l_1, l_2	0.991	0.983	0.941	0.981
$l_1, \Delta\Gamma$	0.993	0.987	0.958	0.987
l_F, l_R	0.997	0.997	0.996	1.000
l_1, l_2, δ	0.994	0.988	0.952	0.984
$l_1, l_2, \Delta\Gamma$	0.999	1.000	1.000	1.000

Evaluated RMS Error (10^{-5})

Fit. Para.	D_l	Σ_{al}	Σ_{fl}	Σ_{l2}
l_1, l_2	13	30	42	59
$l_1, \Delta\Gamma$	13	25	39	49
l_F, l_R	18	11	17	21
l_1, l_2, δ	10	31	45	63
$l_1, l_2, \Delta\Gamma$	17	10	26	16

- L_F, L_R case well estimated GCs → L_T = indirect parameter!

□ Peripheral Assembly – C0

Goodness of Fitting

Fit. Para.	D_l	Σ_{al}	Σ_{fl}	Σ_{l2}
l_1, l_2	0.712	0.676	0.692	0.768
$l_1, \Delta\Gamma$	0.752	0.750	0.814	0.850
l_F, l_R	0.927	0.972	0.990	0.999
l_1, l_2, δ	0.712	0.676	0.695	0.769
*Edge	0.993	0.998	0.973	0.996
*Corner	0.938	0.976	0.992	0.994
$l_1, l_2, \Delta\Gamma$	0.990	0.999	0.984	1.000

Evaluated RMS Error (10^{-5})

Fit. Para.	D_l	Σ_{al}	Σ_{fl}	Σ_{l2}
l_1, l_2	122	418	219	609
$l_1, \Delta\Gamma$	120	390	179	519
l_F, l_R	45	100	15	35
l_1, l_2, δ	121	412	211	595
l_1, l_2, δ^*	65	174	62	233
$l_1, l_2, \Delta\Gamma$	24	21	18	28

- *Edge&Corner separate functionalization works fine
- $L_{F+R}, L_T, \Delta\Gamma$ (LFM+PAT) shows the best result

Conclusions

- **Study on the rationales of leakage parameters**
- **Thermal leakage fraction in fast GCs**
 - Indirect representation of the effect of intermediate range neutrons through its consequence in thermal leakage
- **Spectral Index Shift**
 - Representation of spectrum inside the whole-fast group
 - **Using SIS always improves accuracy of evaluated GCs**
 - **For Peripheral Assembly**
 - A proper index of leakage through reflector (Edge and Corner PA)
 - **For Inner Assembly**
 - L_F and L_T dependent, must be reconsidered when few # of colorset

Details of updated method and results for various cases will be presented in the upcoming paper