
Experimental Investigation of Condensation with Bundle Geometry for the Passive Containment Cooling System

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Jinhoon Kang^a, Dongwook Jerng^b, Byongjo Yun^{a*}

^a*Mechanical Engineering Department, Pusan national Univ., Jangjeon-dong, Guemjeong-gu, Busan,*

^b*School of Energy Systems Engineering, Chung-Ang Univ., Heukseok-dong, Dongjak-gu, Seoul,*



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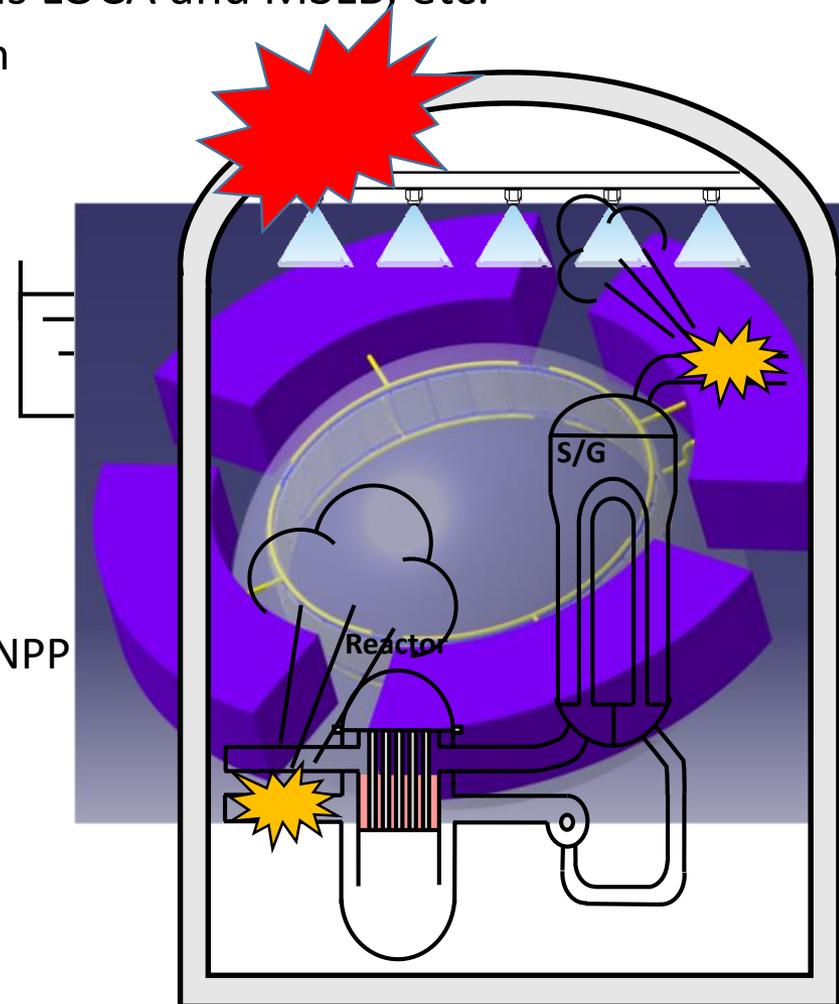


Introduction (1)



■ Background

- In case of postulated accidents such as LOCA and MSLB, etc.
 - High pressure and high energy steam releases to containment building.
 - Containment is threatened by released steam.
- Passive containment cooling system
 - Replacement of active containment spray system
 - Bundle type condensation heat exchanger
 - Considered in the Korean advanced NPP such as APR+ and IPOWER.
- Previous investigations
 - Condensation experiments for plate and single tube



Introduction (2)

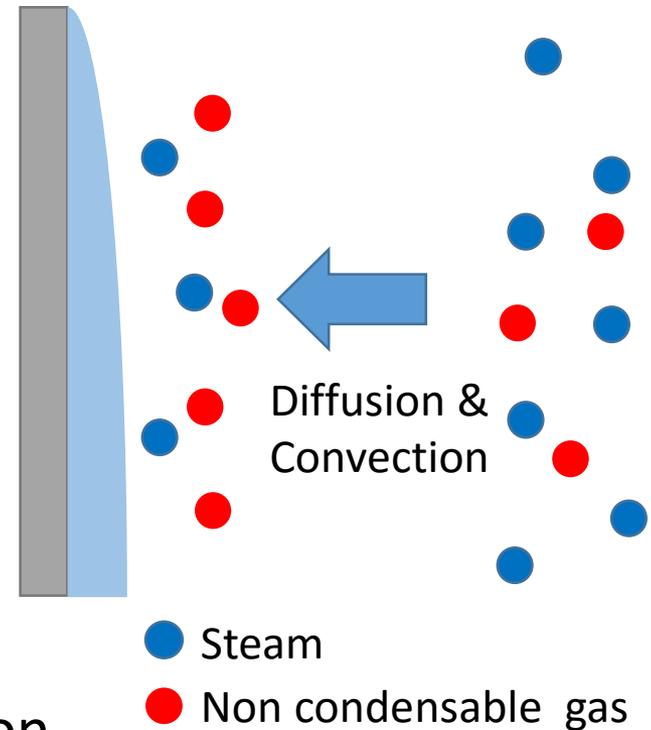


■ Objects of Experiments

- Condensation phenomena of bundle
- Effect of parameters
 - Suction of steam
 - Screening of steam by adjacent tubes
 - Geometric effects
 - Inclination
 - Pitch to diameter (p/d)

■ Development of condensation correlation

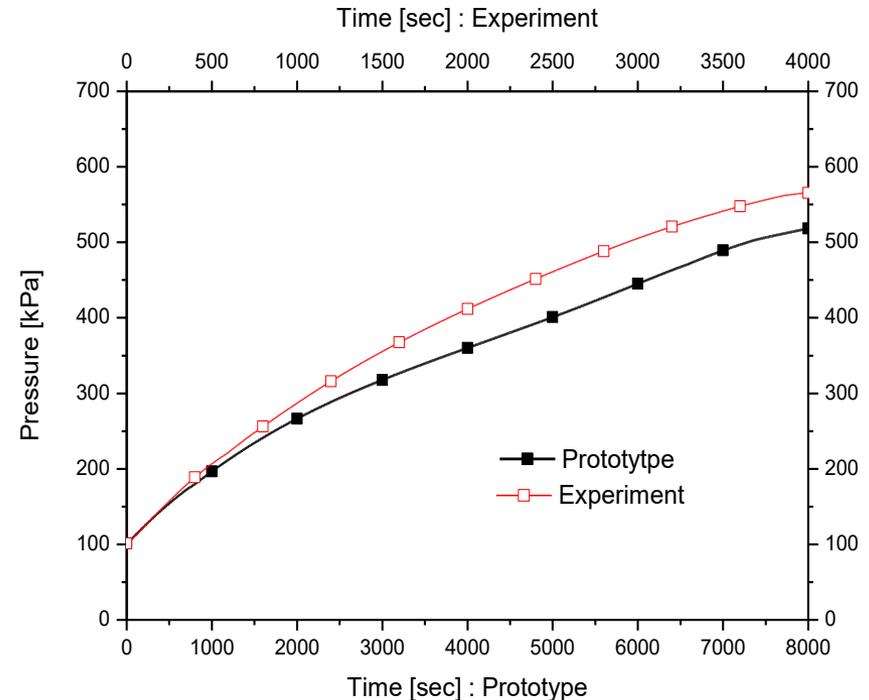
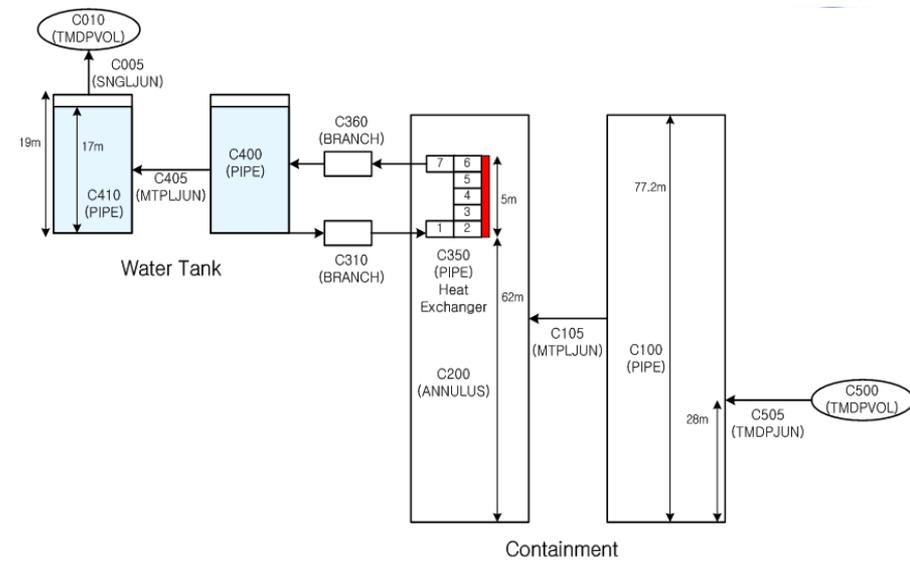
- Correction of deviation between experimental data for bundle and existing correlation for single tube



Experimental Facility (1)

Scaling analysis

Parameter	Scaling Law	Scaling ratio	Value (Proto/Test)
Tube Diameter(OD/ID)	$l_{OR}^{1/2}$	1/2	(40/34) / (21.5/15.5)
Heat Flux Ratio	1/1	1/1	24.35kw/m ²
Height Ratio	l_{OR}	1/4	5/1.25m
Tube Number Ratio	$a_{OR}l_{OR}^{-1}$	1/8032	3ea
Containment Volume Ratio	$a_{OR}l_{OR}$	1/42837	2.18m ³
Total Heat Removal Ratio	$a_{OR}l_{OR}^{1/2}$	1/21418	122885kW/ 5.737kW



< Analysis results of containment >
pressure with ideal scaling

Experimental Facility (2)



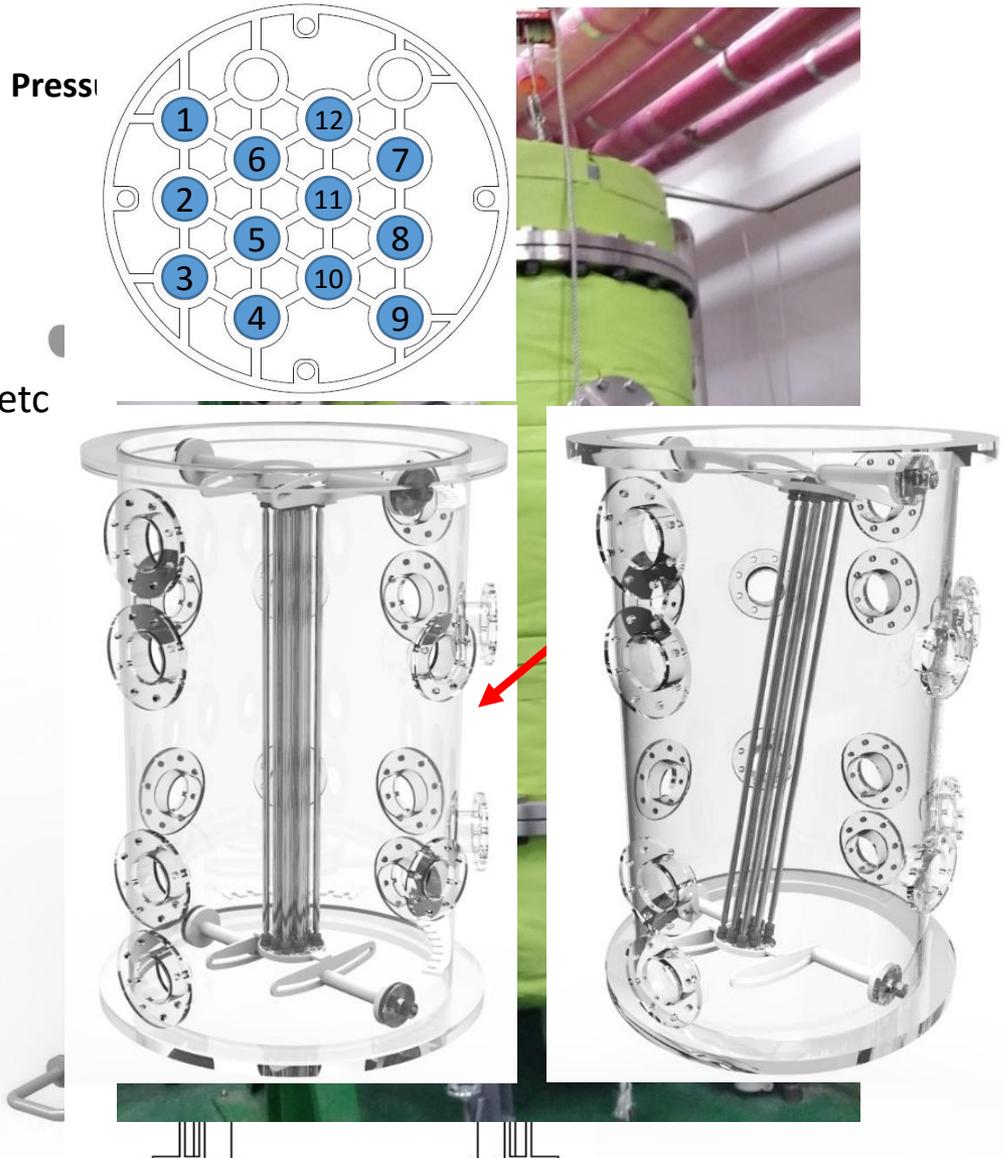
Experimental Apparatus

Components

- Bundle : 12 tubes
- Pressurized vessel
- Coolant supply line
 - Preheater and pump, etc
- Immersion heater

Measurements

- Coolant flow
 - Coriolis, Magnetic
- Temperature
 - K-type thermocouple
- Pressure
 - Transmitter



Experimental Facility (3)



Measurement methods

- Wall temperature

$$- T_w = T_{s,2} + \frac{\ln(R/r_2)}{\ln(r_2/r_1)} (T_{s,2} - T_{s,1})$$

- Heat transfer coefficient of a tube

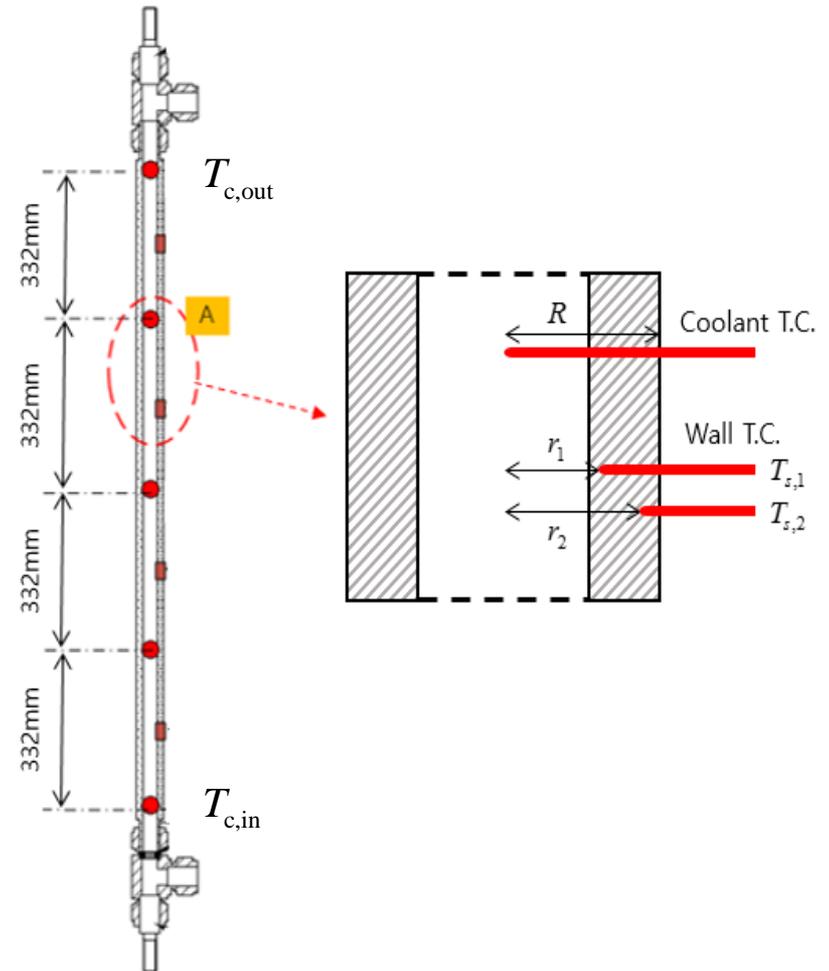
$$- h_{tube} = \frac{\dot{m} c_p (T_{c,out} - T_{c,in})}{\pi d L (T_\infty - T_w)}$$

- Average heat transfer coefficient of a bundle

$$- h_{bundle} = \frac{h_1 + h_2 + h_3 + \dots + h_{12}}{12}$$

- Air mass fraction

$$- W = \frac{\rho_{air} (P_{air}, T_\infty)}{\rho_{air} (P_{air}, T_\infty) + \rho_{steam} (T_{\infty, sat})}$$



Experimental Facility (4)



- Uncertainty of measurement system
 - Temperature sensor (TC)
 - Calibrated with 0.5°C uncertainty
 - Signal line from TC to DAS was checked with FLUKE 754 calibrator.
 - Flow meter, pressure measurement system
 - Calibration sheets were provided from manufacturer

Parameter	Thermocouple (K type)	Coriolis flow meter	Magnetic flow meter	Pressure transmitter	Differential pressure transmitter
Range	-200°C ~ 1000°C	2~226.8 kg/min	0~2m ³ /h	0~1000kPa	0~60kPa
Error	±0.5°C	0.05%(Reading)	0.50%(Reading)	0.08%(FS)	0.40%(FS)

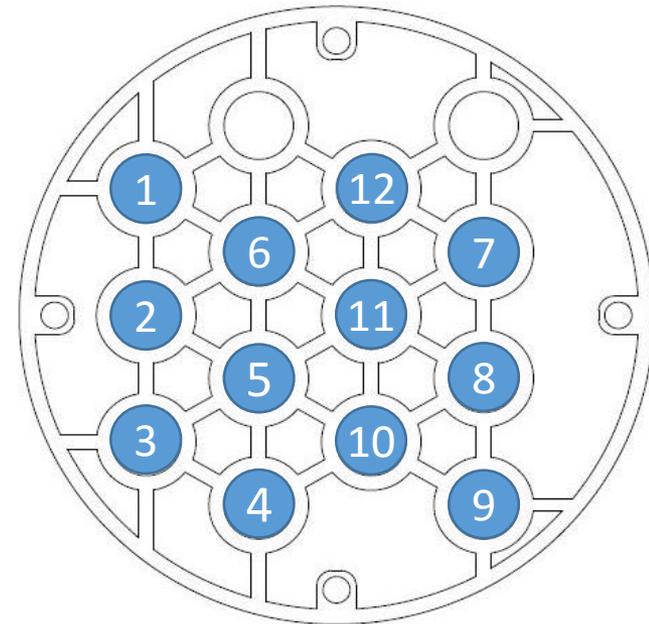
Experiments and Results (1) : Test Matrix and Conditions

■ Test matrix

- Single tube experiments
- Tube Bundle experiments
 - 12 tubes condensation tests
- Obstacle experiments
 - Each single tube condensation test with 11 dummy tubes

■ Bundle Experimental conditions

- Pitch to diameter of bundle : 2.0, 2.5
- Vessel pressure
 - 1.5, 2.0, 3.0 and 4.0 bar
- Inlet temperature of coolant: 70°C
- Air mass fraction
 - 0.3 ~ 0.8
- Inclination : Vertical, 14.5°

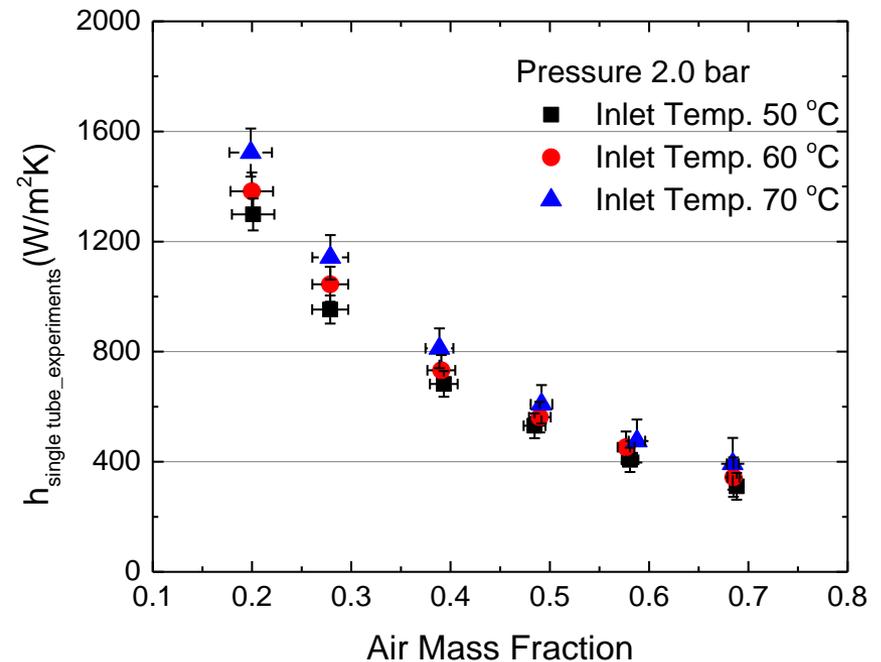
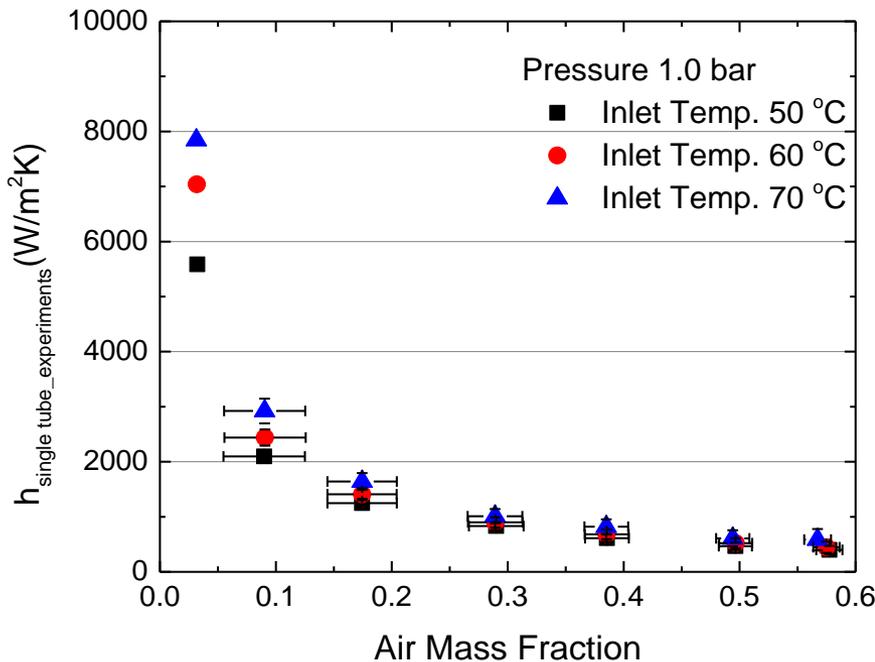


<Bundle experiments>

Experiments and Results (2) : Single Tube Experiments



- Heat transfer coefficient according to air mass fraction and inlet temperature
 - Increase of the heat transfer coefficient with decrease in air mass fraction and a increase in inlet temperature.
 - Drastic increase of heat transfer coefficient under air mass fraction 0.1



Experiments and Results (3) : Single Tube Experiments

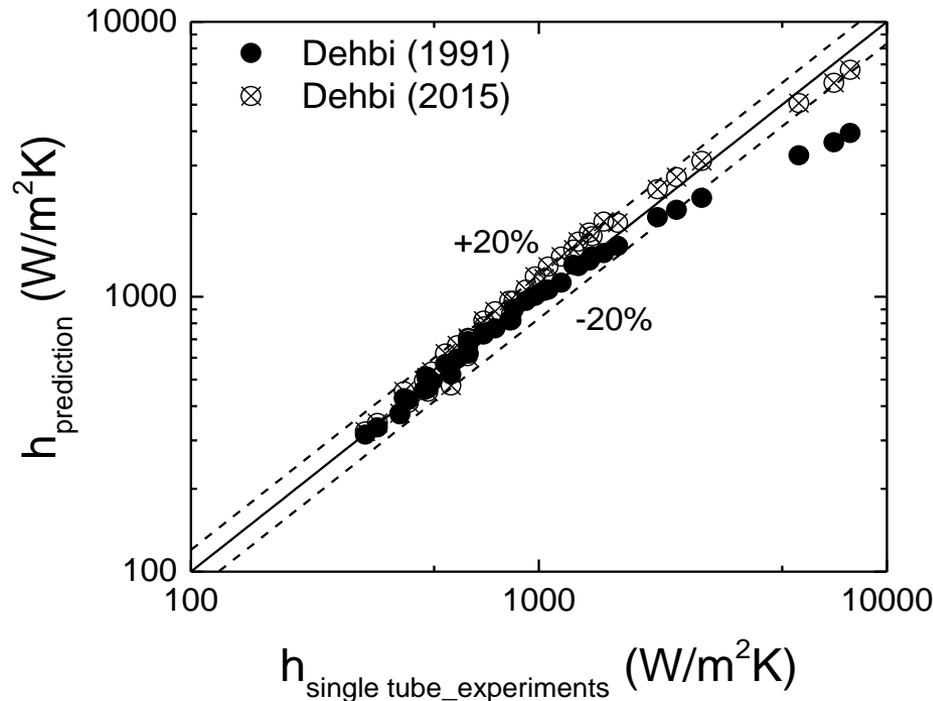


Single tube experiments

- Evaluation of Dehbi correlations(1991, 2015) against single tube data

$$- h_{Dehbi,1991} = 1.25 \frac{L^{0.05} \left[(3.7 + 28.7P) - (2438 + 458.3P) \log W_\infty \right]^{[1]}}{(T_\infty - T_w)^{0.25}}$$

$$- h_{Dehbi,2015} = 0.185 D^{2/3} (\rho_w + \rho_\infty) \left(\frac{\rho_w - \rho_\infty}{\mu} \right)^{1/3} \frac{h_{fg}}{T_\infty - T_w} \ln \left(\frac{W_w}{W_\infty} \right) \left(1 + 0.3 \left(\sqrt{32} Gr^{-1/4} \frac{L}{d} \right)^{0.909} \right)^{[2]}$$



[1] Dehbi, A. "The effect of noncondensable gases on steam condensation under turbulent natural convection conditions," Diss. Massachusetts Institute of Technology, (1991).

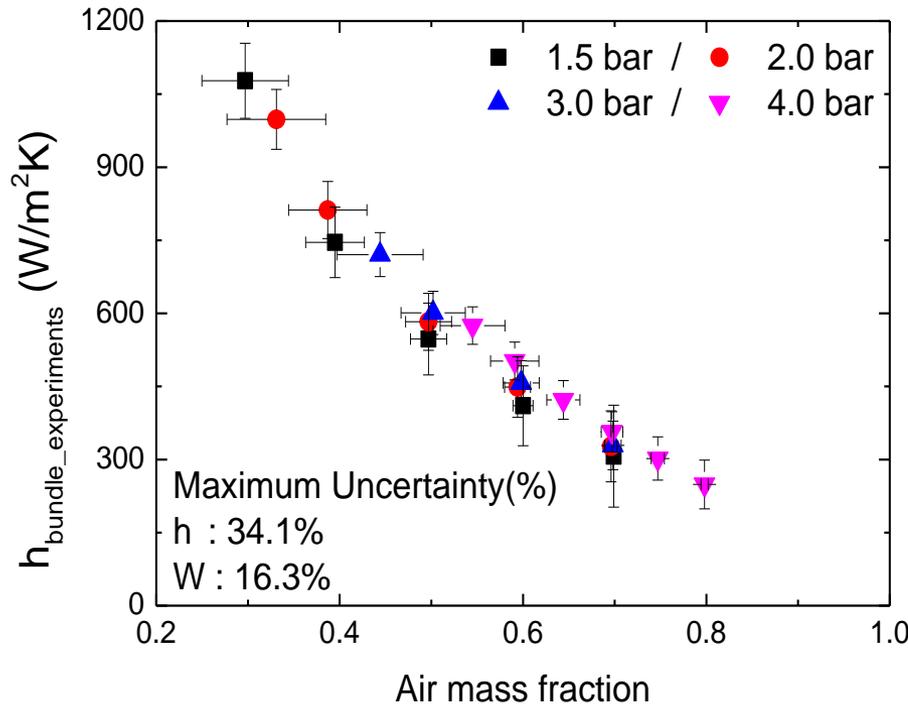
[2] Dehbi, A. "A generalized correlation for steam condensation rates in the presence of air under turbulent free convection," International Journal of Heat and Mass Transfer 86, pp. 1-15 (2015).

Experiments and Results (4) : Bundle Experiments

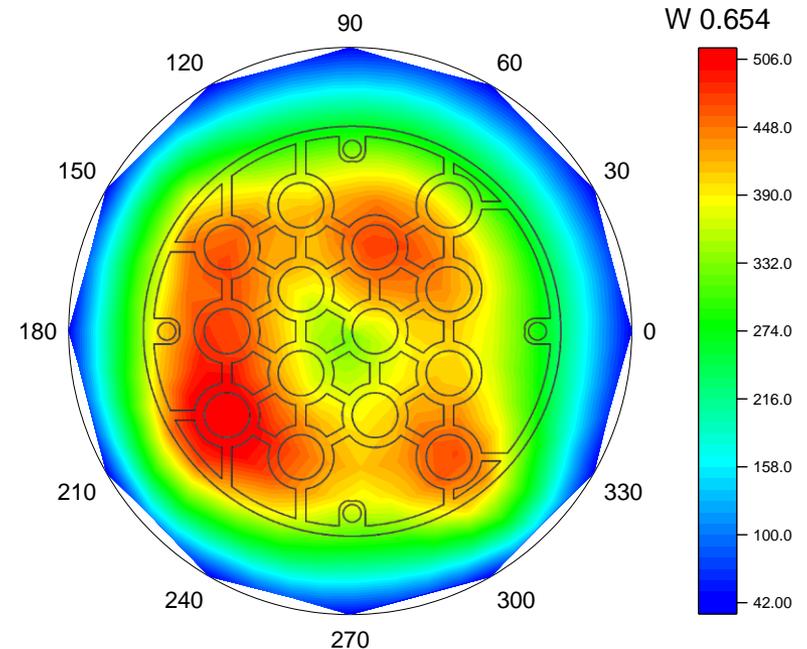


■ Bundle experiments

- Degradation of heat transfer coefficient by screen effect of air mass fraction
- Enhancement of heat transfer coefficient by
 - Suction effect of steam
 - Containment pressure



<Variation of condensation heat transfer coefficient with air mass fraction>



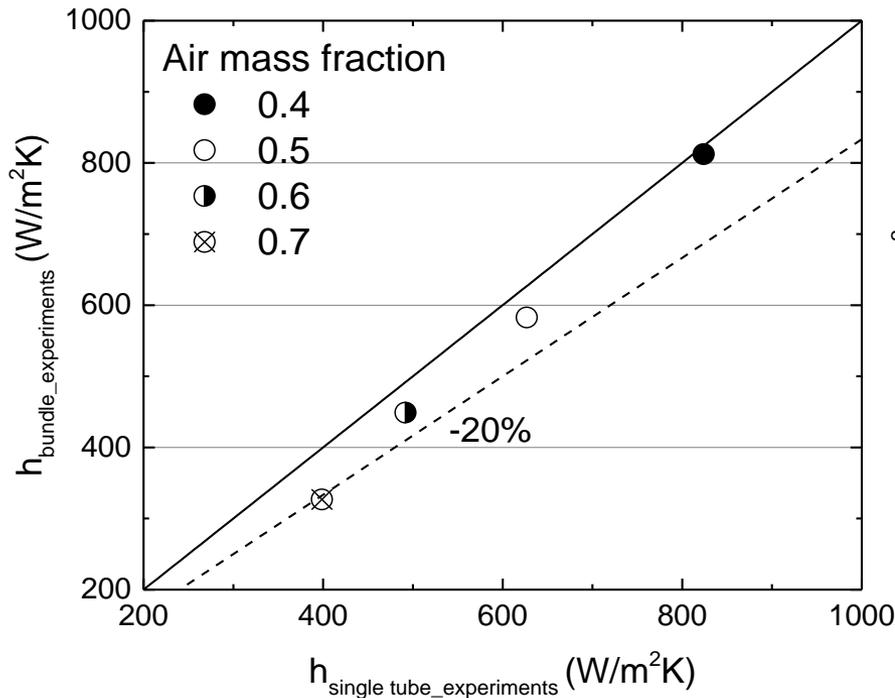
<Distribution of heat transfer coefficient on bundle (4 bar, $W 0.65$)>

Experiments and Results (5) : Bundle Experiments

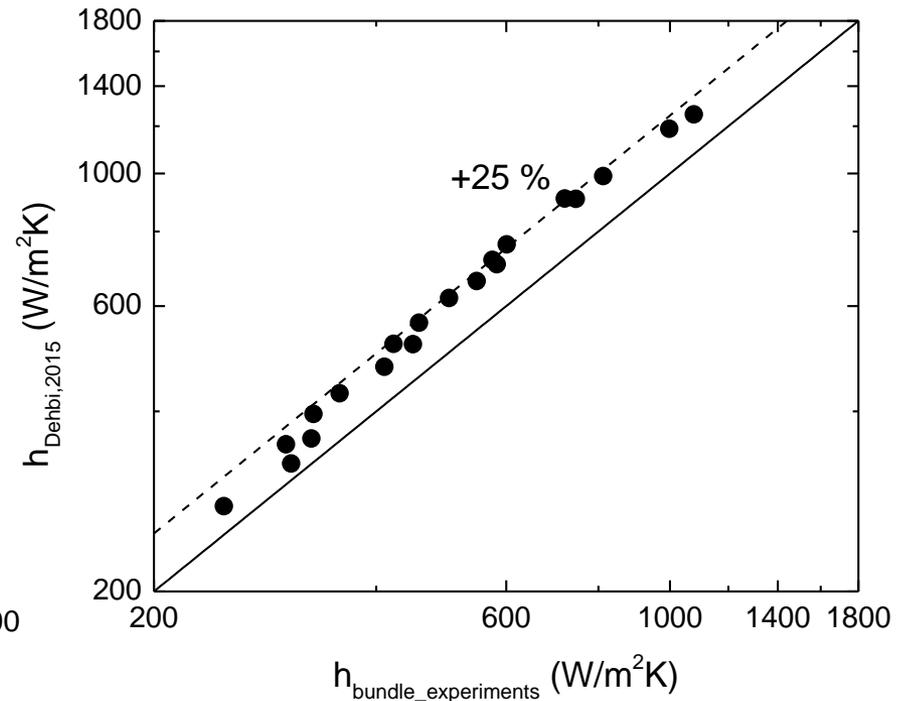


■ Bundle experiments

- Comparison between experiments for single tube and bundle under 2.0 bar
 - The deviation decreases with decrease of air mass fraction
- Evaluation of the Dehbi (2015) correlation against bundle data



<Comparison between bundle
and single rod under 2 bar

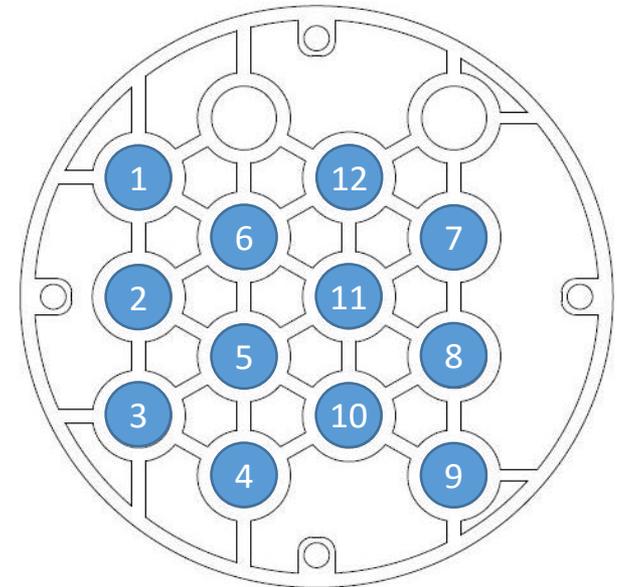
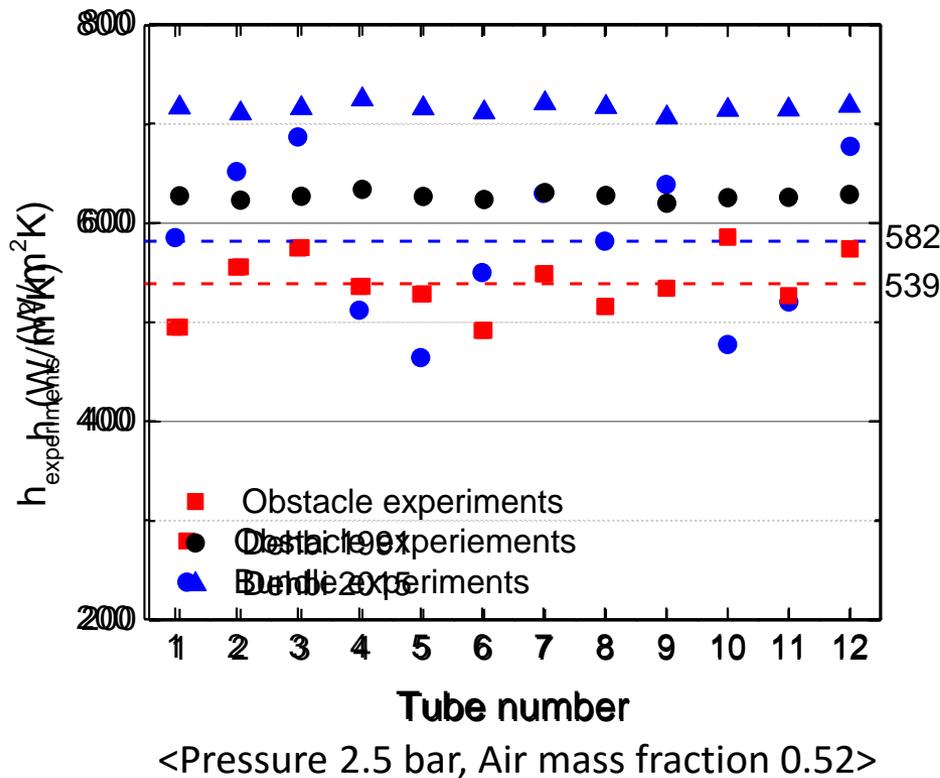


<Comparison between bundle experiments
and Dehbi correlation

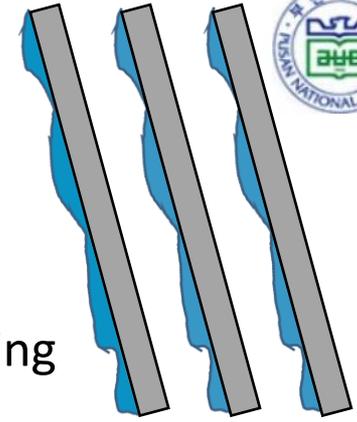
Experiments and Results (6) : Obstacle Experiments



- Comparison data between obstacle tube and bundle
 - Increase of heat transfer of outside tube by suction
 - Decrease of those of inside tube by screening effect
 - Improvement of average heat transfer of a bundle by suction effect of a bundle.

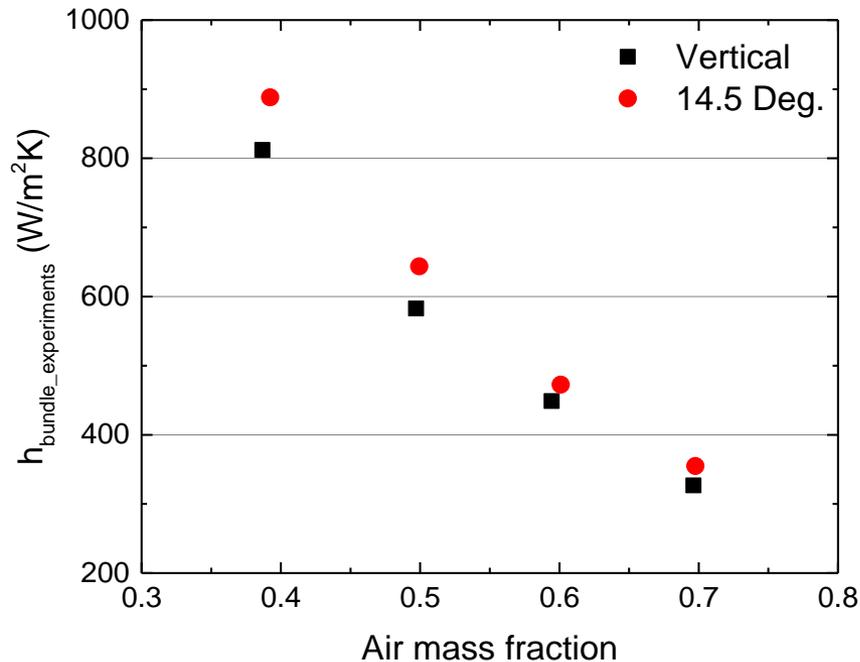


Experiments and Results (7) : Bundle Experiments



■ Inclination effect

- Inclined bundle 14.5°
- Increase of heat transfer coefficients owing to water flowing on lower surface of tube



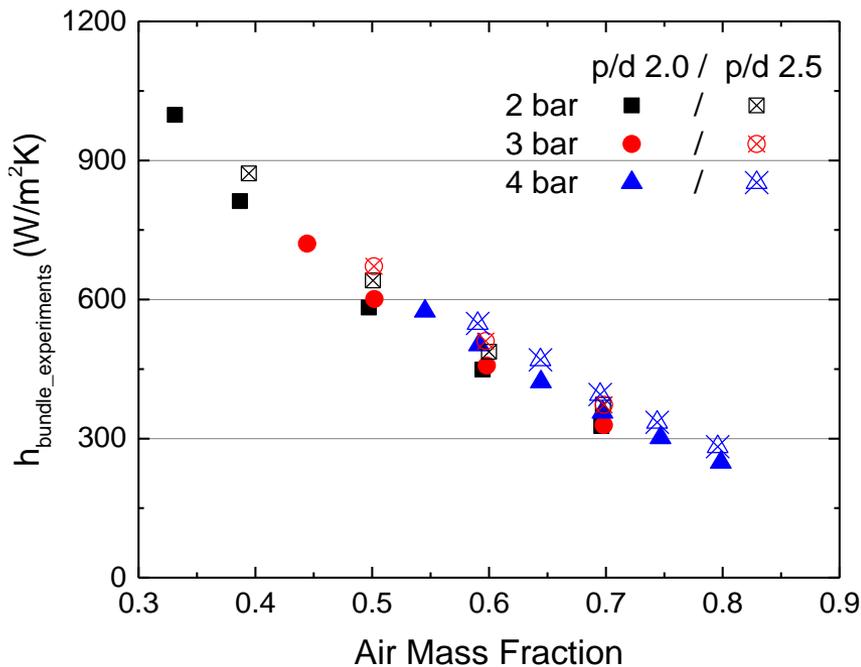
<Variation of condensation heat transfer coefficient >
with air mass fraction and inclination



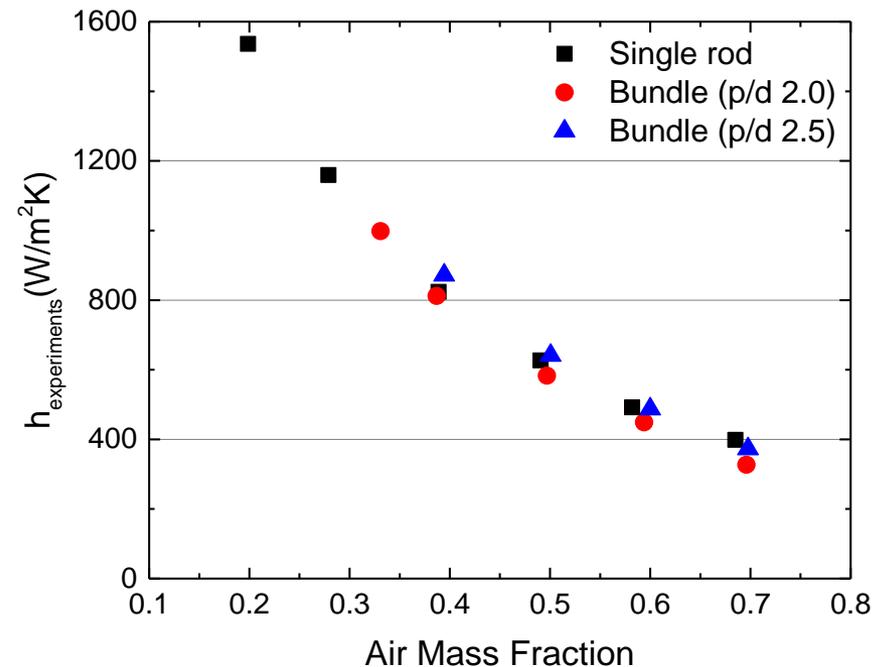
Experiments and Results (8) : Bundle Experiments



- Pitch to diameter effect
 - Reduction of screening effect on the central region of bundle
 - Increase of heat transfer with increase of pitch to diameter ratio



<Variation of heat transfer coefficient with >
air mass fraction and pressure



<Variation of heat transfer coefficient with >
air mass fraction and heat exchanger type

Development of bundle factor correlation

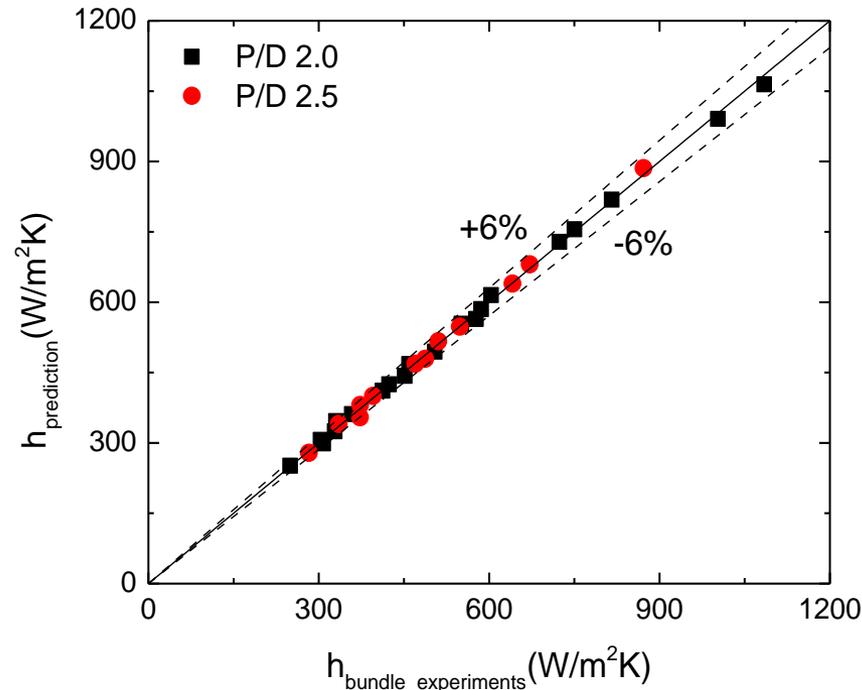


■ Bundle condensation correlation

- Evaluation of the Dehbi correlation against PNU data

$$- f_{bundle} = \frac{h_{bundle}}{h_{single-tube}} = \left(1.316 \left(\frac{P}{P_{cr}} \right)^{0.07} \left(\frac{T_{\infty} - T_w}{T_{cr}} \right)^{-0.0145} - 11 \frac{P}{P_{cr}} \right) \times (1.08W^2 - 0.945W + 1.12) \left(0.187 \frac{P}{d} + 0.65 \right)$$

$$- h_{bundle} = h_{Dehbi,2015} \times f_{bundle}$$



<Comparison between bundle experiments and >
 proposed bundle condensation correlation

Summary & future Plans



- Condensation test with bundle heat exchanger has been performed for the passive containment cooling system (PCCS).
- Major findings from experiments
 - Decrease of heat transfer coefficient is expected because of screening effect of adjacent tubes (structure) in the tube bundle.
 - However, the heat transfer coefficient is not decreased because suction effect compensates screening effect.
 - The heat transfer coefficient increases as inclination and pitch to diameter increase.
- Bundle factor for correction of Dehbi (2015) correlation was proposed.
- Experimental investigation will be continued for the developments of condensation model in the single and tube bundle conditions.

Q & A



Thank you for your attention

