2D 3D

The Comprehensive Analysis on the Thermo-mechanical Behavior of the Assembly Ducts by 2D and 3D Code

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NUBOW 2D - KMOD 3 CRAMP

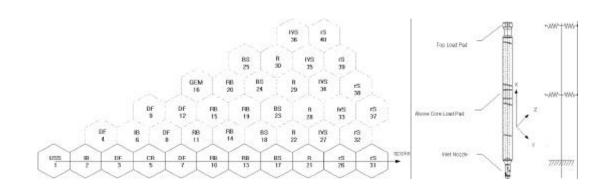
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Abstract

In the design of LMR assembly duct, it is necessary to analyze the thermo-mechanical behavior of the assembly ducts due to the bowing and swelling of the assembly duct. Two codes are available for the thermo-mechanical analysis of the duct in KALIMER, which are the 2D code (NUBOW2D-KMOD) and the 3D code (CRAMP). In this study, the first order creep equation installed into 3D code is corrected by the analysis of the 2D code. And in the analysis of the 2D code, the new analytical results for 2D code are derived by changing input condition in order to get the similar results compared with the analysis of the 3D code. These new results are used for the analysis of the contact pattern between the ducts and the reactivity feedback which are the main issues for the core mechanical analysis. So, the best estimate results for the core mechanical analysis can be derived from the comprehensive analysis on the thermo-mechanical behavior of the assembly ducts by 2D and 3D code.

1.

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•	가	가	가		, 2 가		3				
		3			71			HT9	•		
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Recept	acle,),		, Core fo		(2	(, , 3		,	,	,	,
								ז	NUROV	V 2D - K	$MOD^{1)}$
(NUcle	ar fı	ıel BOW	ing 2Dimen	sional a	nalysis	code-K	aeri l				
Restrai	nt A		odeling Prog		가						2
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CKA			ALAI	1	5			가		Binar	V



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3. 2D 3D

- 2D 3 D HT9

$$\varepsilon = [-2.9 + 9.5 \times 10^{-3} \times (T - 273)] \times 10^{-26} \Phi t \sigma_e^{1.3} + 1.743 \times 10^{18} [\frac{\sigma_e}{E(T)}]^{2.3} \exp(-\frac{36739}{T}) t$$

$$\vdots \qquad (n/cm^2 s)$$

$$T : (K)$$

$$e : 7 + (MPa)$$

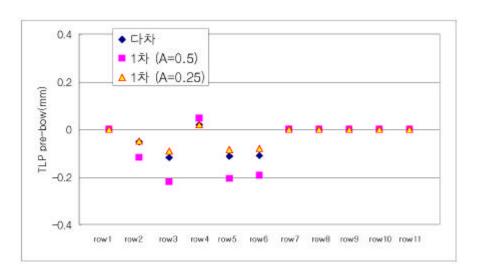
$$E(T) : (MPa)$$

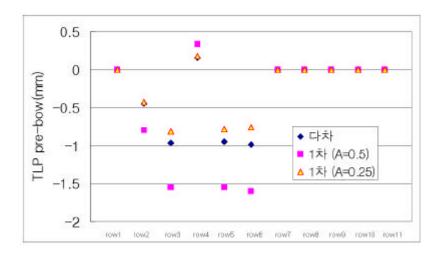
$$2 \qquad , 3$$

$$1 \qquad . 3D \qquad CRAMP \qquad 1$$

3D CRAMP 1

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가
                                                  가
                                                             1
                 3D
                                                             1
             1
         \epsilon = A * [4.01823 x 10^{-6} T + (-1.2266 x 10^{-3})] \sigma
           ε : (% per dpa),
           T : ( )
            σ : 가 (Mpa)
                       100dpa=10^{24}n/cm<sup>2</sup> 7 CRAMP
Α
        가 2D
      2 50
                                           Α
                , 3 540
400 dp a = 10^{24} n/cm^{2}
                (PRISM ) 200 dpa = 10^{24} n/cm^2 7
               A 200 dpa = 10^{24} n/cm^2 0.5, 400 dpa = 10^{24} n/cm^2
                                                                  0.25가
                                      가
     A = 0.25 가
                                                              3D
       A 0.25
                                                                   (540
       , A = 0.25) : 0.22 \text{mm}가
         2D 3D
                                     , 3D
               가 2D
                                                     3D
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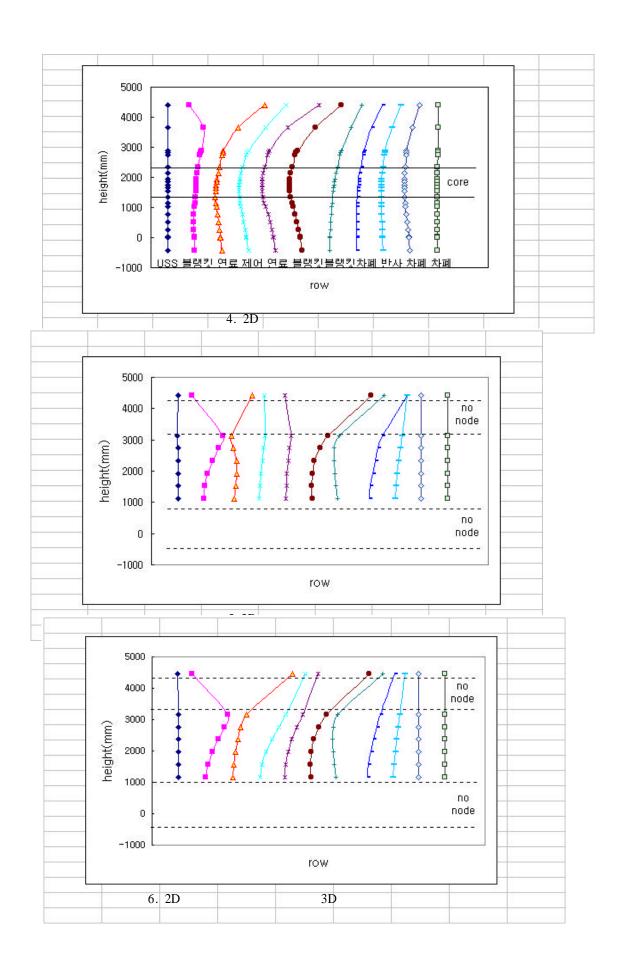




3 540

- 2D 3D

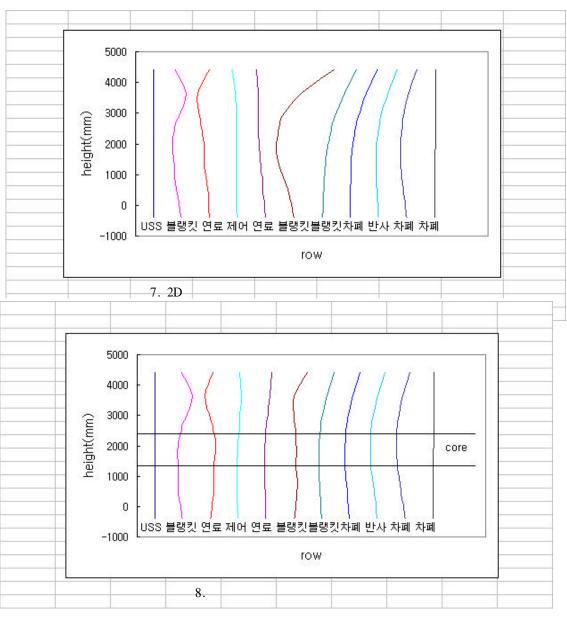
2D 3D 2 3 NUBOW 2D - KMOD 2 5 1/12 spoke 6 3 spoke spoke 2 row 가 2 가 3 5 2 가

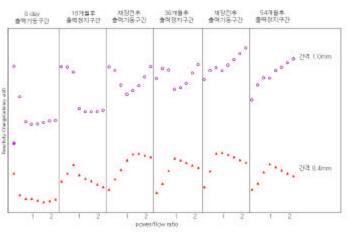


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- 3D **2**D 2 3 2 3 가 3 2 가 6 2 3 가 pad 가 pad 가 pad $1 \mathrm{m}\,\mathrm{m}$ ACLP 가 가 가 6 row ACLP pad pad 가 7 1mm pad 가 가 0.4mm 2 NUBOW 2D - KMOD pad가 8 9 1mm 5). 0.4mm pad

가 pad





4.

NUBOW 2D - KMOE) 3 가	CRAN	МР ,	3	2	
3 3	가 3 가	가 2 · 1 1		가 3	가	3
	2	0.4mm 3	, 가	, 1mm	0.4mm pad7t	

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