

**A Study on Methodology Determining Acceptance Criteria
for Instrument As-found Data**

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Abstract

"As-found" data provides the indication that the instruments have performed their desired function in process dynamic changes. The present acceptance criteria for "as-found" data error includes reference accuracy, measuring & test effect and drift, but there are other errors to be taken into account of acceptance criteria for "as-found" data such as environmental effect under operation, temperature difference effects between two calibrations and human errors. In this paper, the present acceptance criteria for as-left/as-found data was reviewed, and the errors which have an effect on "as-found" data were evaluated. Finally the methodology determining acceptance criteria for as-found data was proposed applicable to Korea Standard Nuclear Power Plant (KSNP).

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(As-found)

(As-left)

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[2,3]

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SRSS(Square Root Sum of Square)

= SRSS[RA, MTE]

, RA(Reference Accuracy)

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. MTE(Measuring and Test Error)

가 , MTE가
 SRSS
 가 MTE
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 가
 MTE (Drift) SRSS
 = SRSS[RA, MTE, Drift]

, Drift
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^[4]

2) 가
 1 가 (NSSS)
 Rosemount

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TID(Total Integrated

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(Technical Manual)

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MTE

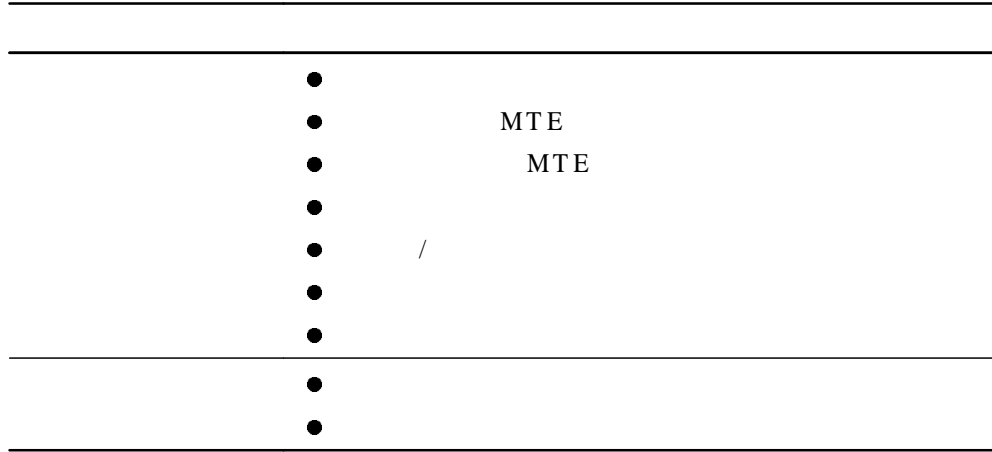
MTE

MTE

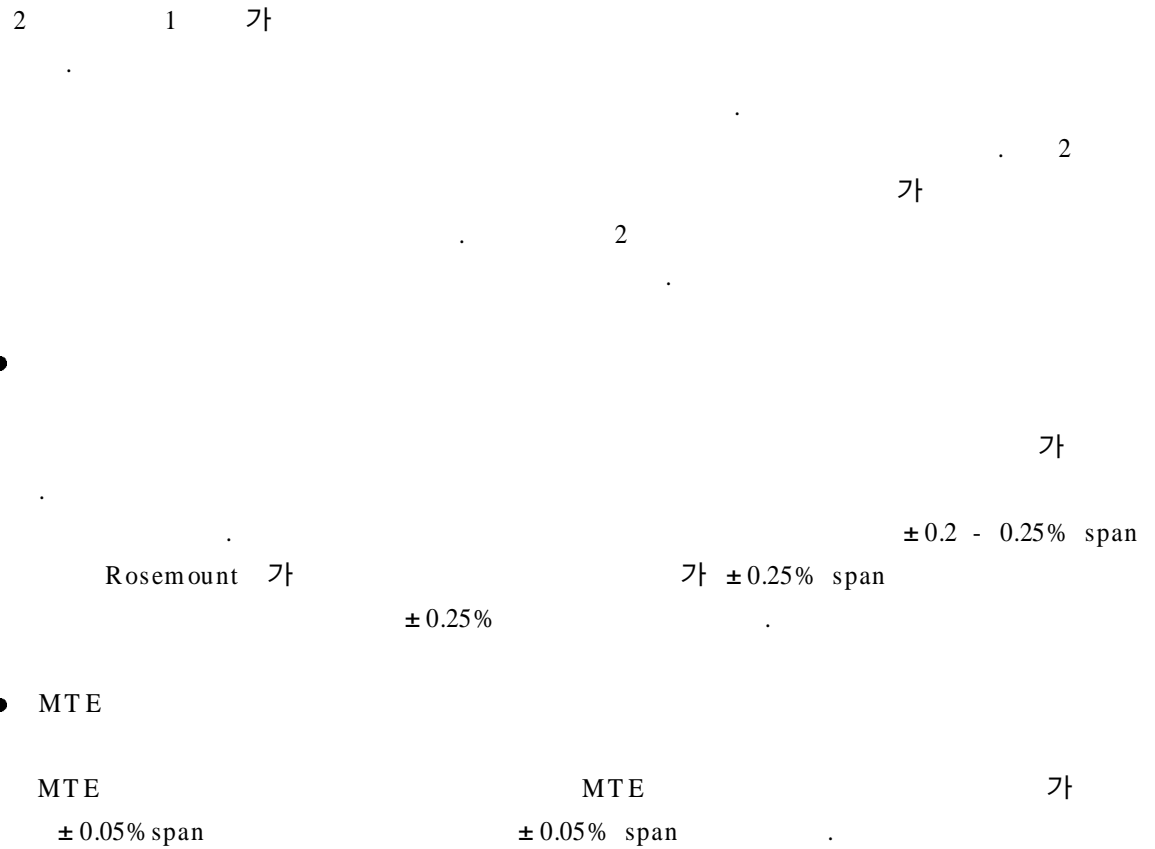
1

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2.



3)



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$\pm 0.2\%$ URL(Upper Range Limit) . URL span TDF(Turn
 Down Factor, URL/ span) . span $\pm (0.25$ *
 TDF)% span .

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. Rosemount /

• 1152 Series

- (1) $\pm (0.5\% \text{ URL} + 0.5\% \text{ span})^*$ /100() : Code Range 4-0
- (2) $\pm (1.0\% \text{ URL} + 1.0\% \text{ span})^*$ /100() : Code Range 3

• 1153 Series

- (1) $\pm (0.75\% \text{ URL} + 0.5\% \text{ span})^*$ /100() : Code Range 4-9
- (2) $\pm (1.5\% \text{ URL} + 1.0\% \text{ span})^*$ /100() : Code Range 3

• 1154 Series

- (1) $\pm (0.75\% \text{ URL} + 0.5\% \text{ span})^*$ /100() : Code Range 4-9
- (2) $\pm (1.13\% \text{ URL} + 1.0\% \text{ span})^*$ /100() : Code Range 0

• 1154 Series H

- $\pm (0.15\% \text{ URL} + 0.35\% \text{ span})^*$ /50() : Code Range 4-9

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MTE

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| I. () ⁽¹⁾ | | | |
|---------------------------|-------------------|-------------------|----------------------------------|
| | Rosemount 1152 | Rosemount 1153 | Rosemount 1154/ 1154 Series H |
| (a) | ± 0.25% span | ± 0.25% span | ± 0.25% span |
| (b) MTE ⁽²⁾ | ± 0.05% span | ± 0.05% span | ± 0.05% span |
| (c) MTE | ± 0.05% span | ± 0.05% span | ± 0.05% span |
| (d) | ± 0.2% URL | ± 0.2% URL | ± 0.2% URL |
| (e) | ⁽³⁾ | ⁽³⁾ | ⁽³⁾ |
| (f) | ± 0.5% URL | ± 0.5% URL | ± (0.2% URL + 0.2% span) |
| = SRSS [a, b, c, d, e, f] | | | |

4)

(KSNP)

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5,6

5,6

Rosemount

| II. () ⁽¹⁾ | | | |
|------------------------|---|---|--|
| | Rosemount 1152 | Rosemount 1153 | Rosemount 1154/ 1154 Series H |
| (a) | $\pm 0.25\%$ span | $\pm 0.25\%$ span | $\pm 0.25\%$ span |
| (b) MTE ⁽²⁾ | $\pm 0.05\%$ span | $\pm 0.05\%$ span | $\pm 0.05\%$ span |
| (c) MTE | $\pm 0.05\%$ span | $\pm 0.05\%$ span | $\pm 0.05\%$ span |
| (d) | $\pm 0.2\%$ URL ⁽³⁾ | $\pm 0.2\%$ URL | $\pm 0.2\%$ URL |
| (e) | (3) | (3) | (3) |
| (f) | $\pm 0.5\%$ URL | $\pm 0.5\%$ URL | $\pm (0.2\% \text{ URL} + 0.2\% \text{ span})$ |
| (g) | $\pm 0.5\%$ span of reading/ 1000psi | $\pm 0.5\%$ span of reading/ 1000psi | $\pm 0.5\%$ span of reading/ 1000psi |

= SRSS [a, b, c, d, e, f, g]

Note : (1) ,

(2) MTE 가 가

(3) “ ” “ “

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Rosemount ,

ITT Barton

. Rosemount

3, 4

1152, 1153 1154/ 1154 Series H

가 ITT Barton

MTE . Rosemount

4-20 mA

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3 (4.8)

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| A . Rosemount 1152 | |
|---|--|
| P - 225 Volume Control Tank Pressure Transmitter | |
| URL | 7031.00 cmH ₂ O |
| 0% | 0.00 cmH ₂ O |
| 100% | 7000.00 cmH ₂ O |
| span | 7000.00 cmH ₂ O |
| | ± 0.250% span |
| | ± 0.200% URL |
| (T _e) | ± (0.5%URL+0.5% span)*4.8/100 = 0.05% span |
| MTE _{old} | ± 0.05% span |
| MTE _{new} | ± 0.05% span |
| = SRSS[, T _e , MTE _{old} , MTE _{new}] = SRSS[0.25, 0.20, 0.05, 0.05, 0.05] = ± 0.332% span | |

B. Rosemount 1152
PD-124W Reactor Vessel Differential Pressure Transmitter

| | |
|--------------------|---|
| URL | 7031.00 cmH ₂ O |
| 0% | 0.00 cmH ₂ O |
| 100% | 5000.00 cmH ₂ O |
| span | 5000.00 cmH ₂ O |
| | ± 0.250% span |
| | ± 0.200% URL |
| (T _e) | ± (0.5% URL + 0.5% span)*4.8/100 = ± 0.06% span |
| (R _e) | ± 0.703% span |
| (ST _e) | ± 0.25% reading/1000psi @2360psia = ± 0.590% span |
| MTE _{old} | ± 0.050% span |
| MTE _{new} | ± 0.050% span |

= SRSS[, , T_e, R_e, ST_e, MTE_{old}, MTE_{new}]
 = SRSS[0.250, 0.281, 0.060, 0.703, 0.590, 0.050, 0.050]
 = ± 0.996% span

C. Rosemount 1154 Series H
P-1013A Steam Generator 1 Pressure Transmitter

| | |
|--------------------|---|
| URL | 210.90 Kg/cm ² G |
| 0% | 0.00 Kg/cm ² G |
| 100% | 107.10 Kg/cm ² G |
| span | 107.10 Kg/cm ² G |
| | ± 0.250% span |
| | ± 0.200% URL |
| (T _e) | ± (0.15% URL + 0.35% span)*4.8/50 = ± 0.062% span |
| (R _e) | ± (0.20% URL + 0.2% span) = ± 0.594% span |
| MTE _{old} | ± 0.050% span |
| MTE _{new} | ± 0.050% span |

= SRSS[, , T_e, R_e, MTE_{old}, MTE_{new}]
 = SRSS[0.250, 0.394, 0.062, 0.594, 0.050, 0.050]
 = ± 0.761% span

| D. Rosemount 1154 Series H L-1114A Steam Generator 1 Level(NR) Transmitter | |
|---|---|
| URL | 381.00 cmH ₂ O |
| 0% | 98.65 cmH ₂ O |
| 100% | 363.52 cmH ₂ O |
| span | 264.87 cmH ₂ O |
| | ± 0.250% span |
| | ± 0.200% URL |
| (T _e) | ± (0.15% URL + 0.35% span)*4.8/50 = ±0.054% span |
| (R _e) | ± (0.20% URL + 0.2% span) = 0.488% span |
| (ST _e) | ± 0.25% reading/1000 psi @1076psia = ±0.734% span |
| MTE _{old} | ± 0.050% span |
| MTE _{new} | ± 0.050% span |
| = SRSS[, , T _e , R _e , ST _e , MTE _{old} , MTE _{new}] = SRSS[0.250, 0.288, 0.054, 0.488, 0.734, 0.050, 0.050] = ± 0.964% span | |

3.

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1. "Methodologies for the Determination of Setpoints for Nuclear Safety-Related Instrumentation", ISA-RP67.04-Part II, 1994.
2. "Guidelines for Instrument Calibration Extension/Reduction Programs", EPRI TR- 103335, 1994.
3. "Rosemount Instrument Manual", Rosemount Nuclear Instruments, Inc., 1995.
4. "Instrument Setpoint/Loop Accuracy Calculation Methodology", SONGS JS- 123- 103C, 1993.