# The Effects of Compaction Pressure, Sintering Temperature and Time on the Fabrication of Simulated Fuel



#### Abstract

In this study, the effects of the variables on sintering of simulated fuel to simulate the spent fuel are described. Mainly, the effects of compaction pressure, sintering temperature and sintering time on the density of pellet are described. The experimental is performed with compaction pressure of  $1 \text{ ton/cm}^2$  4 ton/cm<sup>2</sup>, sintering temperature of 1670 , 1730 and 1780 and sintering time of 4 hr, 8hr and 24hr. Sintered density and grain size is increased with these variables. Apparent densities of the powders after wet milling and grinding in tubular are 1.3444 g/cm<sup>3</sup> and 2.3352 g/cm<sup>3</sup>, respectively. Optimum condition of simulated fuel fabrication is 1730

in sintering temperature,  $3 \text{ ton/cm}^2$  in compaction pressure and 4 hours in sinterin time to satisfy the criteria of the pellet density of CANDU fuel.

1.

DUPIC(Di	irect Use of 가	Spent PWF	R Fuel in CA	NDU React	tors)		
. 1993	3			OREO	X (Oxidatio	on and Red	uction
of Oxide fu	el)가 가			[1]	0	REOX	
				•	DUPIC		
		DUPIC				(	lattice
property)							
			,		CPF	PF	
DUPIC	(Refere	ence Simula	ted DUPIC F	uel) U-23	35 Pu-2.	39	
1.0 % 0.4	5 %	.[2]	DUPIC			가	
,	,			가			
			DU	JPIC			
DUPIC							
				가		DUPIC	
		/			,		
		(		DUPIC	)		
							.[3]
- matrix		: Sr, Zr,	Nb, Y, La, C	Ce, Pr, Nd,	Pm, Sm;		
-	: Mo, Tc	, Ru, Rh, Po	d, Ag, Cd, In,	Sb, Te;			
-	: Ba, Z	r, Nb, Mo,	(Rb, Cs, Te);				
-	: Kr, Xe,	Br, I, (Rb,	Cs, Te).				
						DUPIC	
, ,		,	,	, DUPIC	, -		,
					가		
		,[3-5]		matri	х	[6-8]	
	potential	[9]			,		
		[10,11	]	, simula	ted mixed	(U, Th)O	2

,		[12-	14]	UO <sub>2</sub> [15- 18]				
		가	DUPIC	[15,18,19]		. ,		
DUPIC					가			
,	,	•				1 ton/	$cm^2$ 4 to	$n/cm^2$ ,
	4	, 8	24	,	1670	, 1730	1780	
2.								
2.1								
diuranate	;)					(UO <sub>2</sub> )	ADU (amm ORIC	onium GEN-2
	,		,				18	
가			가	Pr, Sm		Nd	, Pu Ce	, Тс
Ru, Ar	n La		71	, 7f			1	
2.2								
					가		UO	2
$UO_2$	turb	ular m	ixer	24			attrition m	iller
5			-	, 40	-	5	•	
-		_		,			35 sieve	
tub	ular $(0, 4, -)$	5 7L	4	1			Zn stea	rate
0.2 %	(U.4 g)	71	tubular	1	•			

mixing UO<sub>2</sub> and F.P. : mixing UO<sub>2</sub> and F.P. for 24 hrs. in tubular milling : milling mixed powder with methyl alcohol for 24 hrs in attrition miller dry : dry milled powder at 40 in oven for 5 days granulation : shift sieve No. 35 and ratating for 5 hrs in tubular lubricant : mixing granulated powder and Zn stearate(0.2 %) for 1 hrs in tubular

element	chemical	weight	contents	% of	Weight of	weight of	% of
	form	0	(g)	element	Oxide	U 100 g	element
Rb	Rb2O3	85.5	278.6	0.02811	356.83	0.03174	0.0308761
Sr	SrO	87.6	541.7	0.05465	640.62	0.05697	0.0554318
Y	Y2O3	88.9	355.0	0.03582	450.84	0.04010	0.0390104
Zr	ZrO2	91.2	2888.4	0.29142	3901.65	0.34700	0.3376048
Мо	MoO3	96.0	2636.7	0.26602	3955.05	0.35175	0.3422253
Тс	RuO2	.09	612.0	0.06175	822.61	0.07316	0.0711798
Ru	RuO2	101.1	1724.5	0.17399	2270.50	0.20193	0.1964632
Rh	Rh2O3	102.9	330.0	0.03329	406.97	0.03619	0.0352144
Pd	PdO	106.4	1109.3	0.11192	1276.11	0.11349	0.1104203
Те	TeO2	127.6	379.6	0.03830	474.80	0.04223	0.0410836
Ba	BaCO3	137.3	1493.2	0.15065	2145.70	0.19083	0.185665
La	La2O3	138.9	957.7	0.09662	1123.18	0.09989	0.0971871
Ce	CeO2	140.1	1854.6	0.18712	2278.15	0.20261	0.197125
Pr	Nd2O3	140.9	877.6	0.08854	1047.81	0.09319	0.0906659
Nd	Nd2O3	144.2	3157.2	0.31854	3682.52	0.32751	0.318644
Sm	Nd2O3	150.4	693.0	0.06992	775.41	0.06896	0.067095
Th		232.0	396.6	0.04001		0.00000	0
U	UO2	238.0	991154	100.000	1124402.5	100.00000	97.29308
Np		237.0	354.7	0.03579		0.00000	0
Pu(Ce)	CeO2	244.0	7361.9	0.74276	5193.16	0.46186	0.4493571
Am	La 2 O 3	243.0	720.1	0.07265	482.73	0.04293	0.0417703

# 1. UO<sub>2</sub> 7

### 2.3

		10 ton		
		10	1.0 $ton/cm^2$	
4.0 $ton/cm^2$		. 1999		
, 1670 , 1730	1780	4 , 8	24	

# 2.4

### tubular

•

.

			(scanning electron
microscopy, SEM)		,	laser-light
scattering method	B.E.T		,

(immersion method) , linear intercept





3.

a) after wet milling x 100



b) after wet milling x 500



c) after tubular grinding x 100





d) after tubular grinding x 500

c, d) tubular

$$= 3.179 + 1.801 P^{1/3}$$
(1)

, o ( ), P , o A, B





2.



,  $t on/cm^2$ 4 ton/cm<sup>2</sup> 1670 , 1730 1780 8 24 (1730 14 ) 4 2 3 , 가 가 • 가 1670 9.754 g/cm<sup>3</sup>(90.452 % of TD) 10.602 g/cm<sup>3</sup>(98.314 % of TD) 가

1



3.

,

Soaking	Soaking	Sinte	)		
Temp()	Time(hrs)	$1(ton/cm^2)$	$2(ton/cm^2)$	$3(ton/cm^2)$	$4(ton/cm^2)$
	4	9.754(90.452)	9.959(92.348)	10.057(93.262)	10.121(93.851)
1670	8	9.948(92.244)	10.144(94.063)	10.211(94.682)	10.259(95.128)
	24	10.479(97.175)	10.552(97.854)	10.572(98.039)	10.602(98.314)
	4	10.248(95.025)	10.352(95.993)	10.403(96.465)	10.447 (96.874)
1730	8	10.379(96.246)	10.464(97.033)	10.511(97.467)	10.535(97.686)
	14	10.438(96.759)	10.509(97.449)	10.539(97.730)	10.559(97.915)
	4	10.443(96.838)	10.536(97.695)	10.563(97.954)	10.582(98.120)
1780	8	10.560(97.923)	10.650(98.759)	10.656(98.816)	10.677(99.006)
	24	10.710(99.286)	10.737(99.564)	10.729(99.487)	10.746(99.648)

3.3

.

4 1670 .  $(2 \text{ ton/cm}^2)$  $(4 \text{ ton/cm}^2)$ 

.[22]



3.605 μm 5.287 μm 7 · . 6

.[21]

,

$$d^{n} - d_{0}^{n} = C_{1} \exp\left(-\frac{Q}{RT}\right) \cdot \Delta t$$
 (2)







1780 8hrs, 2ton, x500

1780 24hrs, 2ton, x1000

$O_2$		1550	2000		n	2.5	가
	•						
	d =	1.086 +	$0.568 t^{0.4}$ ( $T = 1670$	)		(3)	)
	<i>d</i> =	1.852 +	$0.587 t^{0.4}$ ( $T = 1730$	)		(4)	)
	<i>d</i> =	2.325 +	$0.857 t^{0.4}$ ( $T = 1780$	)		(5)	)

.[22]

 $BaZrO_3$ 

4

5000 Mo-Ru-Rh-Pd

perovskite





(1780,4)

4.

1. 7 tubular . (apparent density) 1.3444 g/cm<sup>3</sup> , tubular 2.3352 g/cm<sup>3</sup> 7 . (granulation) tubular .

2.	2.							tubular						$\mu$ m,
0.45	$\mu$ m	0.37	μm	,				tu	bular			가		
3.												,		
			=	3.17	9 + 1	.801 F	1/3							
77				,	0		(		), P	,	0		Α, Β	
К 4				•					71			C		
4.						(10.3	$a/cm^{3}$		10.6 g/cm	2 <sup>3</sup> )		. (		
1730						(10.2	, <u>6</u> , cm		10.0 5/ 01					
5.														
	d	= :	1.086	+	0.5681	$t^{0.4}$ ( T	= 1670	)						
	d :	= :	1.852	+	0.5871	$t^{0.4}$ ( T	= 1730	)						
	d :	= 2	2.325	+	0.8571	$t^{0.4}$ ( T	= 1780	)						
	d			,	t									
1.	,	"						", K/	AERI/ RR -	1311/9	3			
2. H	angbok compos	Ch cition	oi and n", KA	l Gy AERI	uhong /TR-9	g Roh, 942/98(	"A sen (1998)	sitivi	ty study	on DU	JPIC f	uel		
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