

M<sub>3</sub>O<sub>8</sub> 가 UO<sub>2</sub>-Gd<sub>2</sub>O<sub>3</sub>

Characteristics of M<sub>3</sub>O<sub>8</sub>-added UO<sub>2</sub>-Gd<sub>2</sub>O<sub>3</sub> pellet

150

M<sub>3</sub>O<sub>8</sub> 가가 UO<sub>2</sub>-6wt%Gd<sub>2</sub>O<sub>3</sub> UO<sub>2</sub>-10wt%Gd<sub>2</sub>O<sub>3</sub> ( , , ,  
 , Gd ) . M<sub>3</sub>O<sub>8</sub> 가  
 M<sub>3</sub>O<sub>8</sub> 가 가 (0.035% TD/wt%) , M<sub>3</sub>O<sub>8</sub>  
 가 M<sub>3</sub>O<sub>8</sub> 가 .  
 M<sub>3</sub>O<sub>8</sub> 가 가 가 20 % M<sub>3</sub>O<sub>8</sub> 가  
 가 13μm .

**Abstract**

The effect of M<sub>3</sub>O<sub>8</sub> addition on the pellet properties such as density, grain size, microstructure and Gd homogeneity has been investigated in UO<sub>2</sub>-6wt%Gd<sub>2</sub>O<sub>3</sub> and UO<sub>2</sub>-10wt%Gd<sub>2</sub>O<sub>3</sub> pellets. The sintered density of as-received M<sub>3</sub>O<sub>8</sub>-added pellet decreased linearly with the M<sub>3</sub>O<sub>8</sub> content at the rate of 0.035% TD per 1wt% M<sub>3</sub>O<sub>8</sub>. However, the sintered density of milled M<sub>3</sub>O<sub>8</sub>-added pellet remained invariant with the M<sub>3</sub>O<sub>8</sub> content. The grain size increased with M<sub>3</sub>O<sub>8</sub> content and, thus grain size was about 13μm at 20wt% M<sub>3</sub>O<sub>8</sub>.

**1.**

가 (Gd<sub>2</sub>O<sub>3</sub>) 가 UO<sub>2</sub> , UO<sub>2</sub>-Gd<sub>2</sub>O<sub>3</sub> 가  
 가 [1,2]. Gd<sub>3</sub>O<sub>3</sub>  
 가 4~10wt% 가  
 . UO<sub>2</sub>-Gd<sub>2</sub>O<sub>3</sub> UO<sub>2</sub>  
 [3]. UO<sub>2</sub>-Gd<sub>2</sub>O<sub>3</sub>  
 (U,Gd)<sub>3</sub>O<sub>8</sub> ( M<sub>3</sub>O<sub>8</sub>

)

$UO_2-Gd_2O_3$

$UO_2-Gd_2O_3$

$M_3O_8$  가

$M_3O_8$  가

$M_3O_8$  가  $UO_2-Gd_2O_3$

,  $UO_2-Gd_2O_3$   $475^\circ C$   $M_3O_8$  0~20wt%

가  $UO_2-Gd_2O_3$  ,  $M_3O_8$  가  $UO_2-Gd_2O_3$

## 2.

### 2-1. $M_3O_8$

Scrap  $UO_2-Gd_2O_3$  AUC- $UO_2$  6, 10wt%  $Gd_2O_3$

가 1 attrition mill

(AZB) 0.5 % 가 1 , 3 ton/cm<sup>2</sup>

4  $UO_2-Gd_2O_3$  475°C wet hydrogen

4  $M_3O_8$  X-ray

SEM

laser light scattering

### 2-2. Scrap

$UO_2-Gd_2O_3$

Scrap  $UO_2-Gd_2O_3$  1 AUC-

$UO_2$  6, 10wt%  $Gd_2O_3$   $M_3O_8$  가 1

,  $M_3O_8$  가 (case1)

가 (case2) attrition mill

(AZB) 0.5 % 가 1

, 1 ton/cm<sup>2</sup> (slug)

3 ton/cm<sup>2</sup>

1730°C wet hydrogen

(dew point 24°C) 4

Gd

EPMA

3.

2(a), (b)  $\text{UO}_2$ -6wt%  $\text{Gd}_2\text{O}_3$   $\text{UO}_2$ -10wt%  $\text{Gd}_2\text{O}_3$  475°C  
 4 X- 6wt%  
 10wt%  $\text{Gd}_2\text{O}_3$  475°C  
 $\text{M}_3\text{O}_8$   $\text{UO}_2$ - $\text{Gd}_2\text{O}_3$  Gd  
 [4,5]. Gd 가  
 $\text{M}_4\text{O}_8$  [6].  
 scrap ,  $\text{M}_3\text{O}_8$

3(a), (b)  $\text{UO}_2$ -6wt%  $\text{Gd}_2\text{O}_3$   $\text{UO}_2$ -10wt%  $\text{Gd}_2\text{O}_3$  475°C  
 $\text{M}_3\text{O}_8$  SEM  
 6wt% $\text{Gd}_2\text{O}_3$   $\text{M}_3\text{O}_8$  10 $\mu\text{m}$   
 10wt% $\text{Gd}_2\text{O}_3$   $\text{M}_3\text{O}_8$  16 $\mu\text{m}$  Gd  $\text{M}_3\text{O}_8$   
 가 .

4  $\text{M}_3\text{O}_8$  가 (case1) 가 (case  
 2)  $\text{M}_3\text{O}_8$  가 .  $\text{M}_3\text{O}_8$   
 가 6wt% 10wt%  $\text{Gd}_2\text{O}_3$   
 1wt%  $\text{M}_3\text{O}_8$  가 0.035% ,  $\text{M}_3\text{O}_8$  가  
 6wt% 10wt%  $\text{Gd}_2\text{O}_3$   $\text{M}_3\text{O}_8$  가

$\text{UO}_2$  scrap  $\text{U}_3\text{O}_8$  가 가  
 , 1wt%  $\text{U}_3\text{O}_8$  0.09~0.15% .  $\text{U}_3\text{O}_8$   
 $\text{U}_3\text{O}_8$  0.5  $\text{m}^2/\text{g}$   $\text{UO}_2$   
 ,  $\text{U}_3\text{O}_8$   
 가 500°C  
 가 30%  $\text{U}_3\text{O}_8$

가 .  $\text{M}_3\text{O}_8$   
 $\text{M}_3\text{O}_8$  가 .

$M_3O_8$  가  $M_3O_8$  가  
 $M_3O_8$  ,  $M_3O_8$   
 $M_3O_8$  가  $M_3O_8$   
 $M_3O_8$   
가  $M_3O_8$  가 가  $M_3O_8$  가  
5(a), (b)  $M_3O_8$  가  $M_3O_8$  20wt% 가  
 $UO_2$ -6wt%  $Gd_2O_3$  , 6  
가  
 $10\mu m$  가  $M_3O_8$  20wt% 가  
 $M_3O_8$  가  $4\mu m$   
7  $UO_2$ -6wt%  $Gd_2O_3$  10wt%  $Gd_2O_3$   $M_3O_8$  가  
, 8(a), (b) 9(a), (b)  
.  $M_3O_8$  가 가 가 가 6wt%  
 $Gd_2O_3$   $M_3O_8$  가 가  $9.4\mu m$  10wt% 가  
 $11.2\mu m$ , 20wt% 가  $13.4\mu m$  . 10wt%  $Gd_2O_3$   
 $M_3O_8$  가  $11.2\mu m$  10wt% 가  
 $12.4\mu m$ , 20wt% 가  $13.2\mu m$  . cluster  
10 11  $M_3O_8$  10wt% 가  $UO_2$ -6wt%  $Gd_2O_3$   
Gd EPMA line profile area mapping  
Gd Gd  $UO_2$   
. Gd  
 $Gd_2O_3$  [7] Gd  
 $UO_2$  가

4.

- 1)  $M_3O_8$  가 (U,Gd) $O_2$  1wt%  $M_3O_8$  가  
 0.035% ,  $M_3O_8$  가 (U,Gd) $O_2$   
 $M_3O_8$  가 .
- 2)  $M_3O_8$  가 가 가 가 20 %  $M_3O_8$  가  
 13 $\mu$ m .
- 3)  $M_3O_8$  10wt% 가  $UO_2$ -6wt%  $Gd_2O_3$  Gd , Gd  
 Gd  $UO_2$  .

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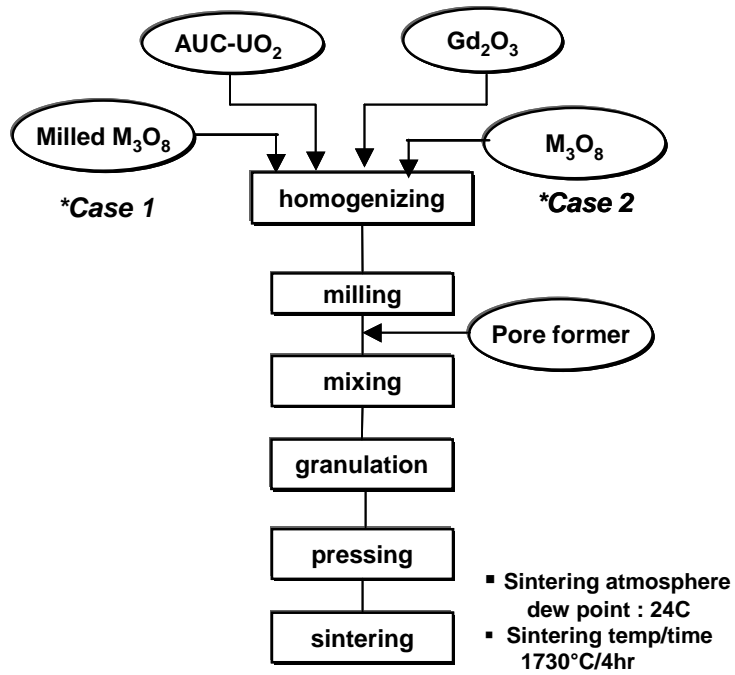
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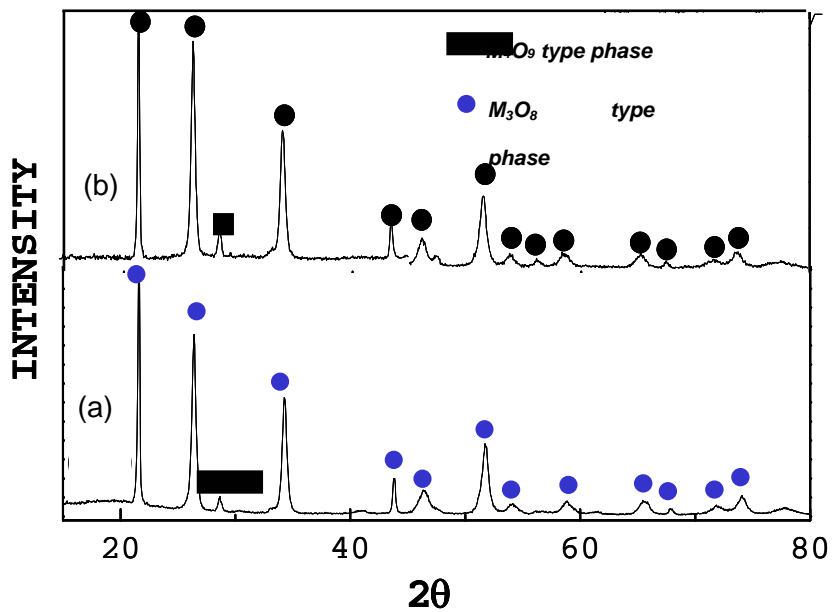
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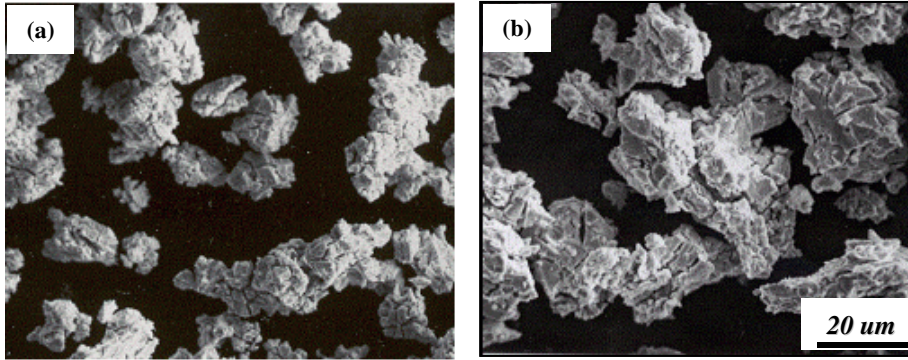
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1. Scrap UO<sub>2</sub>-Gd<sub>2</sub>O<sub>3</sub>  
 (\*case1 : M<sub>3</sub>O<sub>8</sub> 가, case2 : as-received M<sub>3</sub>O<sub>8</sub> 가)



2. 475°C M<sub>3</sub>O<sub>8</sub> XRD  
 (a) UO<sub>2</sub>-6wt%Gd<sub>2</sub>O<sub>3</sub>, (b) UO<sub>2</sub>-10wt%Gd<sub>2</sub>O<sub>3</sub>

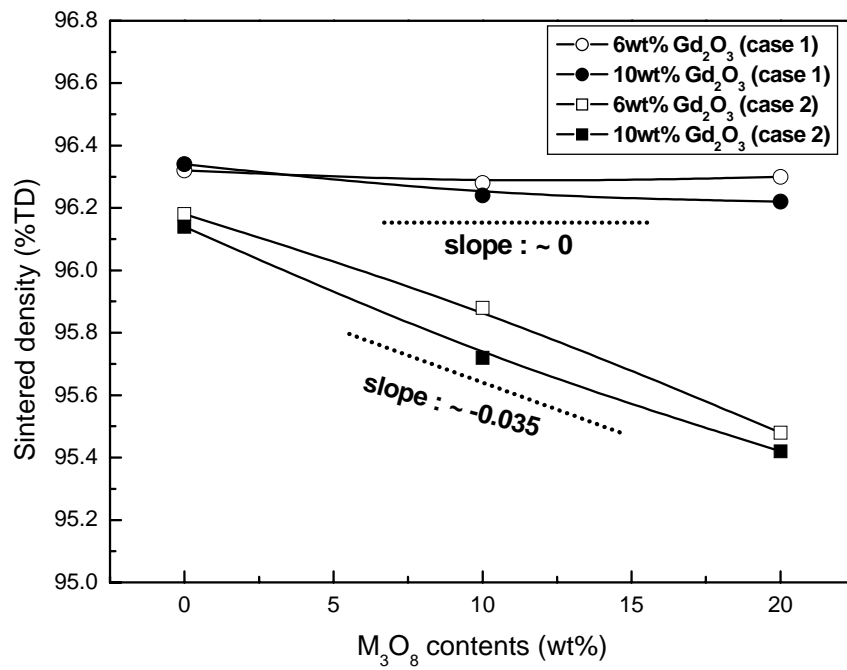


3. 475°C

$M_3O_8$

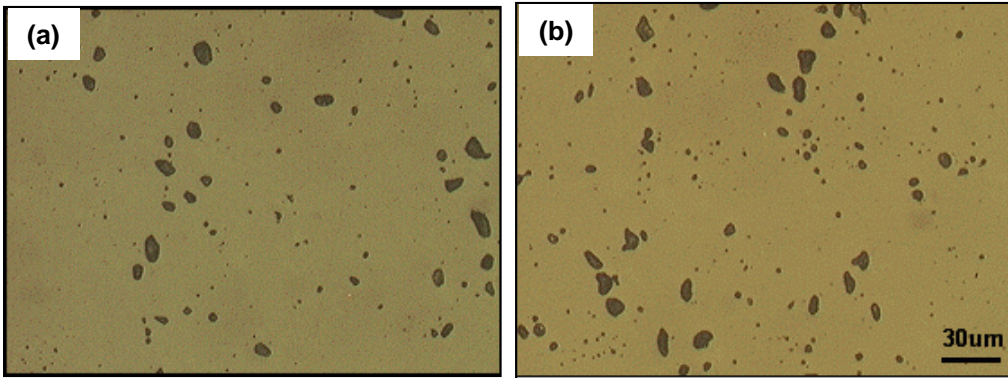
SEM

(a)  $UO_2$ -6wt% $Gd_2O_3$ , (b)  $UO_2$ -10wt% $Gd_2O_3$



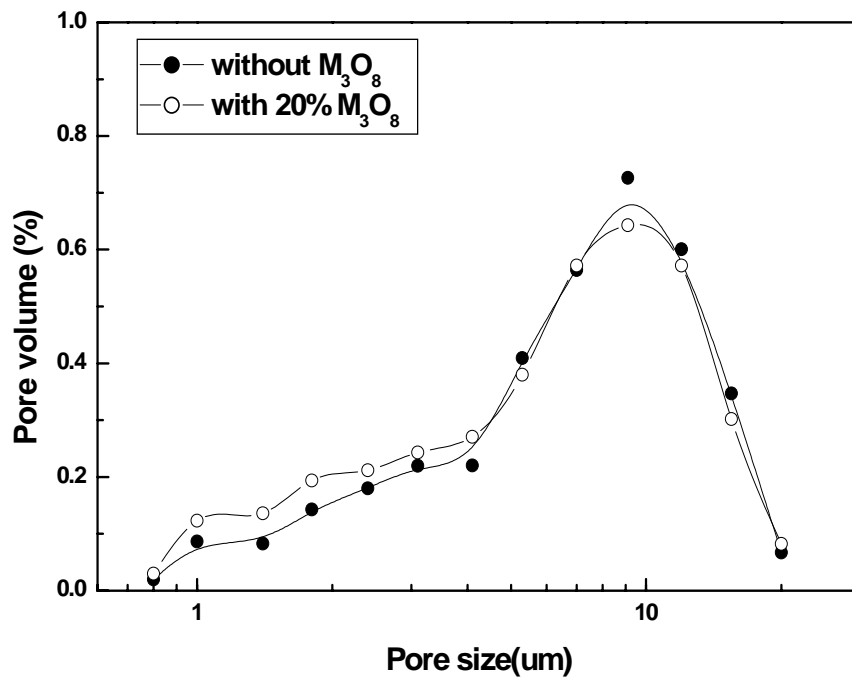
4.  $M_3O_8$  가

$UO_2$ - $Gd_2O_3$



5.  $\text{UO}_2\text{-6wt\%Gd}_2\text{O}_3$

(a) without  $\text{M}_3\text{O}_8$ , (b) with 20wt%  $\text{M}_3\text{O}_8$

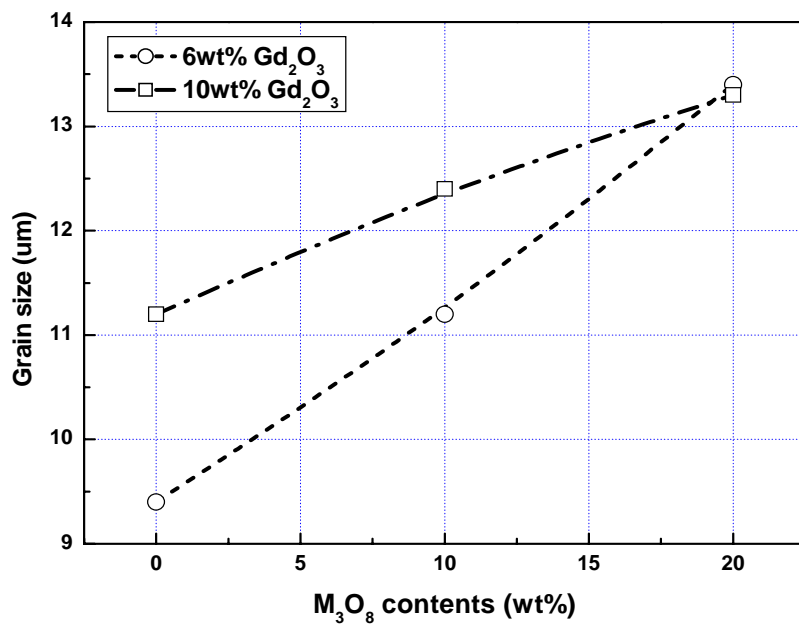


6.  $\text{M}_3\text{O}_8$  가

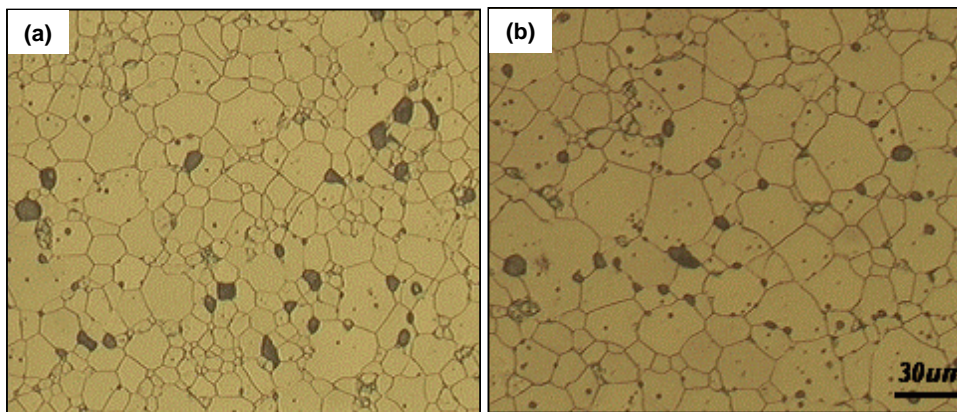
20%  $\text{M}_3\text{O}_8$  가

$\text{UO}_2\text{-6wt\%Gd}_2\text{O}_3$



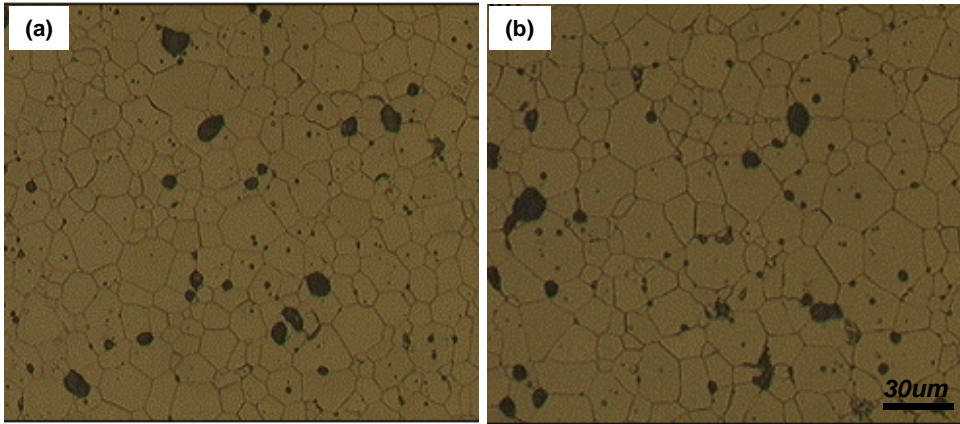


7. M<sub>3</sub>O<sub>8</sub> 가



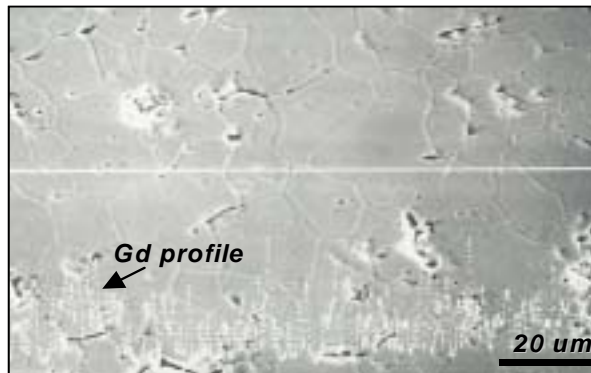
8. UO<sub>2</sub>-6wt%Gd<sub>2</sub>O<sub>3</sub>

(a) without M<sub>3</sub>O<sub>8</sub>, (b) with 20wt% M<sub>3</sub>O<sub>8</sub>



9.  $\text{UO}_2$ -10wt% $\text{Gd}_2\text{O}_3$

(a) without  $\text{M}_3\text{O}_8$ , (b) with 20wt%  $\text{M}_3\text{O}_8$

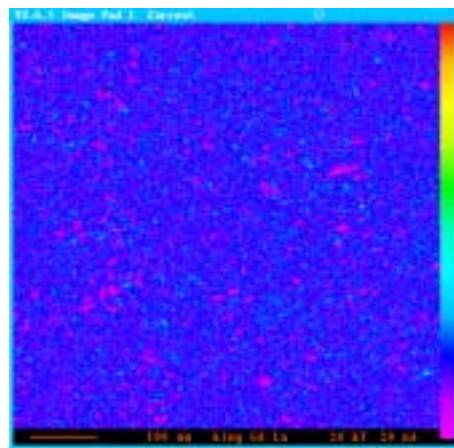


10.  $\text{UO}_2$ -6wt% $\text{Gd}_2\text{O}_3$

(EPMA

Gd

line profile)



11.  $\text{UO}_2$ -6wt% $\text{Gd}_2\text{O}_3$

(EPMA

Gd

area mapping)