# Manufacturing of nuclear fuel pellets by using re-oxidized U<sub>3</sub>O<sub>8</sub> powder

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### 1. Introduction

In a commercial UO<sub>2</sub> fuel pellets manufacturing process, defective UO<sub>2</sub> pellets which do not meet the fuel specifications of density and diameter may be produced. Defective UO<sub>2</sub> pellets should be reused in manufacturing new UO<sub>2</sub> pellets. It is a common recycling method that defective UO<sub>2</sub> pellets are oxidized in air at about 450 °C to make U<sub>3</sub>O<sub>8</sub> powder and then added to  $UO_2$  powder [1]. Because the recycled U<sub>3</sub>O<sub>8</sub> powder has very low sintering activity compared to the UO<sub>2</sub> powder, it tends to decrease the density of UO<sub>2</sub> pellets. Other pellet properties such as grain size and open porosity are a little degraded by the addition of the U<sub>3</sub>O<sub>8</sub> powder. So the amount of the recycled  $U_3O_8$  powder is generally not higher than 10 wt% in UO<sub>2</sub> powder. There has been a series of work to deal with the heat treatments of the recycled U<sub>3</sub>O<sub>8</sub> powder in order to improve its sintering activity [2].

This paper deals with the recycling process of defective  $UO_2$  pellets or scraps. The defective  $UO_2$  pellets are oxidized to  $U_3O_8$  powders at conventional temperature of 350°C and 450°C in air. Those powders are pressed into green pellets and then sintered at 1700°C in H<sub>2</sub> flowing gas. Sintered pellets are re-oxidized to  $U_3O_8$  at 450°C in air. Re-oxidized powders are added to virgin  $UO_2$  powders to fabricate  $UO_2$  pellets. This paper shows that the re-oxidized  $U_3O_8$  powder sizes and the BET surface areas are greatly dependent on the sintered density of  $UO_2$  pellets before oxidation. The re-oxidized  $U_3O_8$  powders having a large BET surface area significantly promote a grain growth of  $UO_2$  pellets.

### 2. Experimental

The defective  $UO_2$  fuel pellets were oxidized at 350°C and 450°C in air, respectively. Those  $U_3O_8$  powders were pressed into green pellets. The compressive pressures were 1, 2, 3 ton/cm<sup>2</sup>, respectively. The green pellets were sintered at 1700°C for 4h in H<sub>2</sub> gas. Re-oxidized  $U_3O_8$  powders were prepared by re-oxidation of above sintered pellets at 450°C. The re-oxidized  $U_3O_8$  powders morphology were examined by SEM and their BET surface areas were measured by BET surface area analyzer.

Two groups of  $U_3O_8$  powder were prepared. First one is as-received un-doped  $U_3O_8$  and other is Al doped

 $U_3O_8$  powders. 5wt% of those  $U_3O_8$  powders was added to the UO<sub>2</sub> powder, which was produced through the ADU process. In Al-doped powders, the final cation weight ratio of Al/U was 40 ppm. Powder mixtures were mixed with a tumbling mixer. The powder mixture was pressed into green pellets at 3 ton/cm<sup>2</sup>. The green pellets were sintered at 1730°C for 4 h in flowing H<sub>2</sub> gas.

The sintered density of  $UO_2$  pellets was measured by the water immersion method. The pellets were sectioned axially, ground and polished. The polished pellets were thermally etched at 1290°C in carbon dioxide gas in order to examine grain boundaries. The pore and grain structure were examined by an optical microscope and grain size was determined by the linear intercept method.

## 3. Results

Fig. 1 shows the pellet densities which were fabricated by sintering the  $U_3O_8$  powders. It can be seen that sintered densities depend on the oxidation temperatures of defective pellets and the pressures for green pellets compaction. The low oxidation temperature and high compaction pressure resulted in higher density of the sintered pellets.

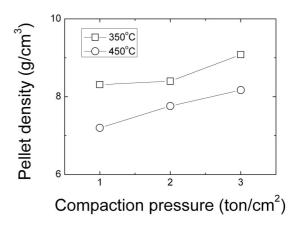


Fig.1. The sintered pellet density dependence on the compaction pressure of green pellets.

The sintered pellets were re-oxidized at 450°C in air. Fig. 2 shows the BET surface area of the re-oxidized  $U_3O_8$  powder according to the density of sintered pellets. The BET surface area has a tendency to increase with a decreasing sintered pellet density. The BET surface area of  $U_3O_8$  powder which obtained by an oxidation of defective  $UO_2$  pellet at 450°C is also shown in this figure (left-lower part). The BET surface area of the re-oxidized  $U_3O_8$  powder can be significantly increased when the sintered pellet before oxidation has low density.

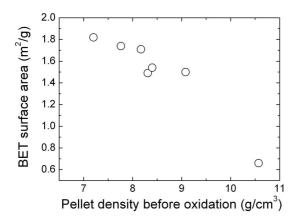


Fig. 2. The BET surface area changes of re-oxidized  $\rm U_3O_8$  powders according to the pellet density

It is known that powder having larger BET surface area has more sintering activity compared to that having lower BET surface area. The effect of the re-oxidized  $U_3O_8$  powder property on the grain growth of  $UO_2$ pellet has been examined. Fig. 3 shows the grain size distribution for the  $UO_2$  pellets in which 5wt% of undoped and Al-doped  $U_3O_8$  were contained.

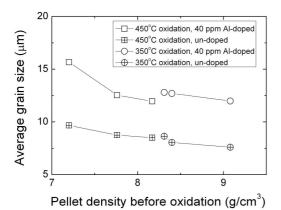


Fig. 3. The re-oxidized  $U_3O_8$  powder effects on the grain size of  $UO_2$  pellets.

The average grain size of  $UO_2$  pellets are increased with decreasing density of sintered pellet before oxidation. This result is coincident with our expectation from the measured BET surface areas of different  $U_3O_8$ powders. That is, the  $U_3O_8$  powder having large BET surface area promotes the grain growth of  $UO_2$  pellets more effectively. Especially, the grain size of 40ppm Al-doped UO<sub>2</sub> pellets are enlarged to about 16  $\mu$ m which is about 2 times larger than the conventionally fabricated UO<sub>2</sub> pellets. Fig. 4 shows the photos of the grain structures of the 5wt% of U<sub>3</sub>O<sub>8</sub> and 40ppm Al doped-UO<sub>2</sub> pellets. The BET surface areas of U<sub>3</sub>O<sub>8</sub> are 1.82m<sup>2</sup>/g for Fig. 4(a) and 1.49m<sup>2</sup>/g for Fig. 4(b), respectively. It can be clearly seen that pellet of Fig.4 (a) has more sound pore structure and larger grain size.

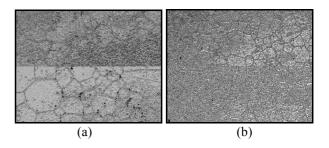


Fig. 4. The grain structures of 5wt% of  $U_3O_8$  and 40 ppm Al containing  $UO_2$  pellets. The BET surface area of  $U_3O_8$  are (a)  $1.82m^2/g$  and (b)  $1.49m^2/g$ .

## 4. Summary

By sintering the  $U_3O_8$  powders from defective pellets or scrap into  $UO_2$  pellets and then re-oxidizing it into  $U_3O_8$  powders, the  $U_3O_8$  powder morphology and its BET surface area can be controlled. The BET surface area of the re-oxidized  $U_3O_8$  powder is increased with decreasing the sintered pellet density before oxidation. The  $U_3O_8$  powder having higher BET surface area acts as grain-size-enlarging promoter of  $UO_2$  pellet more effectively.

## Acknowledgements

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#### REFERENCES

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